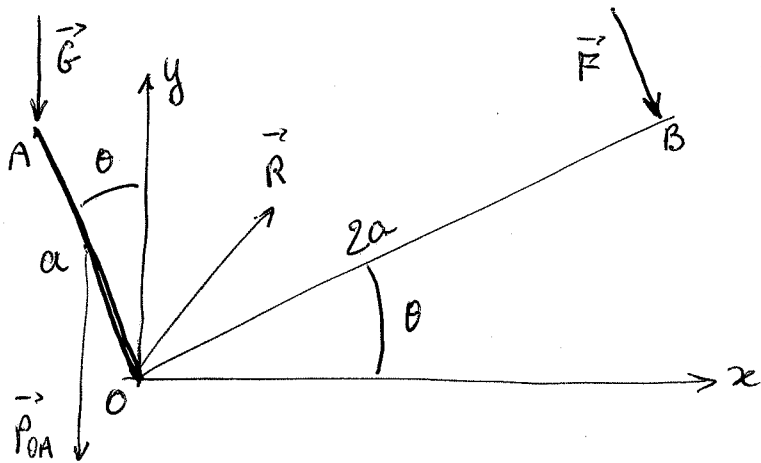


Equilibre statique d'une barre courbée



$$11) \quad \vec{G} = \begin{pmatrix} 0 \\ -G \\ 0 \end{pmatrix} \quad \vec{F} = \begin{pmatrix} F \sin \theta \\ -F \cos \theta \\ 0 \end{pmatrix} \quad \vec{P}_{OA} = \begin{pmatrix} 0 \\ -mg \\ 0 \end{pmatrix} \quad \vec{R} = \begin{pmatrix} R_x \\ R_y \\ R_z \end{pmatrix}$$

Equilibre statique: $\sum \vec{F}_{\text{ext}} = \vec{0} \quad \sum \vec{M}_O(\vec{F}_{\text{ext}}) = \vec{0}$

12) 124) On calcule la résultante des moments en O :

$$\begin{aligned} \sum \vec{M}_O(\vec{F}_{\text{ext}}) &= \vec{OA} \wedge \vec{G} + \vec{OB} \wedge \vec{F} + \frac{\vec{OA}}{2} \wedge \vec{P}_{OA} + \vec{OO} \wedge \vec{R} \\ &= \begin{vmatrix} -a \sin \theta & 0 \\ a \cos \theta & -G \\ 0 & 0 \end{vmatrix} \wedge \begin{pmatrix} 0 \\ -G \\ 0 \end{pmatrix} + \begin{vmatrix} 2a \cos \theta & 0 \\ 2a \sin \theta & -F \cos \theta \\ 0 & 0 \end{vmatrix} \wedge \begin{pmatrix} F \sin \theta \\ -F \cos \theta \\ 0 \end{pmatrix} + \begin{vmatrix} -\frac{a}{2} \sin \theta & 0 \\ \frac{a}{2} \cos \theta & -mg \\ 0 & 0 \end{vmatrix} \wedge \begin{pmatrix} 0 \\ -mg \\ 0 \end{pmatrix} \\ &= \left[aG \sin \theta - 2aF \cos^2 \theta - 2aF \sin^2 \theta + \frac{amg}{2} \sin \theta \right] \vec{e}_z = 0 \end{aligned}$$

$$\Rightarrow aG \sin \theta - 2aF + \frac{amg}{2} \sin \theta = 0$$

$$\left(G + \frac{mg}{2} \right) \sin \theta = 2F \quad \rightarrow \quad \theta = \arcsin \left[\frac{2F}{G + \frac{mg}{2}} \right]$$

Mouvement Circulaire uniformément accéléré

Coordonnées polaires: $\vec{OM} = r \vec{e}_r$

$$\vec{v} = \begin{pmatrix} \dot{r} \\ r\dot{\theta} \end{pmatrix} \quad \vec{a} = \begin{pmatrix} \ddot{r} - r\dot{\theta}^2 \\ 2\dot{r}\dot{\theta} + r\ddot{\theta} \end{pmatrix}$$

21) ici $R = \text{cte}$ et $\ddot{\theta} = \text{cte} \Rightarrow r = R, \dot{r} = 0, \ddot{r} = 0$

$$\Rightarrow \vec{OM} = R \vec{e}_r \quad \vec{v} = R\dot{\theta} \vec{e}_\theta \quad \vec{a} = -R\dot{\theta}^2 \vec{e}_r + R\ddot{\theta} \vec{e}_\theta$$

$$\dot{\theta} = \int \ddot{\theta} dt = \ddot{\theta} t + c_1 \quad \text{à } t=0; \dot{\theta}=0 \rightarrow c_1 = 0$$

$$\Rightarrow \boxed{\dot{\theta} = \ddot{\theta} t}$$

$$\theta = \int \dot{\theta} dt = \frac{\ddot{\theta} t^2}{2} + c_2 \quad \text{à } t=0; \theta=0 \rightarrow c_2 = 0$$

$$\Rightarrow \theta = \frac{1}{2} \ddot{\theta} t^2$$

en B, $\theta = \pi \Rightarrow$

$$\boxed{t = \left(\frac{2\pi}{\ddot{\theta}} \right)^{1/2}}$$

221) $d\vec{l} = dO\vec{M} = dr \vec{e}_r + r d\vec{e}_r$

222) $\vec{a} = d^2 O\vec{M} / dt^2 \dots$ (cours et plus haut)

