

Combining texture, structure, microstructure and phase analyses for multiphase bulks and thin films diffraction characterisation: some case studies

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**Bi2223
Superconductors**

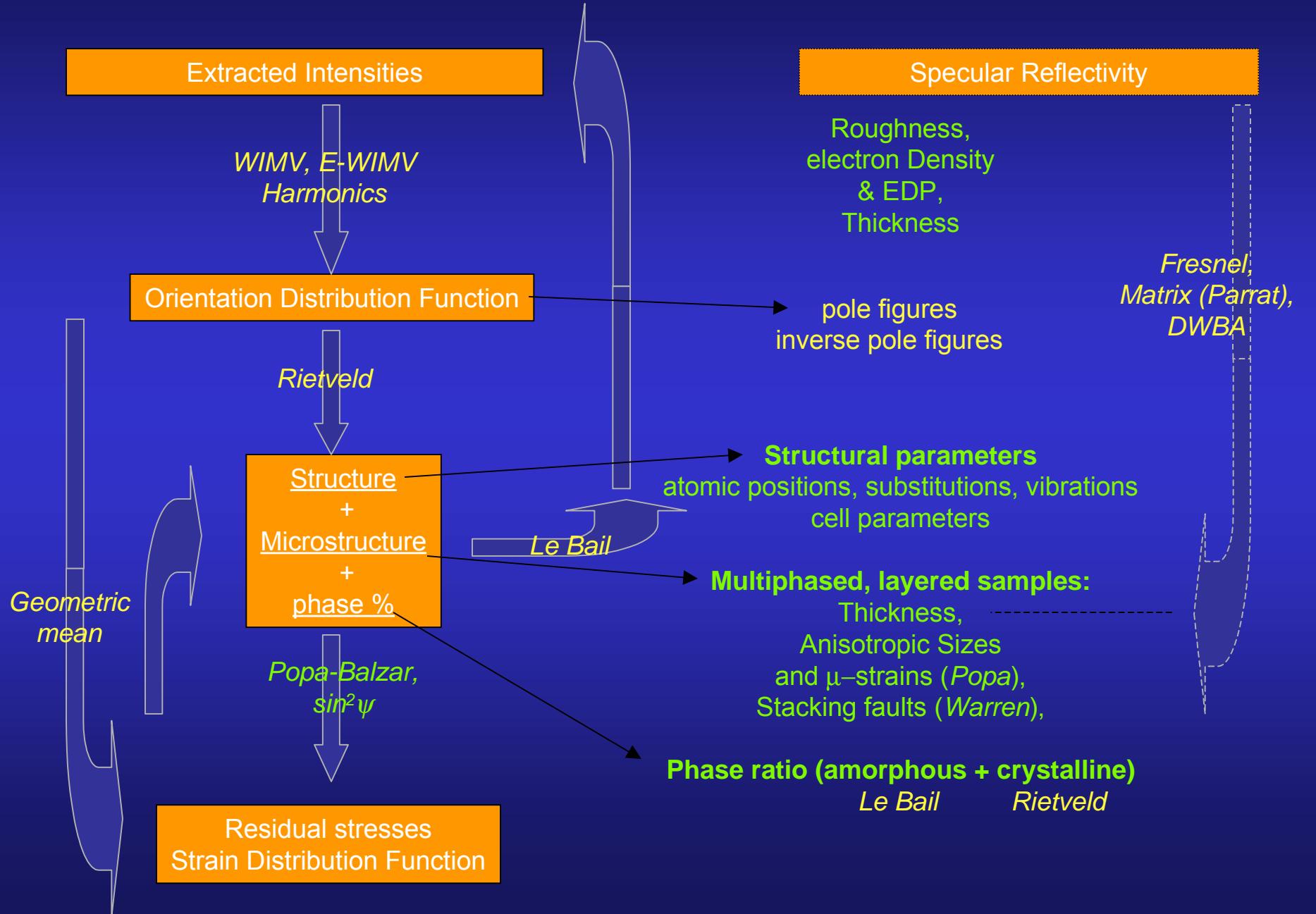
**Irradiated
FAp ceramics**

**$\text{Ca}_3\text{Co}_4\text{O}_9$
Thermoelectrics**

**PCT
Ferroelectrics**

**nano-Si
thin films**

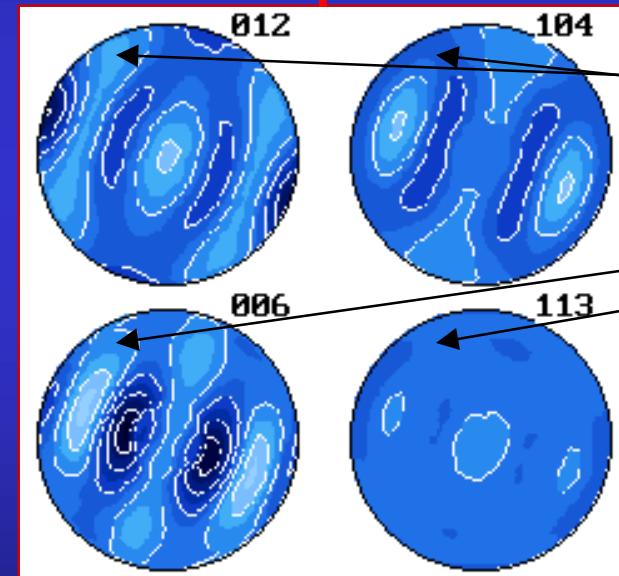
Implemented codes



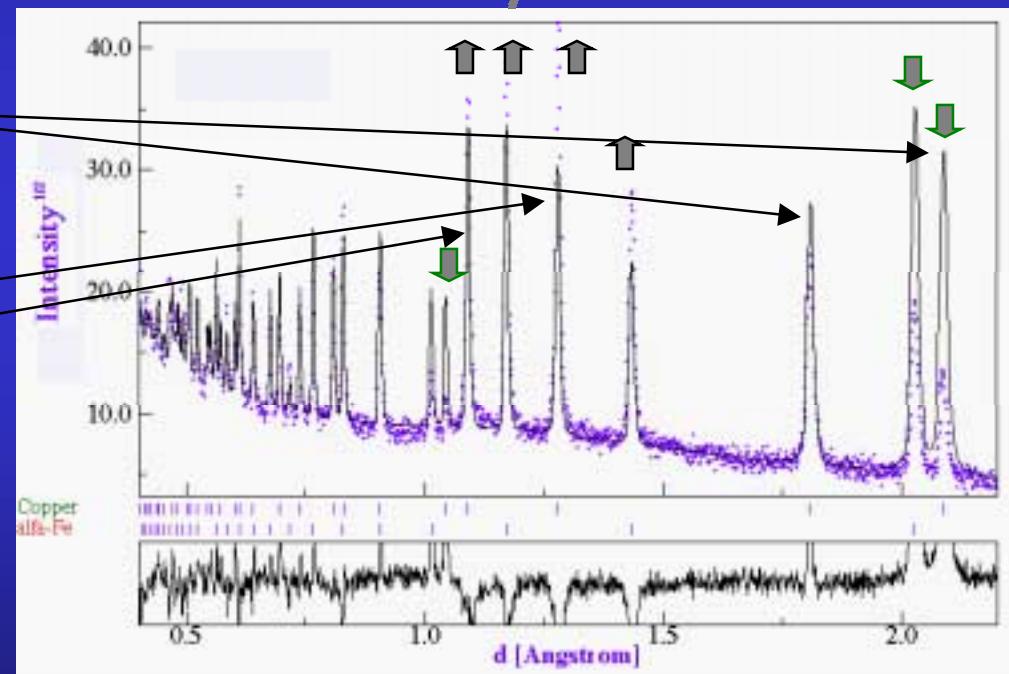
Texture from Spectra

Orientation Distribution Function (ODF)

From pole figures



From spectra



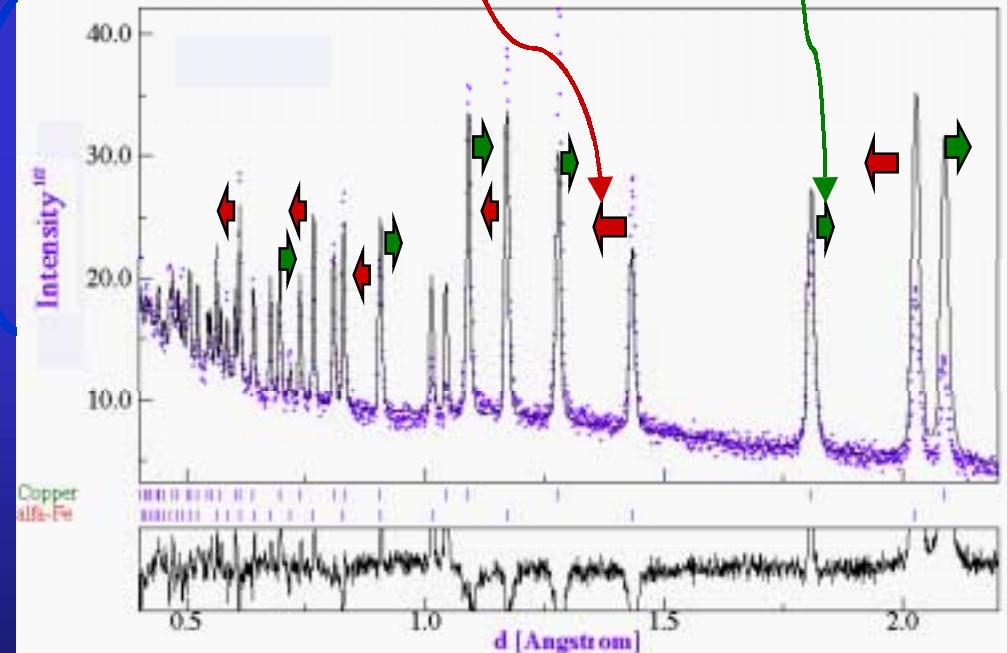
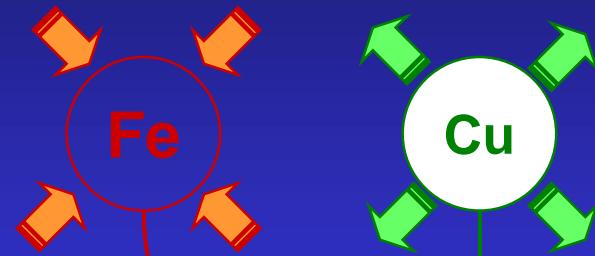
Residual Stresses and Rietveld

- Macro elastic strain tensor (I kind)
- Crystal anisotropic strains (II kind)

Macro and micro stresses

Applied macro stresses

C



Textured samples: Reuss, Voigt, Hill, Bulk geometric mean approaches

How it works (Combined)

$$I_i^{calc}(\chi, \phi) = \sum_{n=1}^{Nphases} S_n \sum_k L_k |F_{k;n}|^2 S(2\theta_i - 2\theta_{k;n}) P_{k;n}(\chi, \phi) A + bkg_i$$

Texture

$$P_k(\chi, \phi) = \int_{\varphi} f(g, \varphi) d\varphi$$

- from Generalized Spherical Harmonics:

$$P_k(\chi, \phi) = \sum_{l=0}^{\infty} \frac{1}{2l+1} \sum_{n=-l}^l k_l^n(\chi, \phi) \sum_{m=-l}^l C_l^{mn} k_n^{*m}(\Theta_k \phi_k)$$

$$f(g) = \sum_{l=0}^{\infty} \sum_{m,n=-l}^l C_l^{mn} T_l^{mn}(g)$$

- from the WIMV (left) iterative process or entropy maximisation (right):

$$f^{n+1}(g) = N_n \frac{f^n(g) f^0(g)}{\left(\prod_{\mathbf{h}=1}^I \prod_{m=1}^{M_{\mathbf{h}}} P_{\mathbf{h}}^n(\mathbf{y}) \right)^{\frac{1}{IM_{\mathbf{h}}}}}$$

$$f^{n+1}(g) = f^n(g) \prod_{m=1}^{M_{\mathbf{h}}} \left(\frac{P_{\mathbf{h}}(\mathbf{y})}{P_{\mathbf{h}}^n(\mathbf{y})} \right)^{\frac{r_{\mathbf{h}}}{M_{\mathbf{h}}}}$$

Layering

$$C_{\chi}^{\text{top film}} = g_1 (1 - \exp(-\mu T g_2 / \cos \chi)) / (1 - \exp(-2\mu T / \sin \omega \cos \chi))$$

$$C_{\chi}^{\text{cov. layer}} = C_{\chi}^{\text{top film}} \left(\exp\left(-g_2 \sum \mu_i' T_i' / \cos \chi\right) \right) / \left(\exp\left(-2 \sum \mu_i' T_i' / \sin \omega \cos \chi\right) \right)$$

Popa anisotropic shapes & microstrains

$$\langle R_h \rangle = R_0 + R_1 P_2^0(x) + R_2 P_2^1(x) \cos \varphi + R_3 P_2^1(x) \sin \varphi + R_4 P_2^2(x) \cos 2\varphi + R_5 P_2^2(x) \sin 2\varphi + \dots$$

$$\langle \varepsilon_h^2 \rangle E_h^4 = E_1 h^4 + E_2 k^4 + E_3 \ell^4 + 2E_4 h^2 k^2 + 2E_5 \ell^2 k^2 + 2E_6 h^2 \ell^2 + 4E_7 h^3 k + 4E_8 h^3 \ell + 4E_9 k^3 h + 4E_{10} k^3 \ell + 4E_{11} \ell^3 h + 4E_{12} \ell^3 k + 4E_{13} h^2 k \ell + 4E_{14} k^2 h \ell + 4E_{15} \ell^2 k h$$

Roughness and/or microabsorption

$$R^{rough}(q_z) = R(q_z) \exp(-q_{z,0} q_{z,1} \sigma^2) \quad \text{Low-angles (reflectivity)}$$

$$S_R = 1 - p \exp(-q) + p \exp\left(\frac{-q}{\sin \theta}\right) \quad \text{high-angle (Suortti)}$$

Specular reflectivity: $\mathbf{q}=(0,0,z)$

- Fresnel:

$$R(\mathbf{q}) = \left| \frac{q_z - \sqrt{q_z^2 - q_c^2 + \frac{32i\pi^2\beta}{\lambda^2}}}{q_z + \sqrt{q_z^2 - q_c^2 + \frac{32i\pi^2\beta}{\lambda^2}}} \right|^2 \delta q_x \delta q$$

- matrix:

$$R^{flat} = \frac{r_{0,1}^2 + r_{1,2}^2 + 2r_{0,1}r_{1,2} \cos 2k_{Z,1}h}{1 + r_{0,1}^2 r_{1,2}^2 + 2r_{0,1}r_{1,2} \cos 2k_{Z,1}h}$$

- Born approximation:

$$R(q_z) = r \cdot r^* = R_F(q_z) \left| \frac{1}{\rho_s} \int_{-\infty}^{+\infty} \frac{d\rho(z)}{dz} e^{iq_z z} dz \right|^2$$

Phase

$$W_{\Phi} = \frac{S_{\Phi} Z_{\Phi} M_{\Phi} V_{\Phi}}{\sum_{i=1}^{N_{\Phi}} S_i Z_i M_i V_i}$$

Strain-Stress

$$\boldsymbol{\varepsilon}(\mathbf{X}) = \boldsymbol{\varepsilon}^I + \boldsymbol{\varepsilon}^{II}(\mathbf{X}) + \boldsymbol{\varepsilon}^{III}(\mathbf{X})$$

$$\begin{aligned} \langle \boldsymbol{\varepsilon}_h(y) \rangle_{V_d} &= \frac{1}{V_d} \int_{V_d} (\boldsymbol{\varepsilon}_{33}^I + \boldsymbol{\varepsilon}_{33}^{II} + \boldsymbol{\varepsilon}_{33}^{III}) dV \\ &= (\boldsymbol{\varepsilon}_{11}^I \cos^2 \phi + \boldsymbol{\varepsilon}_{12}^I \sin 2\phi + \boldsymbol{\varepsilon}_{22}^I \sin^2 \phi - \boldsymbol{\varepsilon}_{33}^I) \sin^2 \psi + \boldsymbol{\varepsilon}_{33}^I + \\ &\quad (\boldsymbol{\varepsilon}_{13}^I \cos \phi + \boldsymbol{\varepsilon}_{23}^I \sin \phi) \sin 2\psi + \frac{1}{V_d} \int_{V_d} (\boldsymbol{\varepsilon}_{33}^{Iie} + \boldsymbol{\varepsilon}_{33}^{Iii} + \boldsymbol{\varepsilon}_{33}^{Ipi}) dV \\ &= \frac{\langle d(hkl, \phi, \psi) \rangle_{V_d} - d_0(hkl)}{d_0(hkl)} \end{aligned}$$

Isotropic samples:
triaxial, biaxial uniaxial stress state

Textured samples:
triaxial, biaxial uniaxial stress state
+ ODF + SDF + model

$$\begin{aligned} \langle E(g) \rangle_{V_d} &= \frac{1}{V_d} \int_{V_d} E^{SC}(g) f(g) dg \\ &= \left(\prod_{V_d} E^{SC}(g) f(g) dg \right)^{\frac{1}{V_d}} \end{aligned}$$

Reuss, Voigt, Hill

Geometric mean

Minimum experimental requirements



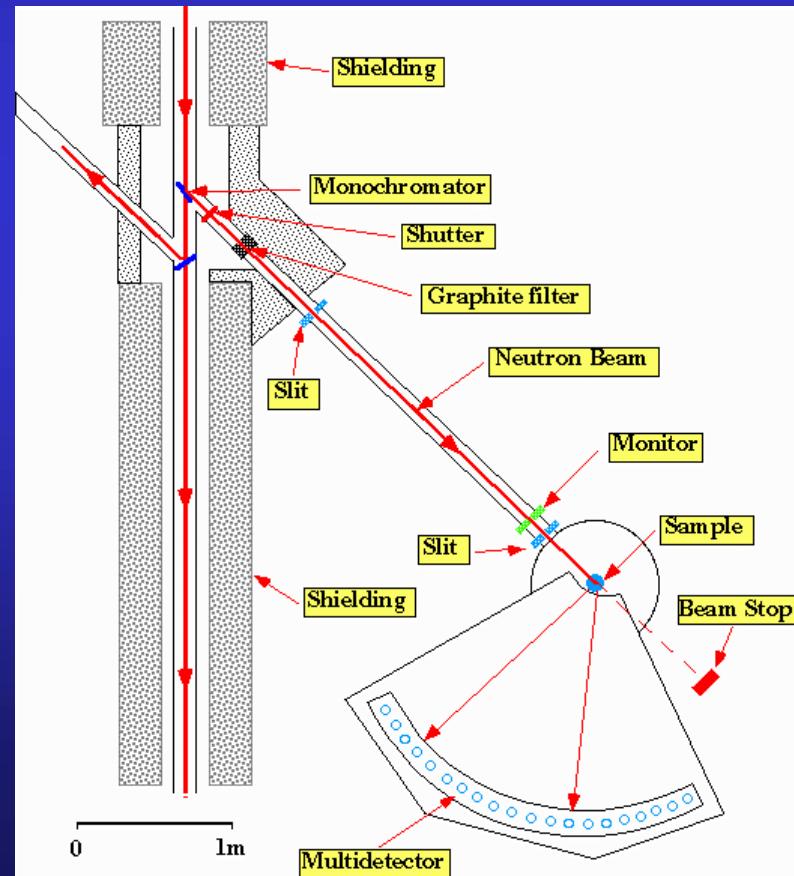
1D or 2D Detector + 4-circle diffractometer
(X-rays and neutrons)
CRISMAT, ILL

+

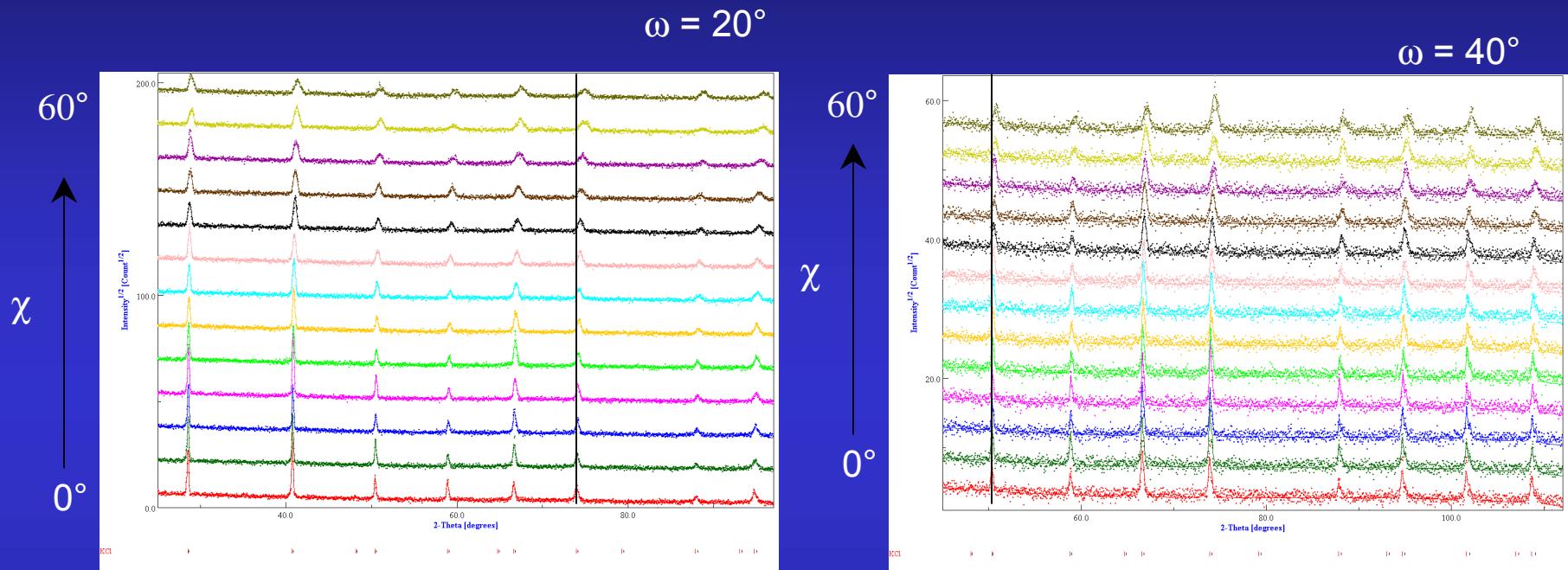
~1000 experiments (2θ diagrams)
in as many sample orientations

+

Instrument calibration
(peaks widths and shapes,
misalignments, defocusing ...)



Calibration

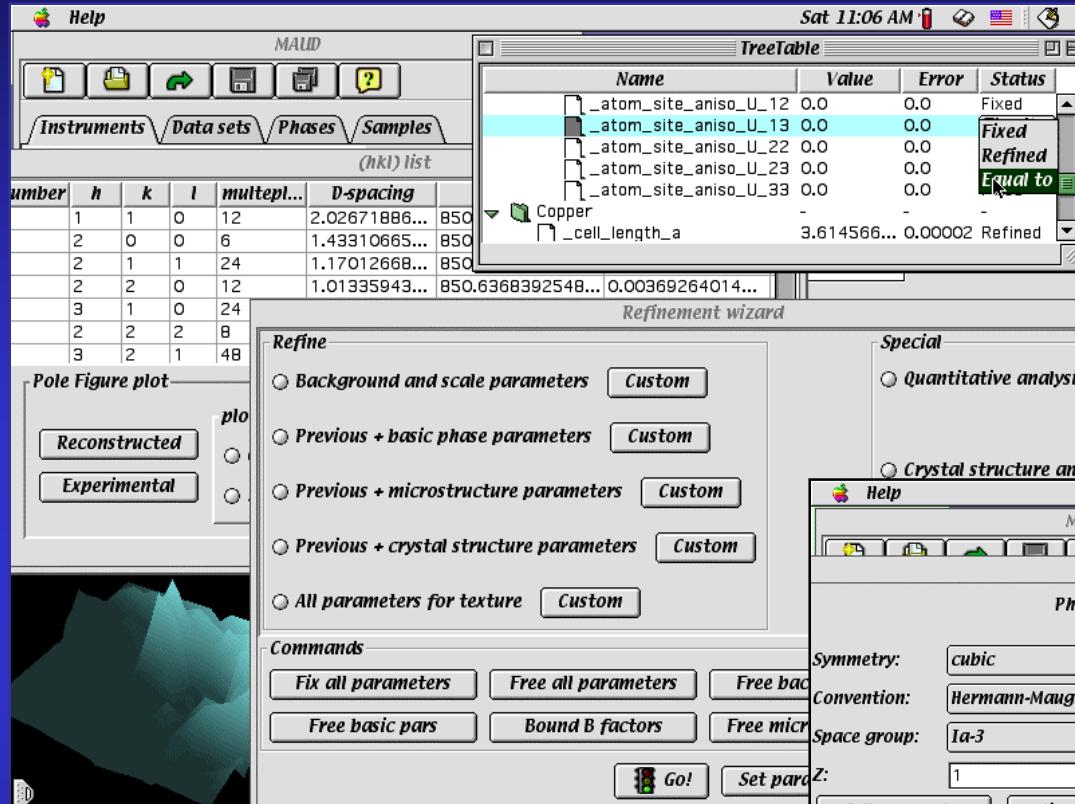


KCl, LaB₆ ...

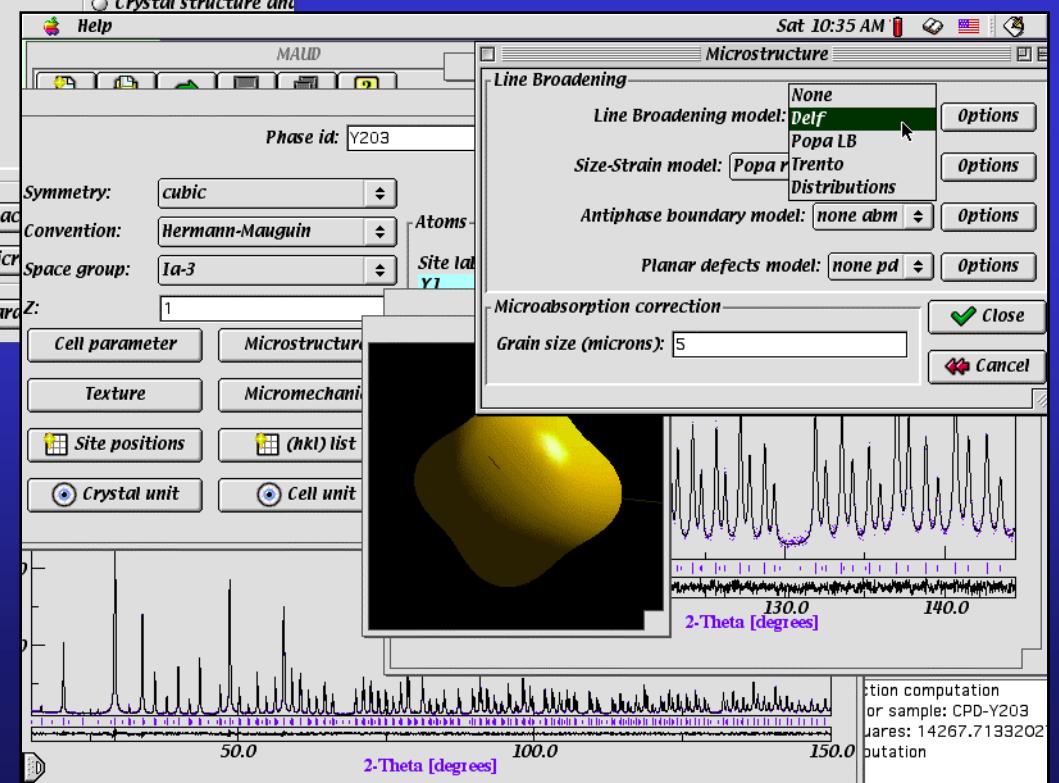


FWHM ($\omega, \chi, 2\theta \dots$)
2θ shift
gaussianity
asymmetry
misalignments ...