223) Principe fondamental de la dynamique: $\vec{F} = m\vec{a}$

de façon générale en base polaire: $\vec{F} = f_r \vec{e}_r + f_\theta \vec{e}_\theta$

avec $\vec{a} = -R\dot{\theta}^2 \vec{e}_r + R\ddot{\theta} \vec{e}_\theta$: $\vec{F} = m(-R\dot{\theta}^2 \vec{e}_r + R\ddot{\theta} \vec{e}_\theta)$

identifiants:

$$\boxed{\begin{aligned} f_r &= -mR\dot{\theta}^2 \\ f_\theta &= mR\ddot{\theta} \end{aligned}}$$

23) On peut ici utiliser 2 méthodes :

a) définition du travail élémentaire :

$$dW = \vec{F} \cdot d\vec{\ell} = \vec{F} \cdot d\vec{OM}$$

$$d\vec{OM} = d(R\vec{e}_r) = R d\vec{e}_r = R d\theta \vec{e}_\theta \quad (\vec{e}_\theta = \frac{d\vec{e}_r}{d\theta})$$

$$\vec{F} = -mR\dot{\theta}^2 \vec{e}_r + mR\ddot{\theta} \vec{e}_\theta \quad (\text{exercice 12:})$$

$$\rightarrow dW = (-mR\dot{\theta}^2 \vec{e}_r + mR\ddot{\theta} \vec{e}_\theta) \cdot R d\theta \vec{e}_\theta$$

$$= mR^2 \ddot{\theta} d\theta$$

$$\vec{F} \text{ va de } A(\theta=0) \text{ à } B(\theta=\pi) : W_{A \rightarrow B} = \int_0^\pi dW$$

$$W_{A \rightarrow B} = \int_0^\pi mR^2 \ddot{\theta} d\theta = mR^2 \ddot{\theta} [\theta]_0^\pi = m\pi R^2 \ddot{\theta}$$

$$\boxed{W_{A \rightarrow B} = m\pi R^2 \ddot{\theta}}$$

b) Théorème de l'énergie cinétique :

$$W_{A \rightarrow B} = \frac{1}{2} m v_B^2 - \frac{1}{2} m v_A^2$$

$$v_A = 0 \quad \text{et} \quad v_B = R\dot{\theta}_B = R\ddot{\theta} t_B = R\ddot{\theta} \left(\frac{2\pi}{\dot{\theta}} \right)^{1/2}$$

$$\Rightarrow W_{A \rightarrow B} = \frac{1}{2} m (R\ddot{\theta})^2 \cdot \frac{2\pi}{\dot{\theta}} = \underline{m\pi R^2 \ddot{\theta}}$$

$$24) \vec{M}_O(\vec{F}(M)) = \vec{OM} \wedge \vec{F} = \begin{vmatrix} R & & -mR\dot{\theta}^2 \\ & \wedge & \\ 0 & & mR\ddot{\theta} \end{vmatrix} = mR^2 \ddot{\theta} \vec{e}_z$$

$$25) \vec{J}_O = \vec{OM} \wedge \vec{p} = \begin{vmatrix} R & & R \\ & \wedge & \\ 0 & & R\dot{\theta} \end{vmatrix} = mR^2 \dot{\theta} \vec{e}_z$$

Théorème du moment cinétique :

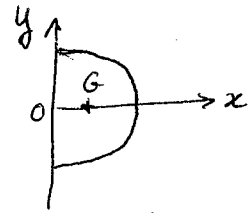
$$\frac{d\vec{\sigma}_0}{dt} = m R^2 \frac{d\dot{\theta}}{dt} \vec{e}_z = m R^2 \ddot{\theta} \vec{e}_z = \vec{M}_0(\vec{F}(m))$$

cqfd

Centre de Masse et Moment d'inertie

31) Théorème de Pappus: $y_G = 0$

(symétrie $\frac{1}{2}$
plan (xOz))



$$2\pi S x_G = V$$

$$S = \frac{1}{2}\pi R^2 \quad V = \frac{4}{3}\pi R^3 \quad \rightarrow \quad \frac{2\pi}{2} \pi R^2 x_G = \frac{4}{3}\pi R^3$$

$$\Rightarrow \boxed{x_G = \frac{4R}{3\pi}}$$

32)