Methodology implementation



Java codes
Java web start updates

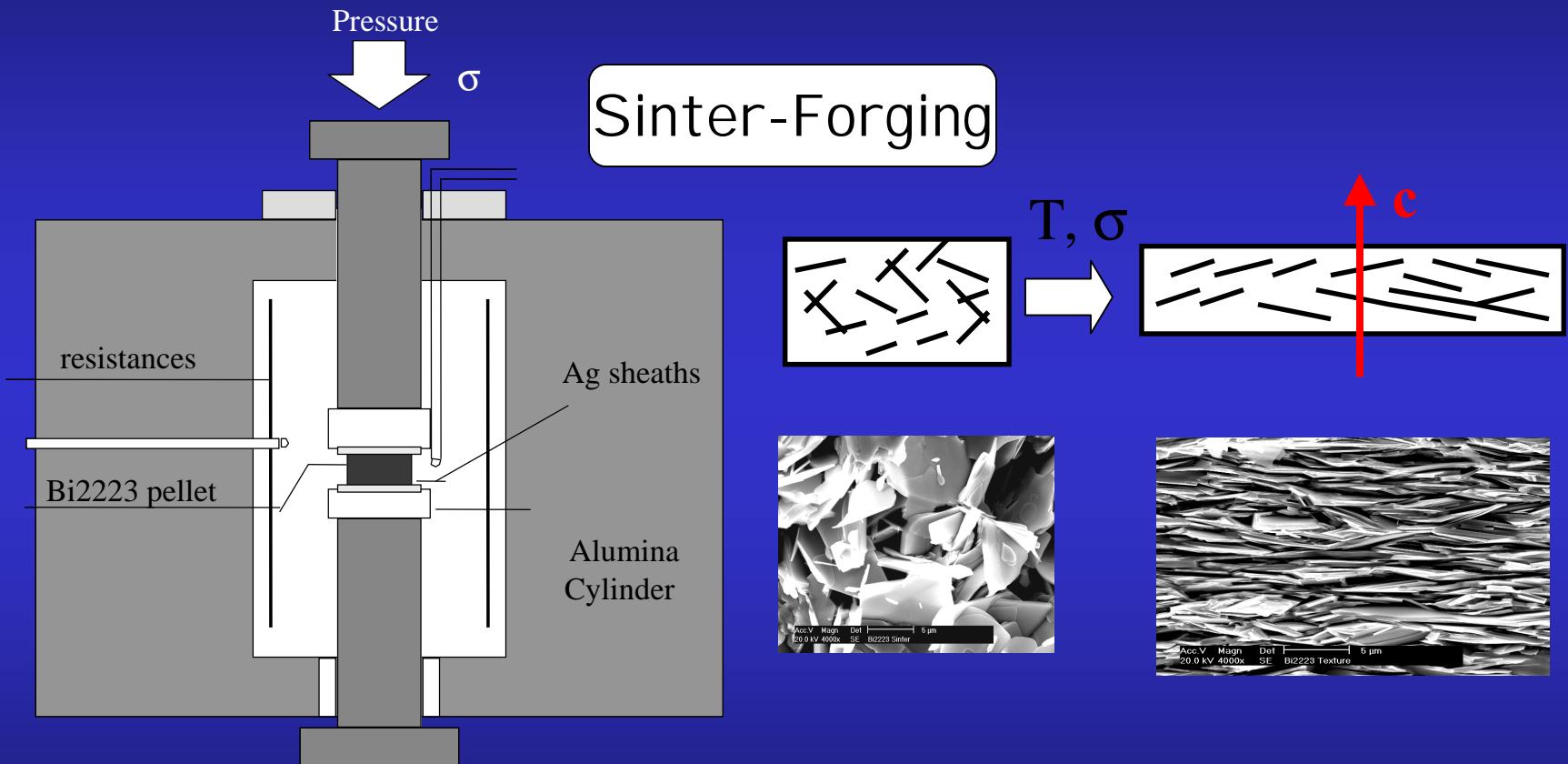


L. Lutterotti, Trento

User friendly interface

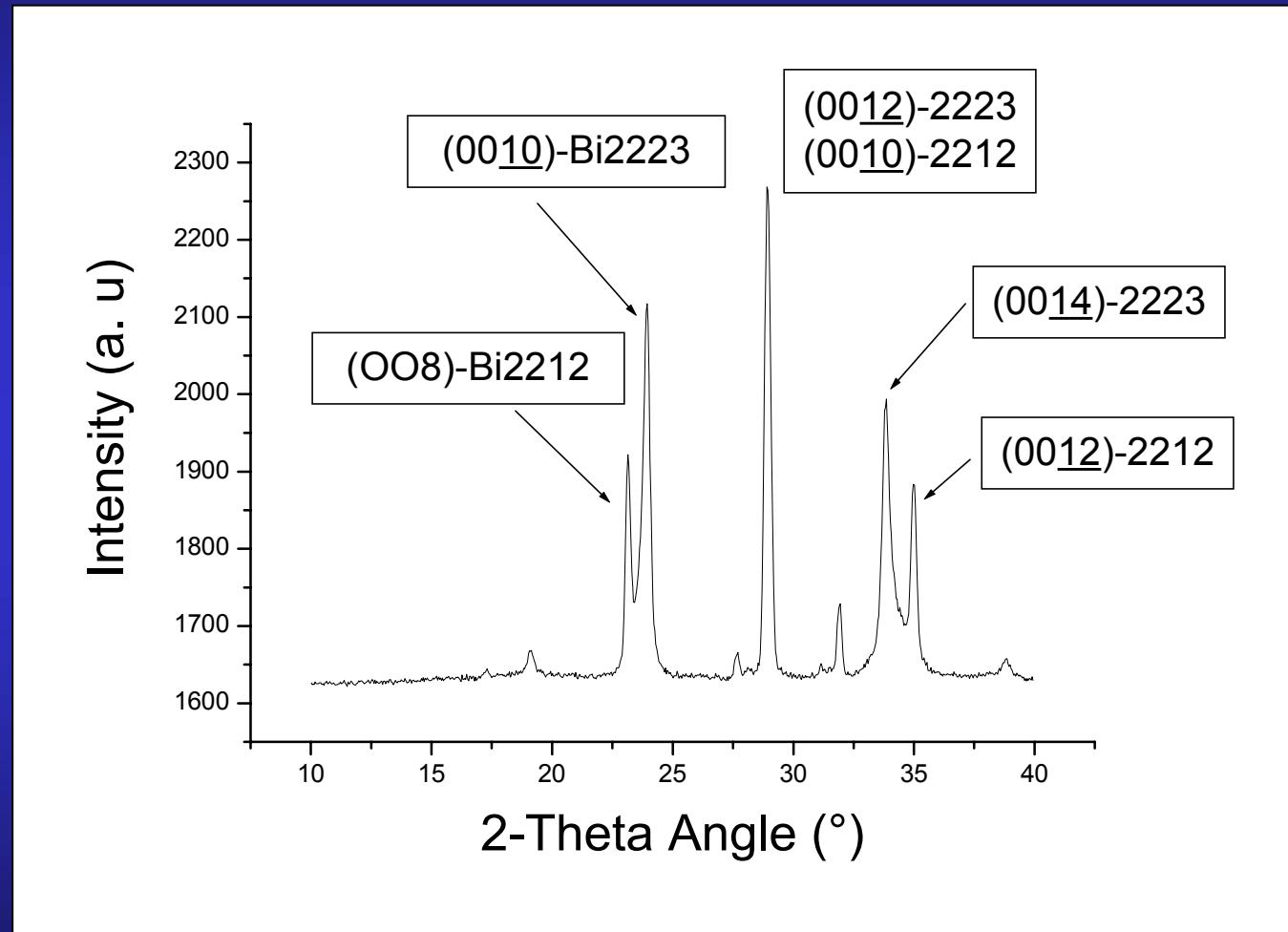
Bi2223 compounds

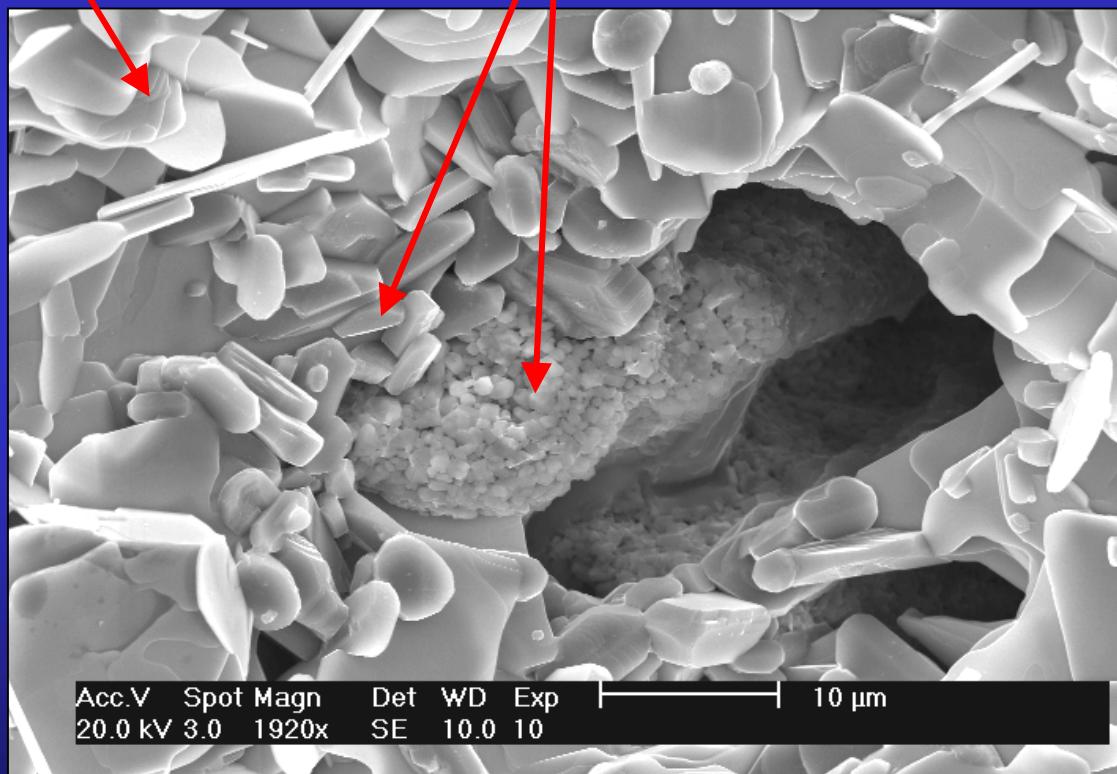
E. Guilmeau, PhD



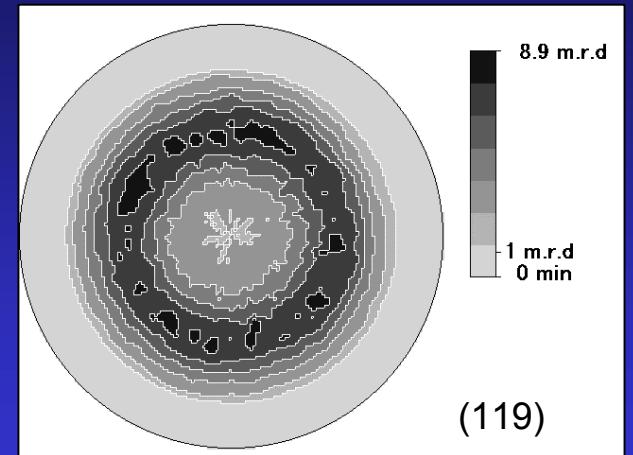
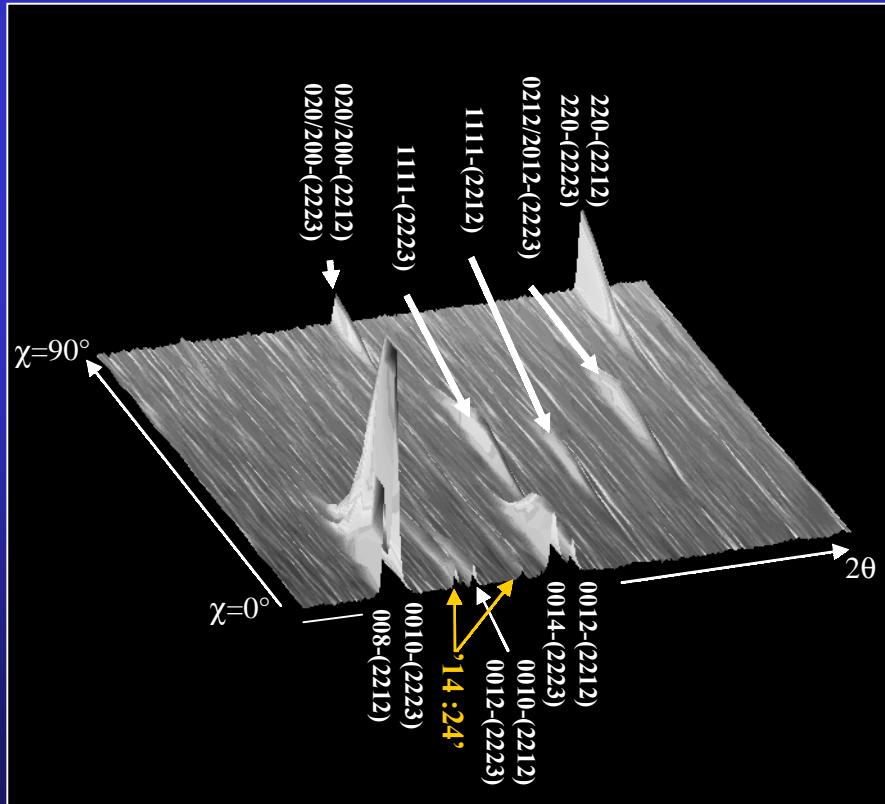
Grain alignment \Rightarrow $\nearrow J_c$

(00 ℓ) Texture

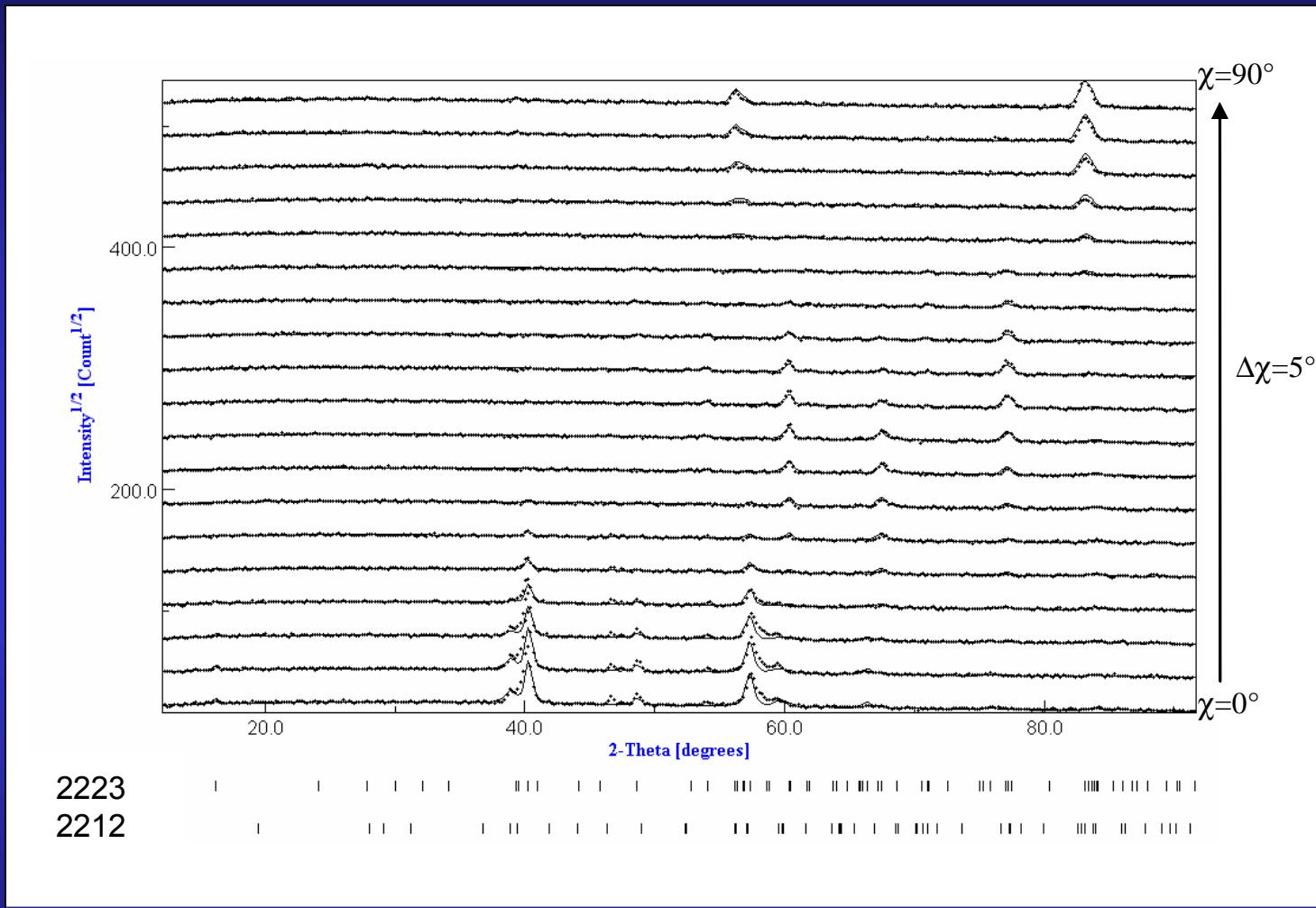




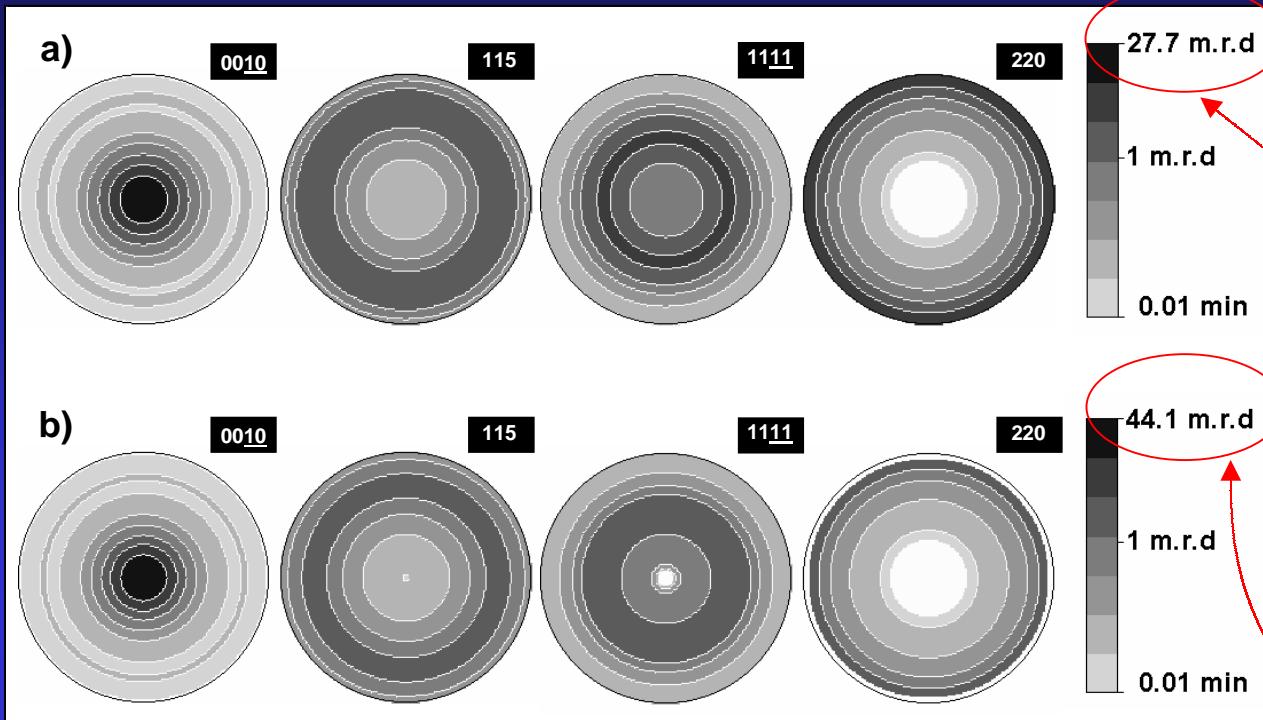
Combined Analysis



- Neutrons
- Sample: $\sim 70 \text{ mm}^3$
- 2θ patterns for $\chi=0^\circ$ to 90°
- No ϕ rotation (fibre texture).

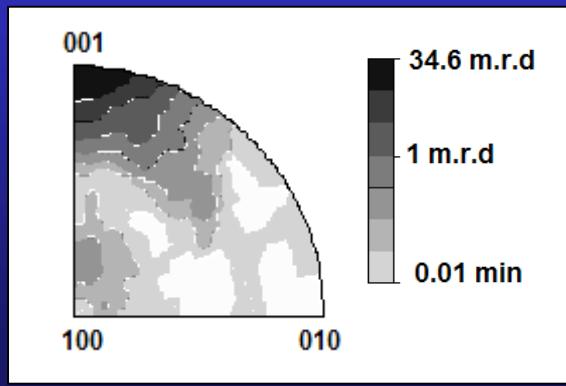


R_w=9.12
R_P=16.24



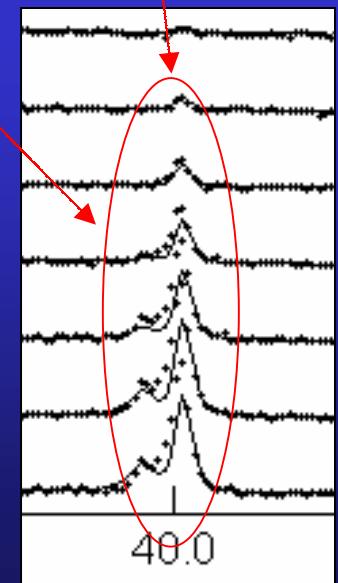
**Recalculated
(WIMV)**

**Extracted
(Le Bail)**



Stacking faults and/or intergrowth on the c-axis
→ New periodicities and peaks characterized with intermediate c parameters.

However, no algorithm is included to solve intergrowths in the combined approach.



Effect of the sinter-forging treatment on the texture development, crystal growth, transport properties

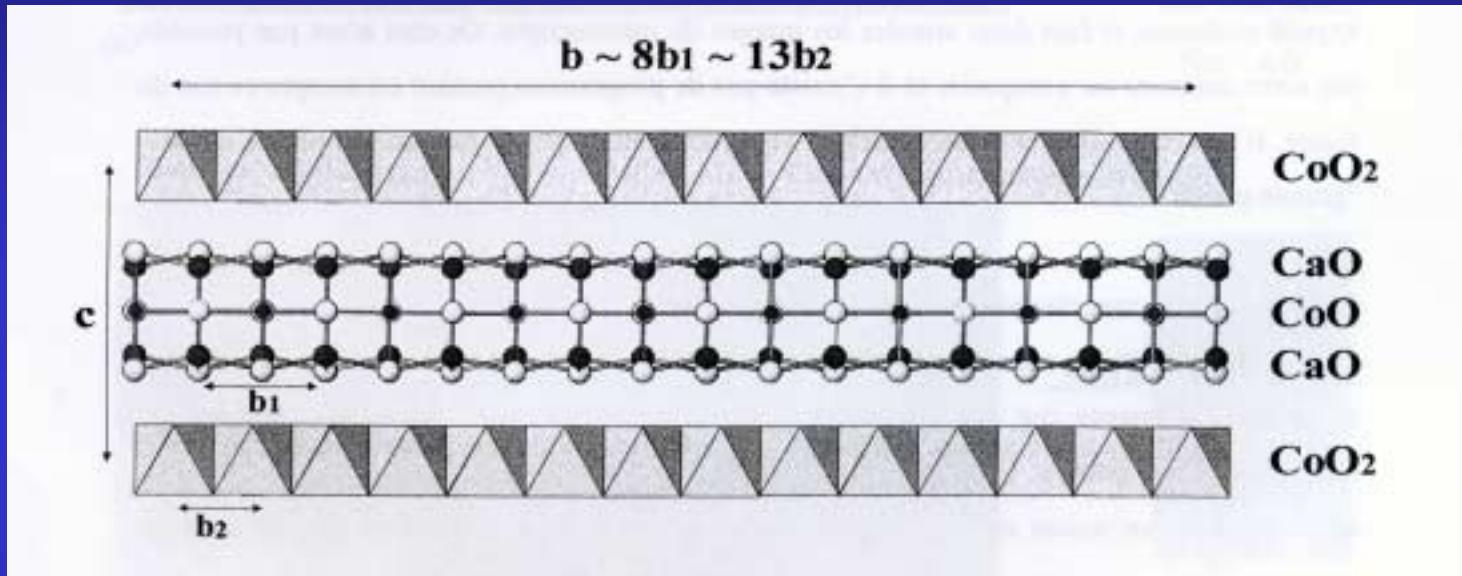
Sinter-forging dwell time (h)	Orientation Distribution		% Bi2223	Cell parameters (Å)		Crystallite size Bi2223 (nm)	Rb (%)	Rw (%)	Rexp (%)	RP0 (%)	RP1 (%)	J_c (A/cm²)	
	Max (m.r.d.)			Bi2212	Bi2223								
	Bi2212	Bi2223											
20	21.8	20.7	59.9±1.3	a=5.419(3) b=5.391(3) c=37.168(3)	a=5.414(3) b=5.393(3) c=30.800(3)	205±7	7.56	11.1	4.55	17.74	10.56	12500	
50	24.1	24.4	72.9±2.9	a=5.419(3) b=5.408(3) c=37.192(3)	a=5.416(3) b=5.396(3) c=30.806(3)	273±10	7.54	11.37	4.58	17.05	11.04	15000	
100	31.5	25.2	84.4±4.6	a=5.410(3) b=5.405(3) c=37.144(3)	a=5.412(3) b=5.403(3) c=30.752(3)	303±10	5.4	8.04	3.69	13.54	9.31	19000	
150	65.4	27.2	87.0±4.1	a=5.417(3) b=5.403(3) c=37.199(3)	a=5.413(3) b=5.407(3) c=30.792(3)	383±13	6.13	9.12	4.8	16.24	12.25	20000	



$Ca_3Co_4O_9$ thermoelectrics

J.G. Noudem, Caen

$Ca_3Co_4O_9$: Misfit lamellar and modulated Structure, with high thermopower

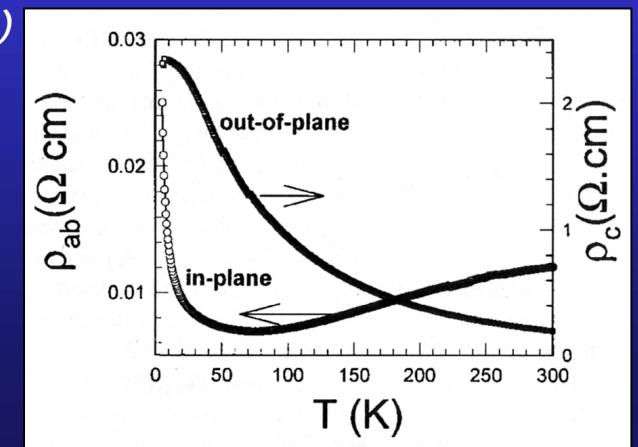


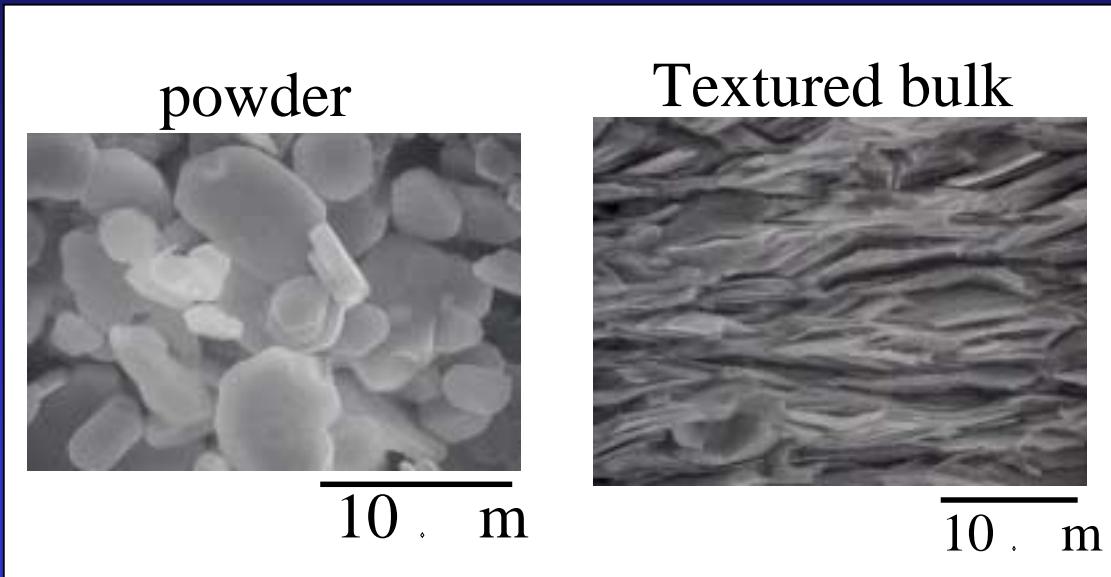
Two monoclinic sub-systems:

$S1$ with $a \sim 4.8\text{\AA}$, $b_1 \sim 4.5\text{\AA}$, $c \sim 10.8\text{\AA}$ et $\beta \sim 98^\circ$ (NaCl-type)

$S2$ with $a \sim 4.8\text{\AA}$, $b_2 \sim 2.8\text{\AA}$, $c \sim 10.8\text{\AA}$ et $\beta \sim 98^\circ$ (CdI_2 -type)