$$I_{Gz} = I_{Oz} - m d^2(Gz, Oz)$$

$$d(Gz, Oz) = \frac{4R}{3\pi}$$

$$I_{Oz} = \int d^2 dm \quad d=r$$

$$dm = \sigma r d\theta dr$$

$$I_{Oz} = \sigma \int r^3 d\theta dr = \sigma \int_0^R r^3 dr \int_{-\frac{\pi}{2}}^{\frac{\pi}{2}} d\theta = \sigma \frac{R^4}{4} \cdot \pi$$

$$m = \sigma \frac{\pi R^2}{2} \quad \rightarrow \quad \sigma = \frac{2m}{\pi R^2}$$

$$I_{Oz} = \frac{2m}{\pi R^2} \cdot \frac{R^4 \pi}{4} = \frac{m R^2}{2}$$

$$I_{Gz} = \frac{m R^2}{2} - m \left(\frac{4R}{3\pi} \right)^2 = m R^2 \left(\frac{1}{2} - \frac{16}{9\pi^2} \right)$$

$$\boxed{I_{Gz} = m R^2 \left(\frac{1}{2} - \frac{16}{9\pi^2} \right)}$$

Oscillateur Amorti

44) On avait le choix !

$$\sum M_{O_3} = I_{O_3} \ddot{\theta} ; \quad \frac{dE_m}{dt} = \mathcal{P}_{\text{non cons.}} ; \quad \frac{dE_c}{dt} = \mathcal{P}(\vec{F})$$

Forces: poids \vec{P} appliqué en G

amortissement $M_{O_3} = -\alpha \dot{\theta}$

$$\underline{\sum M_{O_3} = I_{O_3} \ddot{\theta}} ; \quad \vec{M}_{O_3}(\vec{P}) = \vec{OG} \wedge \vec{P} = -mgb \sin\theta \vec{e}_3$$

$$\rightarrow M_{O_3}(\vec{P}) = (\vec{OG} \wedge \vec{P}) \cdot \vec{e}_3 = -mgb \sin\theta$$

$$\rightarrow I_{O_3} \ddot{\theta} = -mgb \sin\theta - \alpha \dot{\theta} \quad (\text{avec } \sin\theta \approx \theta)$$

$$\rightarrow \boxed{amR^2 \ddot{\theta} + \alpha \dot{\theta} + mgb\theta = 0}$$

$$\underline{\frac{dE_m}{dt} = \mathcal{P}_{\text{non cons.}} ;}$$

$$E_c = \frac{1}{2} I_{O_3} \dot{\theta}^2$$

$$\frac{dE_c}{dt} = I_{O_3} \dot{\theta} \ddot{\theta}$$

$$E_p = mg(R - b \cos\theta)$$

$$\frac{dE_p}{dt} = mgb \dot{\theta} \sin\theta$$

$$\mathcal{P}(M_{O_3}) = -\alpha \dot{\theta}^2$$

$$amR^2 \dot{\theta} \ddot{\theta} + mgb \dot{\theta} \sin\theta + \alpha \dot{\theta}^2 = 0$$

$$amR^2 \ddot{\theta} + \alpha \dot{\theta} + mgb\theta = 0$$

$$\frac{dE_c}{dt} = \mathcal{P}(\vec{F}) :$$

$$\frac{dE_c}{dt} = \mathcal{P}(\vec{P}) + \mathcal{P}(M_{Oy})$$

$$E_c = \frac{1}{2} I_{Oy} \dot{\theta}^2 \quad \frac{dE_c}{dt} = I_{Oy} \dot{\theta} \ddot{\theta}$$

$$\mathcal{P}(\vec{P}) = m \vec{g} \cdot \vec{v}(G)$$

$$\vec{OG} = \begin{pmatrix} b \sin \theta \\ -b \cos \theta \\ 0 \end{pmatrix} \rightarrow \mathcal{P}(\vec{P}) = \begin{vmatrix} 0 \\ -mg \\ 0 \end{vmatrix} \cdot \begin{pmatrix} b \cos \theta \\ b \sin \theta \\ 0 \end{pmatrix}$$

$$\vec{v}(G) = \frac{d\vec{OG}}{dt} = \dot{\theta} \begin{pmatrix} b \cos \theta \\ -b \sin \theta \\ 0 \end{pmatrix} = -mgb \sin \theta \dot{\theta}$$

$$\rightarrow I_{Oy} \dot{\theta} \ddot{\theta} = -mgb \dot{\theta} \sin \theta - \alpha \dot{\theta}^2 \quad (\sin \theta \approx \theta)$$

$$am R^2 \ddot{\theta} + mgb \theta + \alpha \dot{\theta} = 0$$

42) On met l'équation sous la forme: $\ddot{\theta} + 2\xi\omega_0 \dot{\theta} + \omega_0^2 \theta = 0$

$$\ddot{\theta} + \frac{\alpha}{am R^2} \dot{\theta} + \frac{gb}{a R^2} \theta = 0$$

$$\rightarrow \left[\omega_0 = \left(\frac{gb}{a R^2} \right)^{1/2} \right] \quad \left[\xi = \frac{\alpha}{2mR \sqrt{abg}} \right]$$