$$\Gamma = \sigma_{ab}/\sigma_c \sim 10 \quad \xrightarrow{\text{Texture}}$$

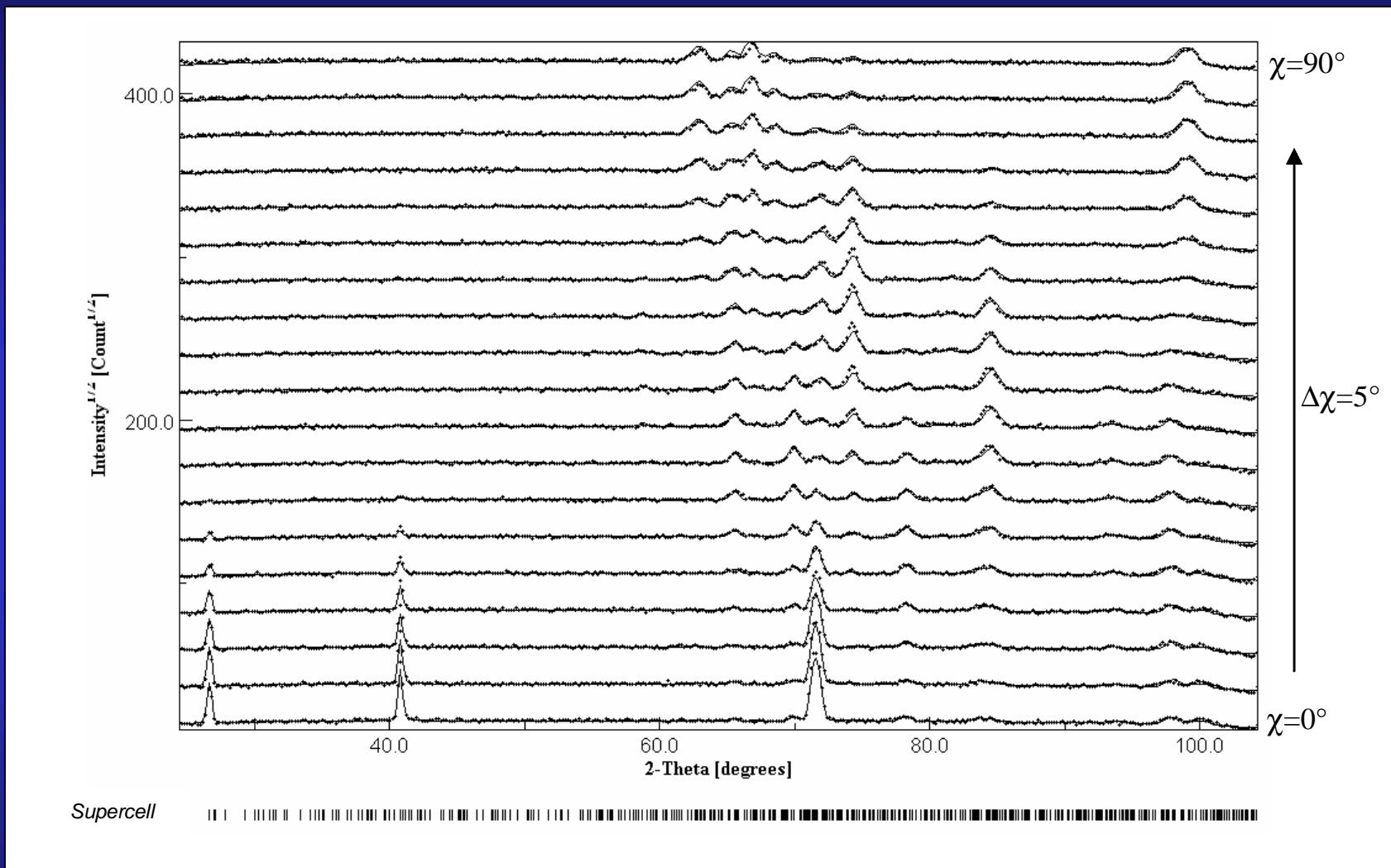




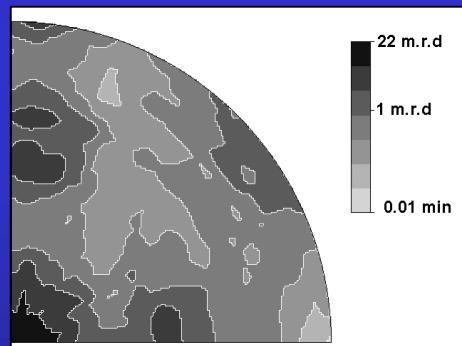
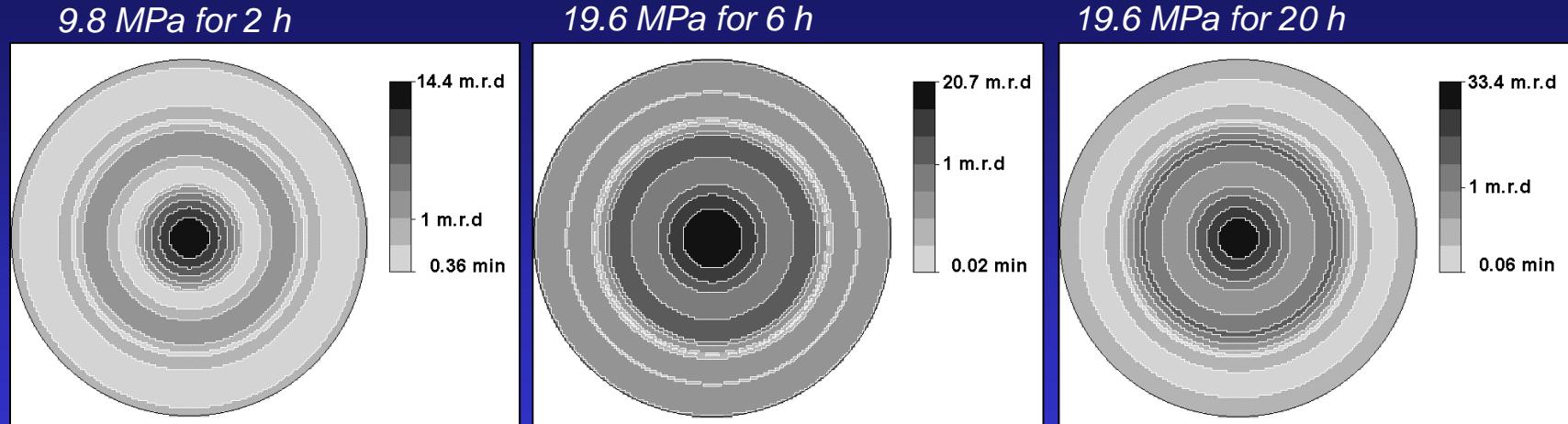
*Magnetic alignment
and
Templated Growth
method*

Analysis:

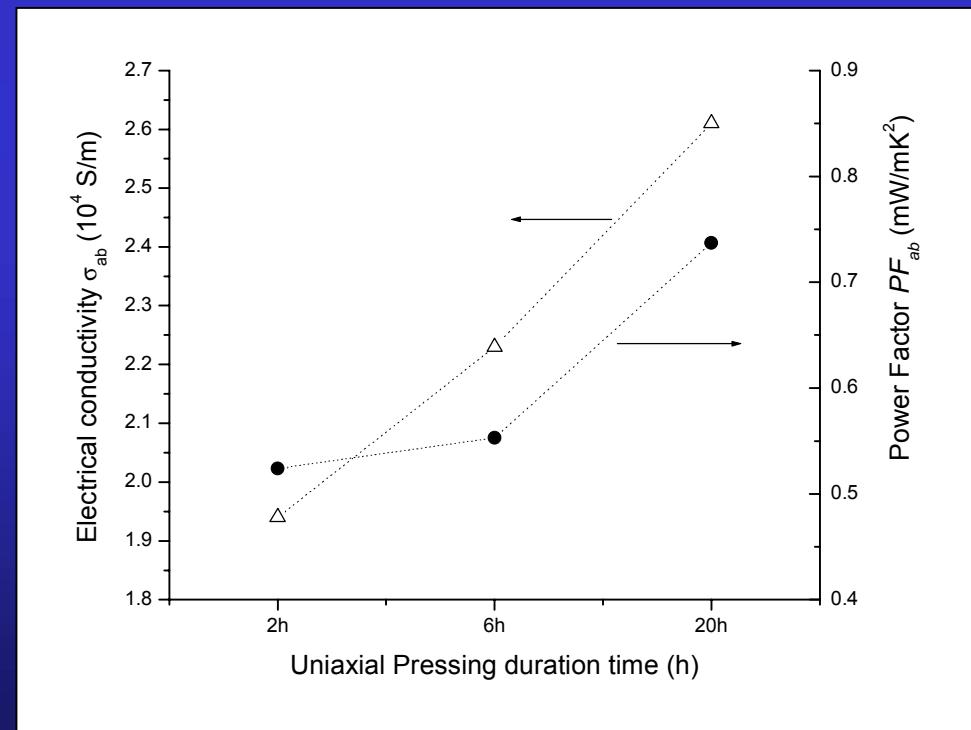
- *neutrons*
- *3D Supercell: $a=4.8309\text{\AA}$, $b\sim8b_1\sim13b_2\sim36.4902\text{\AA}$, $c=10.8353\text{\AA}$, $\beta=98.13^\circ$*
- 174 atoms/cell*
- Sample : 0.6 cm^3*



RP=19.7%, Rw=11.9%

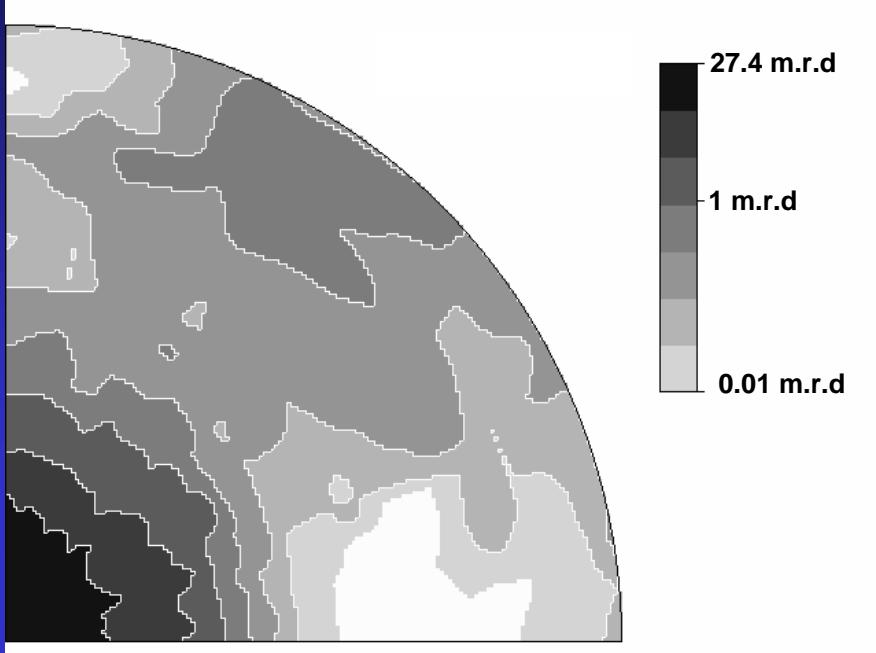


Templated Growth Method



Magnetic Alignment

Logarithmic density scale, equal area projection



- *magnetic alignment really efficient to obtain strong textures*
- *combined analysis of modulated structures possible*

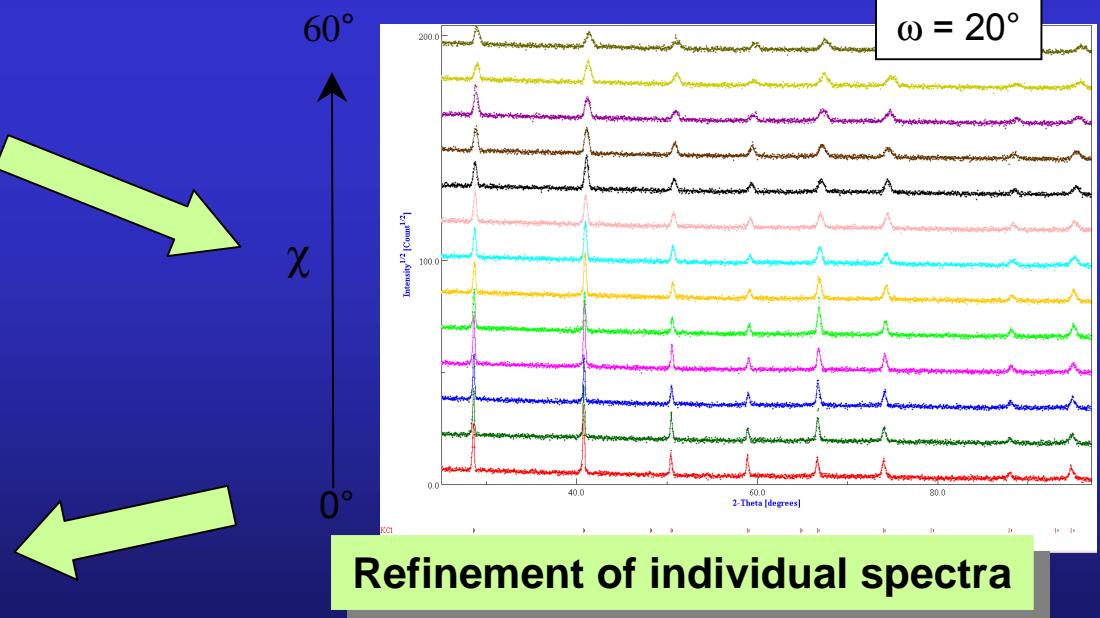
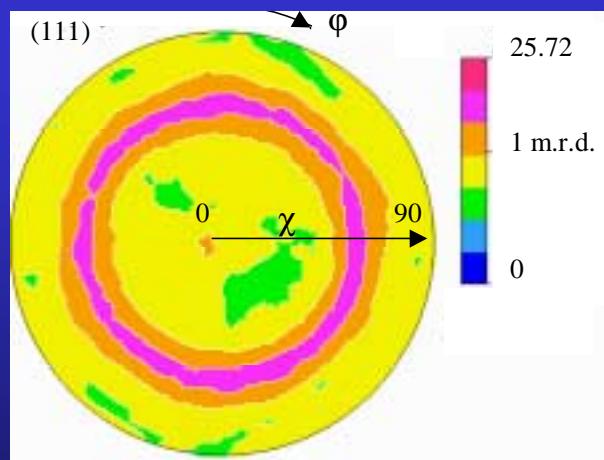
Ferroelectric PCT films

J. Ricote, Madrid

thin films:

$(\text{Ca}_{0.24}\text{Pb}_{0.76})\text{TiO}_3$ sol-gel synthesised solutions deposited by spin coating on a substrate of Pt/TiO₂/Si, with and without a treatment at 650°C for 30 min.

All films are crystallised at 700°C for 50 s by Rapid Thermal Processing (RTP; 30°C/s). A series is also recrystallised at 650°C for 1 to 3 h.



Limitations of the simple Quantitative Texture Analysis

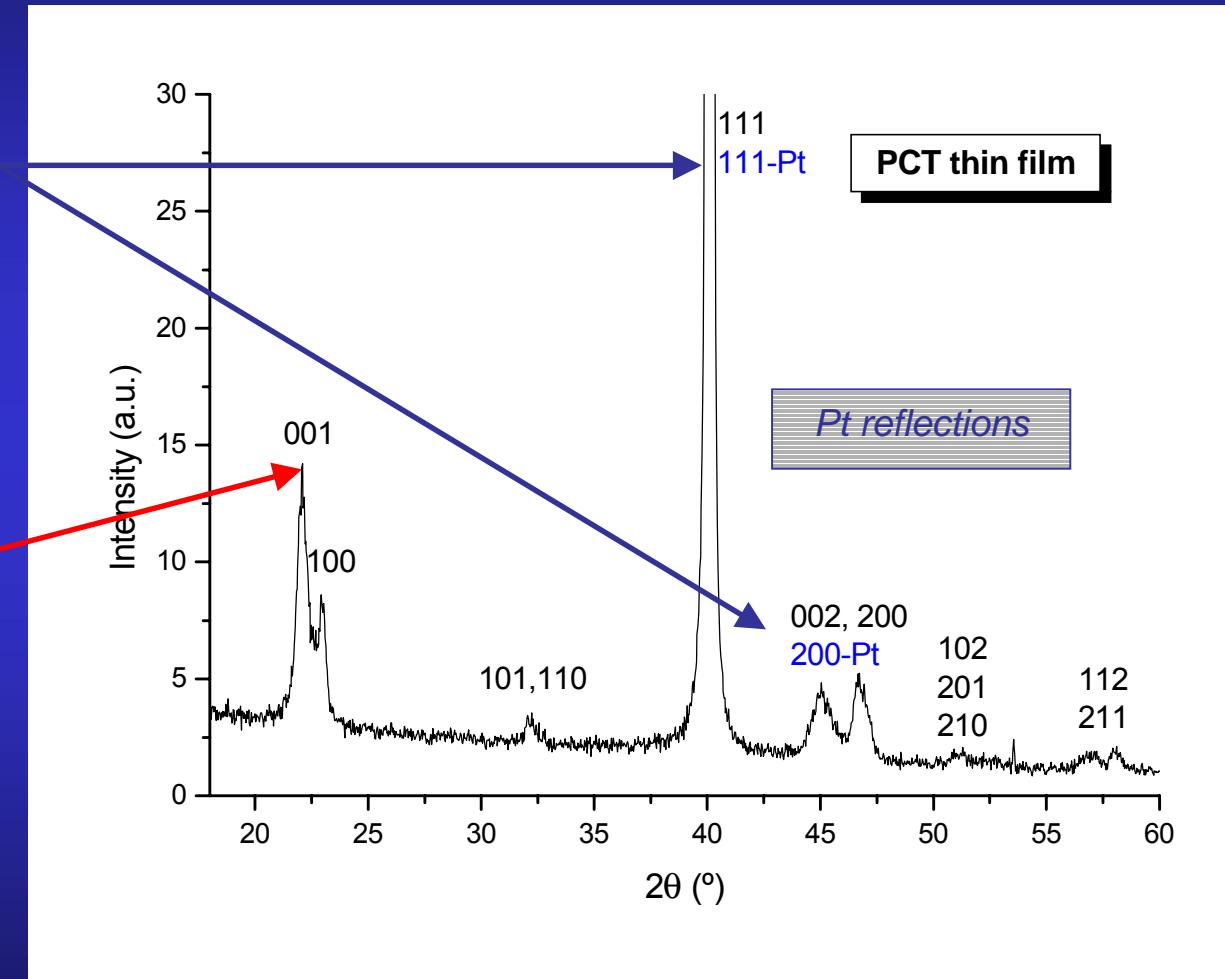
Structural parameters are difficult to obtain due to:

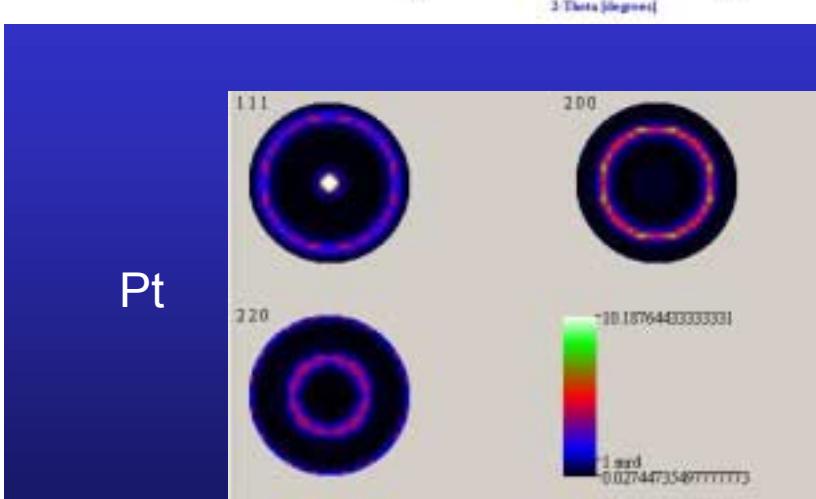
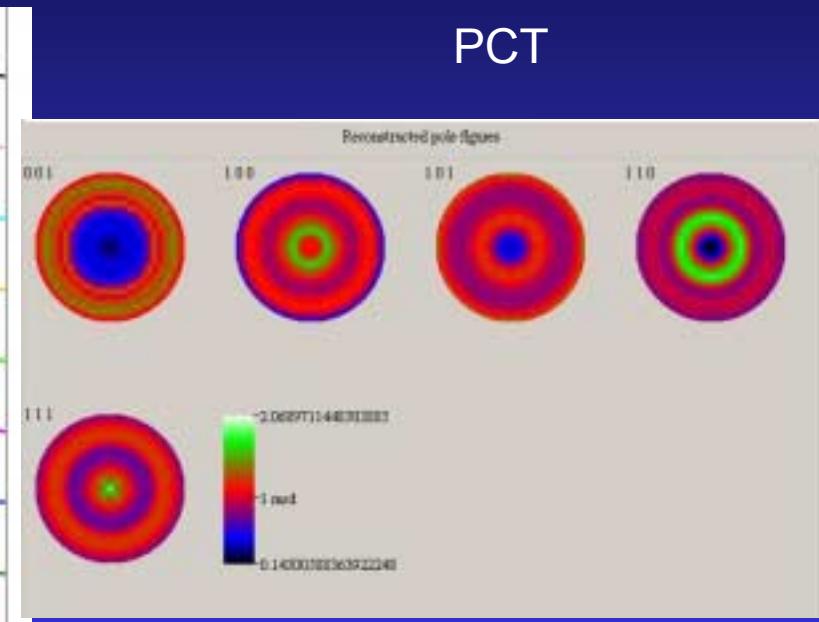
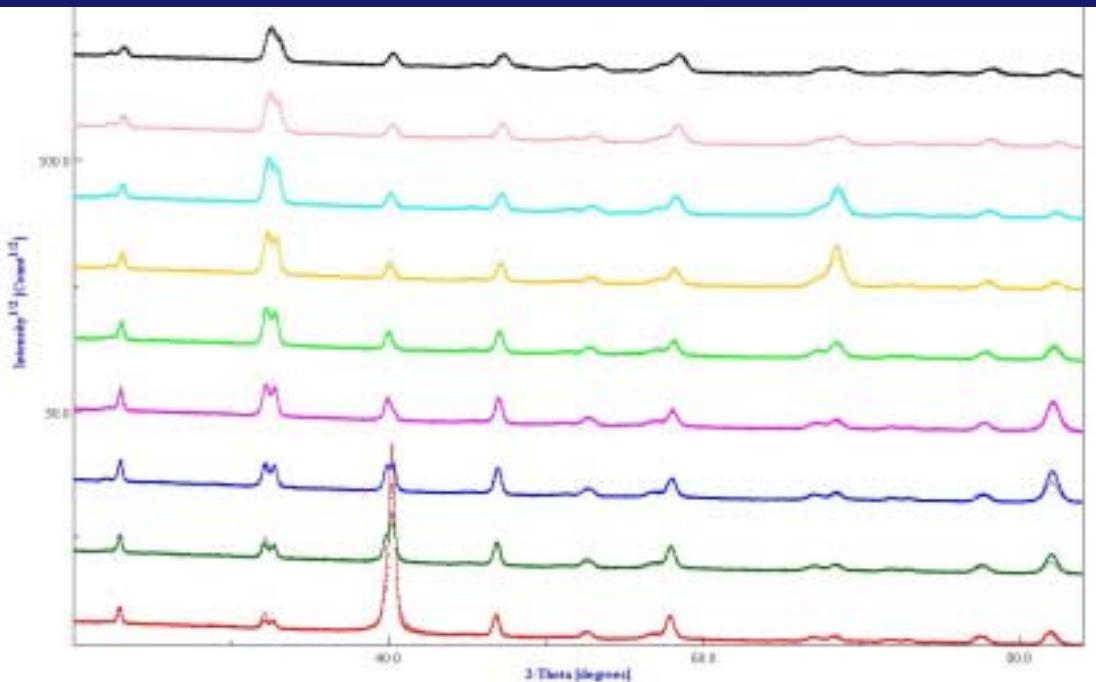
Substrate influence:

overlapping of reflections from the film and the substrate

TEXTURE effects:

peaks that do not appear at low χ angles



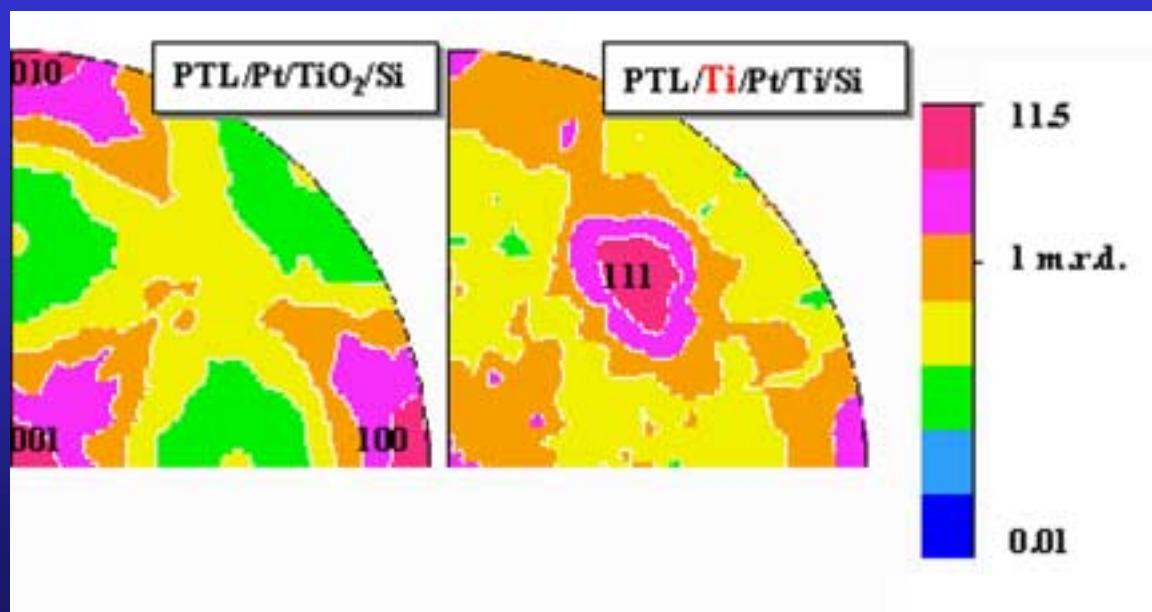


$a = 3.9108(1)$ Å
 $T = 457(3)$ Å
 $t_{\text{iso}} = 458(3)$ Å
 $\varepsilon' = 0.0032(1)$ rms

$a = 3.9156(1)$ Å
 $c = 4.0497(3)$ Å
 $T = 2525(13)$ Å
 $t_{\text{iso}} = 390(7)$ Å
 $\varepsilon' = 0.0067(1)$ rms

$R_W = 13\%$; $R_B = 12\%$; $R_{\text{exp}} = 22\%$. (Rietveld)
 $R_W = 5\%$; $R_B = 6\%$ (E-WIMV)

Atom	Occupancy	x	y	z
Pb	0.76	0.0	0.0	0.0
Ca	0.24	0.0	0.0	0.0
Ti	1.0	0.5	0.5	0.477(2)
O1	1.0	0.5	0.5	0.060(2)
O2	1.0	0.0	0.5	0.631(1)



Structural parameters

Pt layer

	a (Å)	thickness (nm)	R factors (%)
non-treated substrate			
Pt	3.9108(1)	45.7(3)	$R_w=13, R_B=12, R_{exp}=22$
annealed substrate			
Pt	3.9100(4)	46.4(3)	$R_w=8, R_B=14, R_{exp}=21$
Pt (Recryst. 1h)	3.9114(2)	47.8(3)	$R_w=9, R_B=20, R_{exp}=21$
Pt (Recryst. 2h)	3.9068(1)	46.9(3)	$R_w=9, R_B=14, R_{exp}=22$
Pt (Recryst. 3h)	3.9141(4)	47.5(9)	$R_w=27, R_B=12, R_{exp}=21$

Annealing of the substrate does not introduce significant variations on the structure of the Pt layer

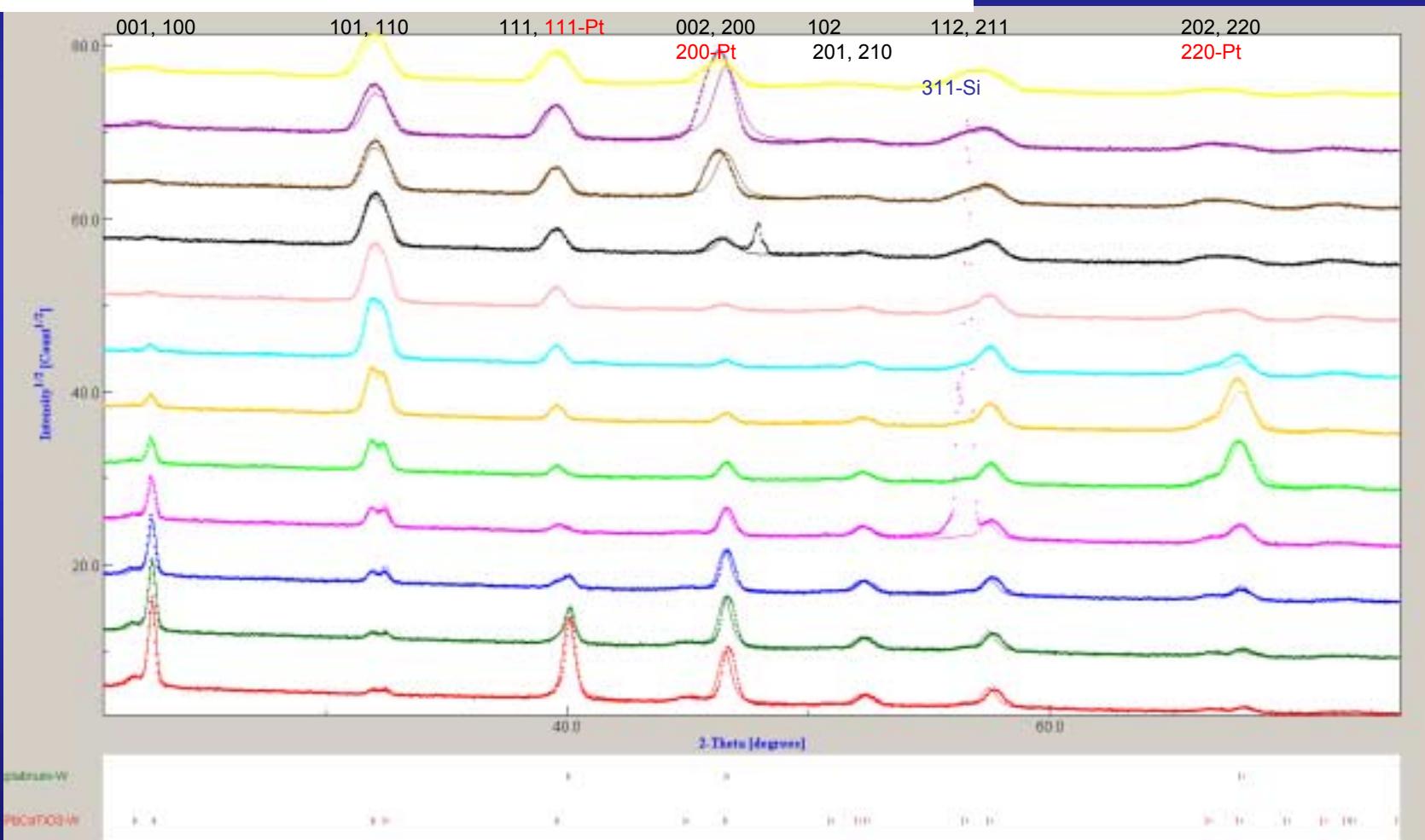
PTC film

	a (Å)	c (Å)	thickness (nm)
on non-treated substrate			
PCT	3.9156(1)	4.0497(6)	272.5(13)
on annealed substrate			
PCT	3.8920(6)	4.0187(8)	279.0(9)
PCT (Recryst. 1h)	3.8929(2)	4.0230(4)	266.1(11)
PCT (Recryst. 2h)	3.8982(2)	4.0227(4)	258.4(9)
PCT (Recryst. 3h)	3.9001(4)	4.0228(11)	253.6(29)

Recrystallisation reduces the stress on the film, and, increases the lattice parameters

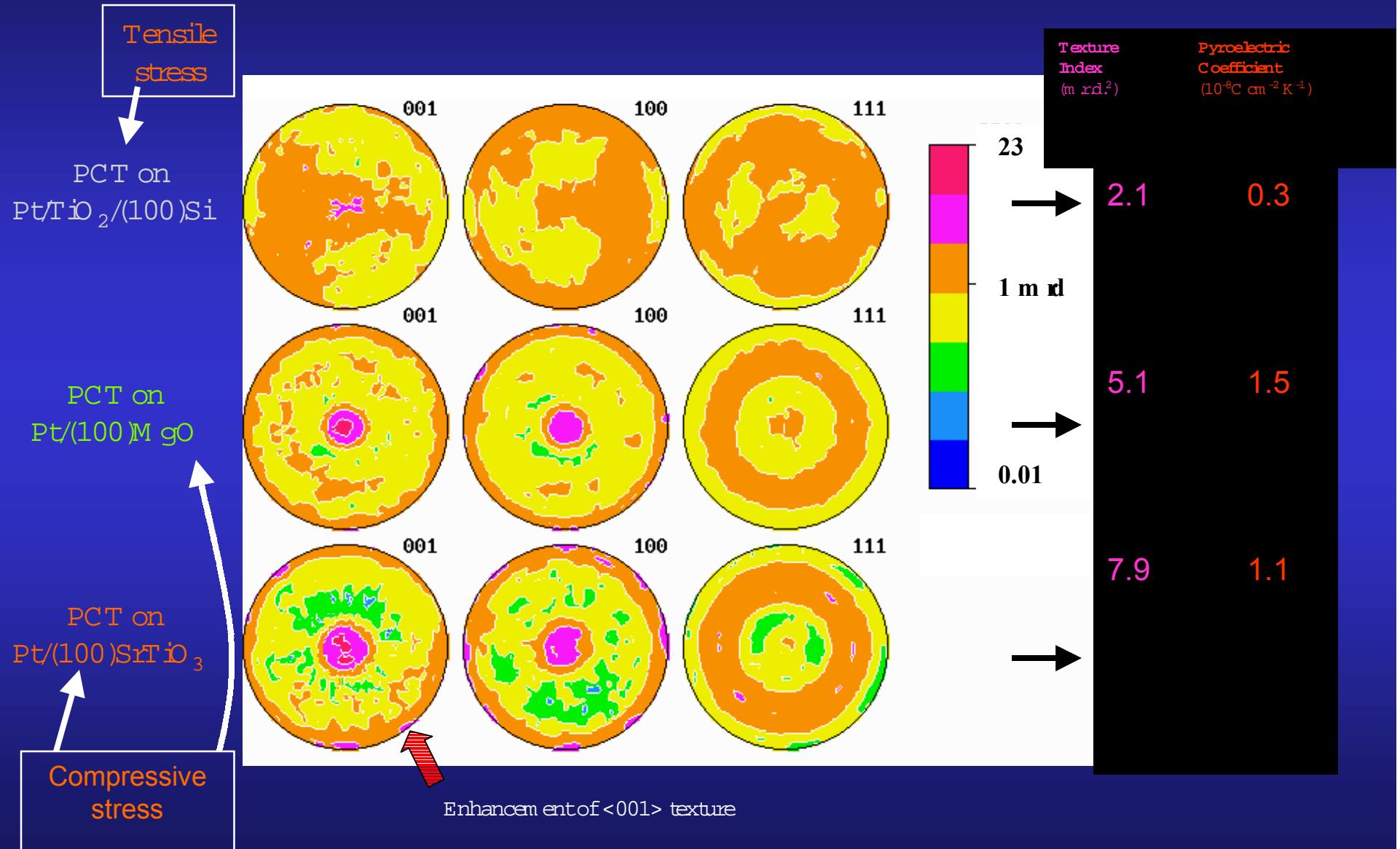
Structural, microstructural and texture quantitative characterisation of ferroelectric thin films by the combined method

Analysis of the X-ray diffraction diagrams of a PCT film on Pt/TiO₂/Si



$R_w = 13\%$; $R_B = 12\%$; $R_{exp} = 22\%$. (Rietveld)
 $R_w = 5\%$; $R_B = 6\%$ (E-WIMV)

Substrate influence on Residual Stress and Texture



Compliance coefficients [10^{-3} GPa $^{-1}$]	PbTiO ₃ single crystal (data set A)	Film random orientation	PCT-Si <001> contrib. \approx 17%	PLT <001> contrib. \approx 49%	PCT-Mg <001> contrib. \approx 68%
s ₁₁	6.5	10.1	10.5	10.0	9.7
s ₂₂	6.5	10.0	10.5	10.0	9.7
s ₃₃	33.3	9.8	9.0	10.3	11.3
s ₄₄	14.5	13.2	12.8	12.9	13.1
s ₅₅	14.5	13.2	12.8	13.0	13.1
s ₆₆	9.6	13.4	14.0	13.5	12.7
s ₁₂	-0.35	-3.3	-3.5	-3.2	-3.0
s ₂₁	-0.35	-3.3	-3.5	-3.2	-3.0
s ₁₃	-7.1	-3.2	-3.1	-3.4	-3.6
s ₃₁	-7.1	-3.2	-3.1	-3.4	-3.6
s ₂₃	-7.1	-3.2	-3.1	-3.4	-3.6
s ₃₂	-7.1	-3.2	-3.1	-3.4	-3.6
s ₃₃ /s ₁₁	5.1	0.97	0.86	1.03	1.16
s ₁₃ /s ₁₂	20.3	0.97	0.89	1.06	1.20

Geometric mean average + biaxial stress state

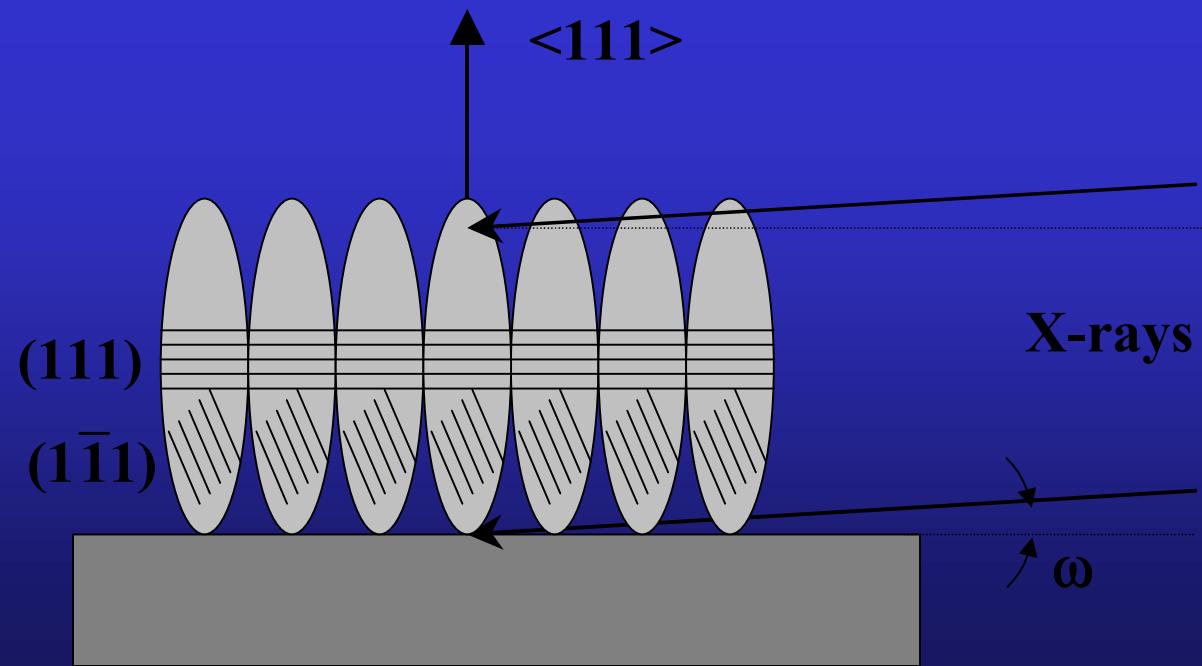
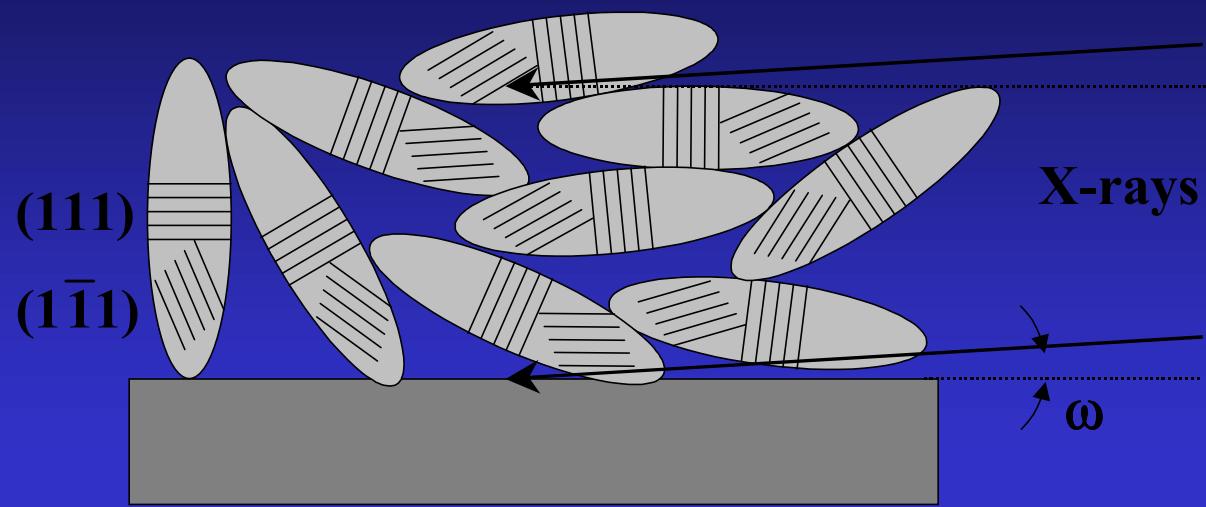
Si nanocrystalline thin films

M. Morales, Caen

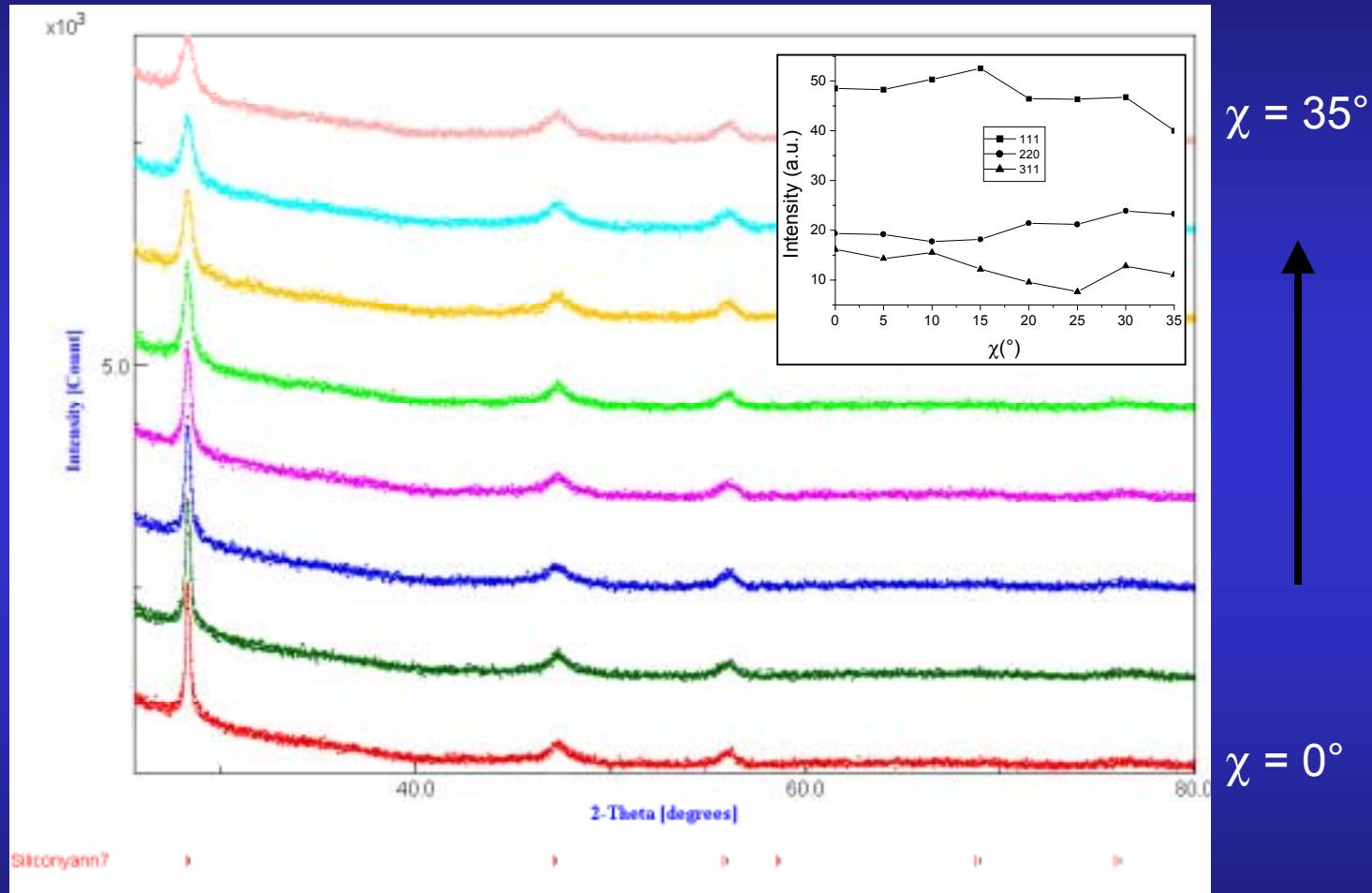
Silicon thin films deposition by reactive magnetron sputtering:

- ↳ power density 2W/cm²
- ↳ total pressure: $p_{\text{total}} = 10^{-1}$ Torr
- ↳ plasma mixture: H₂ / Ar, pH₂ / p_{total} = 80 %
- ↳ temperature: 200°C
- ↳ substrates: amorphous SiO₂ (a-SiO₂)
(100)-Si single-crystals
- ↳ target-substrate distance (d)
 - a-SiO₂ substrates: d = 4, 6, 7, 8, 10, 12 cm
films A, B, C, D, E, F
 - (100)-Si: d = 6, 12 cm
films G, H

Aim: quantum confinement, photoluminescence properties



Typical refinement

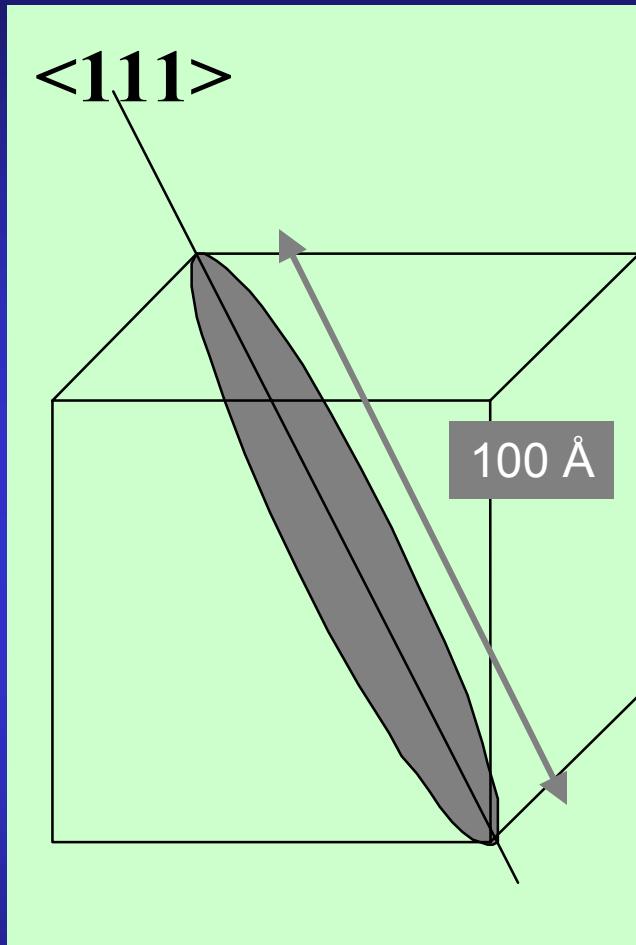


broad, anisotropic diffracted lines, textured samples

Refinement Results

Sample	d (cm)	a (Å)	RX thickness (nm)	Anisotropic sizes (Å)			Texture parameters			Reliability factors (%)			
				<111>	<220>	<311>	Maximum (m.r.d.)	minimum (m.r.d.)	Texture index F ² (m.r.d ²)	R _{P0}	R _w	R _B	R _{exp}
A	4	5.4466 (3)	—	94	20	27	1.95	0.4	1.12	1.72	4.0	3.7	3.5
B	6	5.4439 (2)	711 (50)	101	20	22	1.39	0.79	1.01	0.71	4.9	4.3	4.2
C	7	5.4346 (4)	519 (60)	99	40	52	1.72	0.66	1.05	0.78	4.3	4.0	3.9
D	8	5.4461 (2)	1447 (66)	100	22	33	1.57	0.63	1.04	0.90	5.5	4.6	4.5
E	10	5.4462 (2)	1360 (80)	98	20	25	1.22	0.82	1.01	0.56	5.0	3.9	4.0
F	12	5.4452 (3)	1110 (57)	85	22	26	1.59	0.45	1.05	1.08	4.2	3.5	3.7
G	6	5.4387 (3)	1307 (50)	89	22	28	1.84	0.71	1.01	1.57	5.2	4.7	4.2
H	12	5.4434 (2)	1214 (18)	88	22	24	2.77	0.50	1.12	2.97	5.0	4.5	4.3

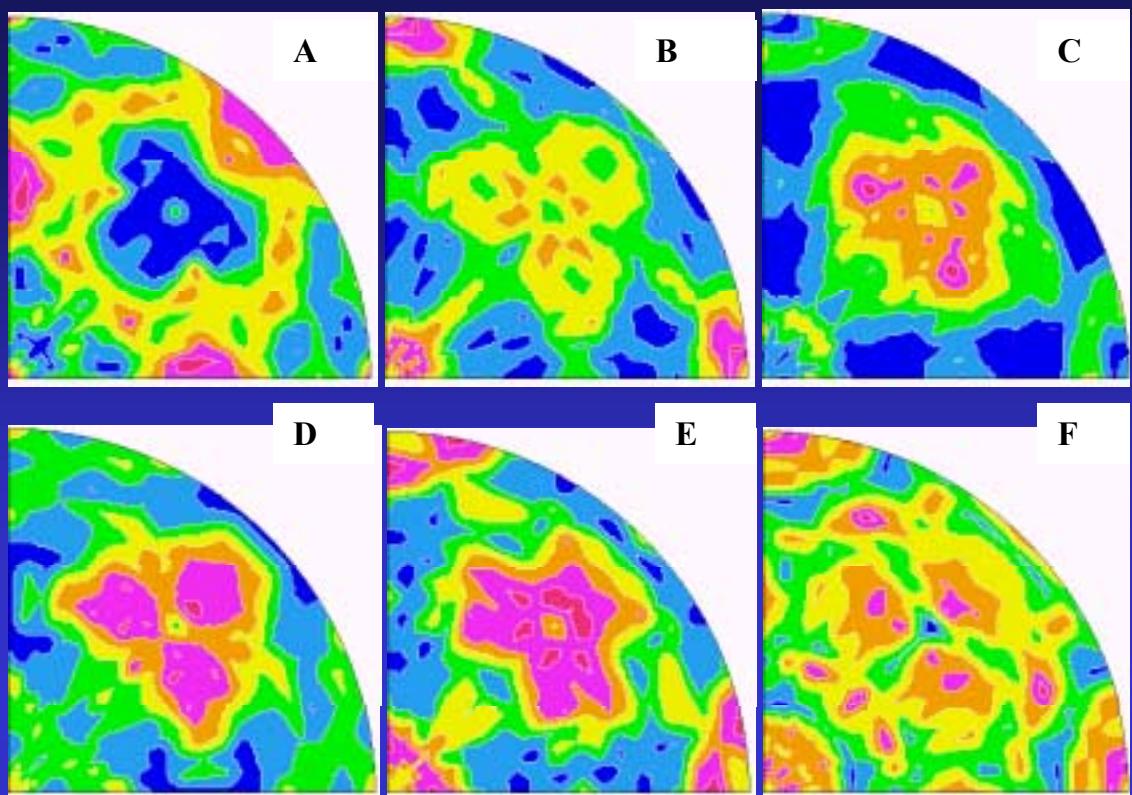
Mean anisotropic shape



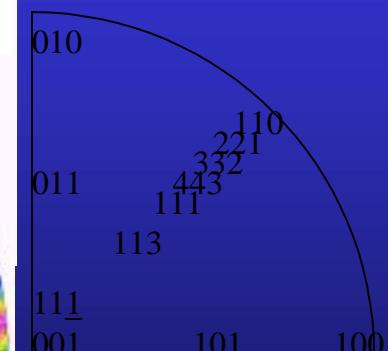
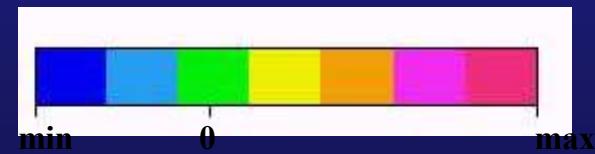
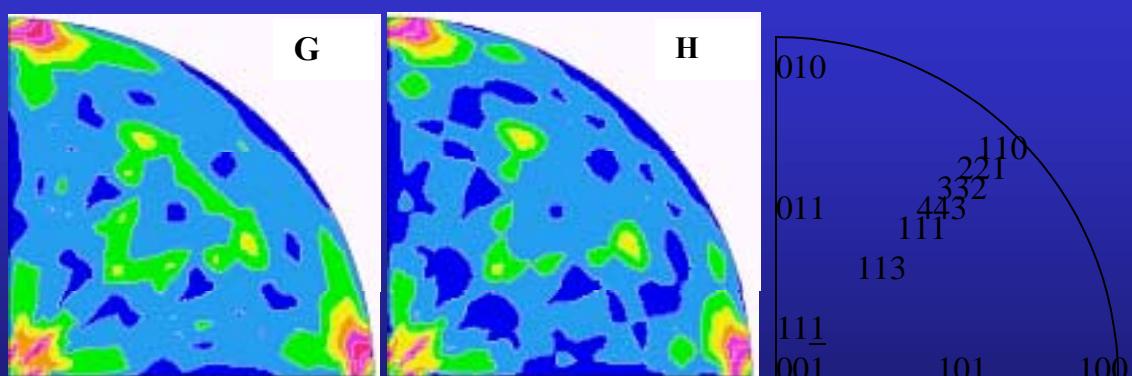
Schematic of the mean crystallite shape for Sample D represented in a cubic cell, as refined using the Popa approach and exhibiting a strong elongation along <111> (see Table).

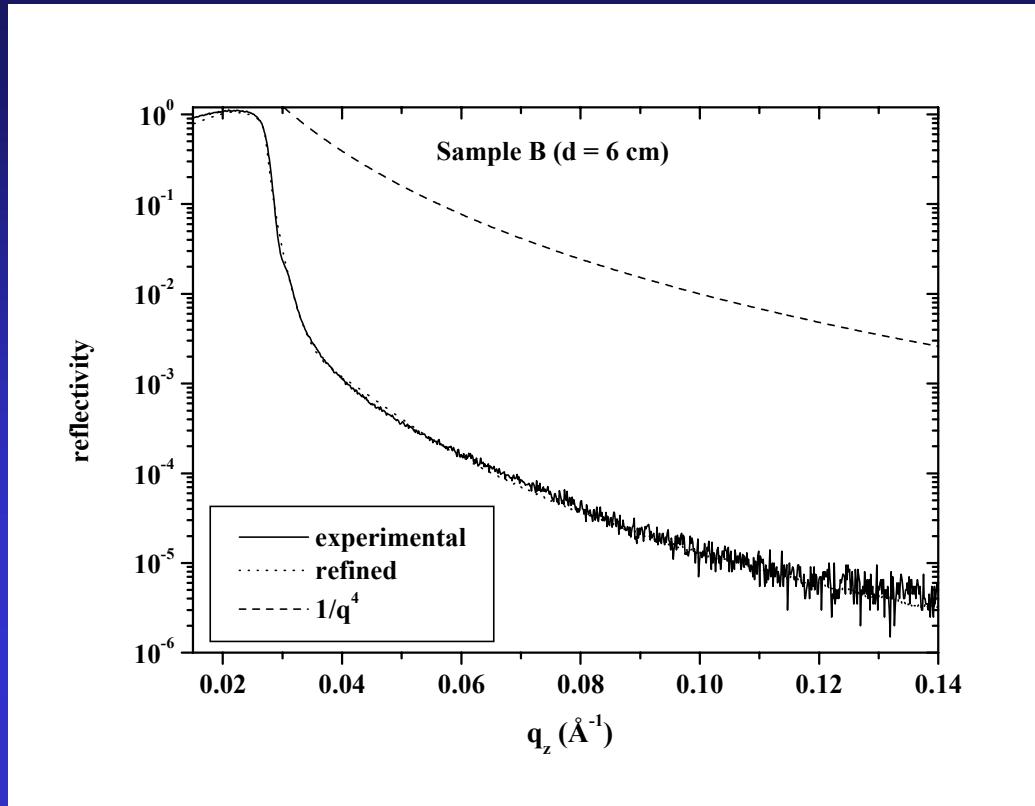
001 Inverse Pole Figures

a-SiO₂



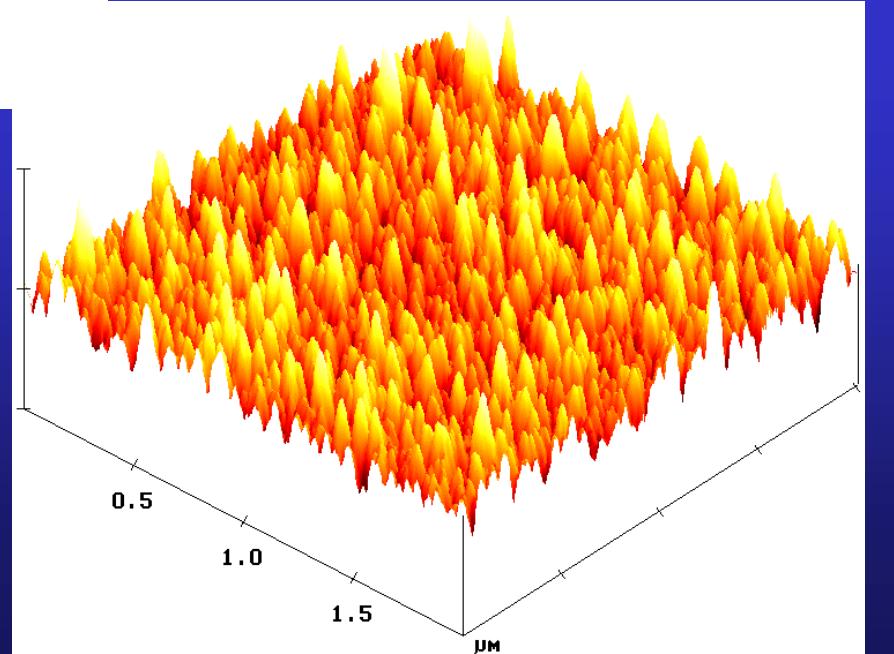
(100)-Si

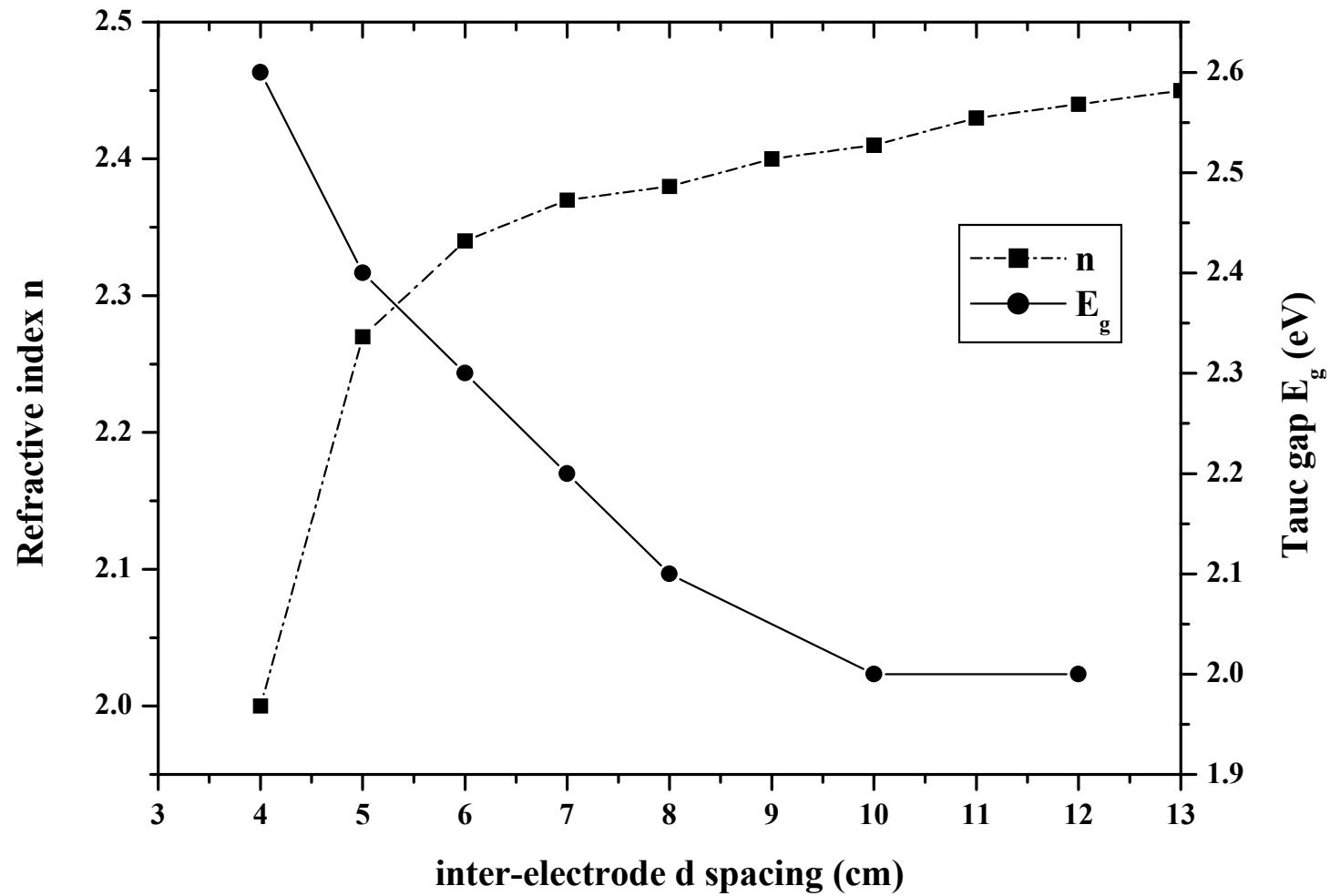




XRR:
Roughness
governed

AFM:
homogeneous
roughness

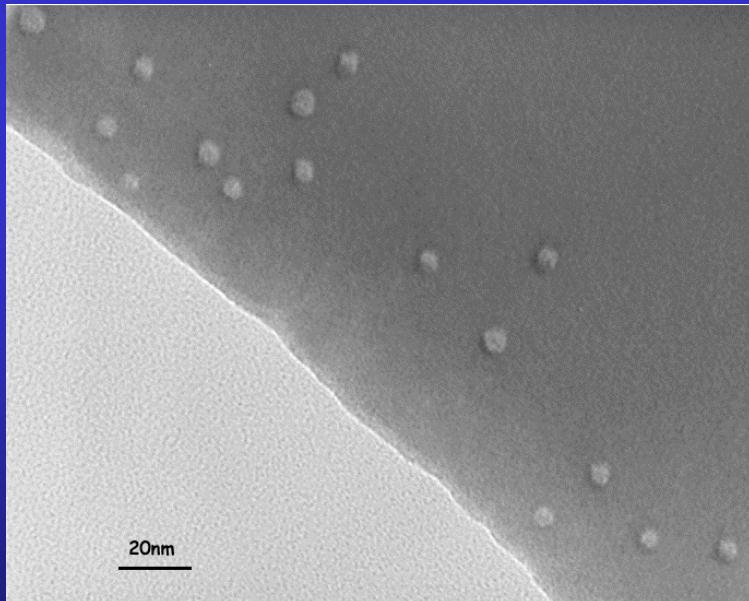




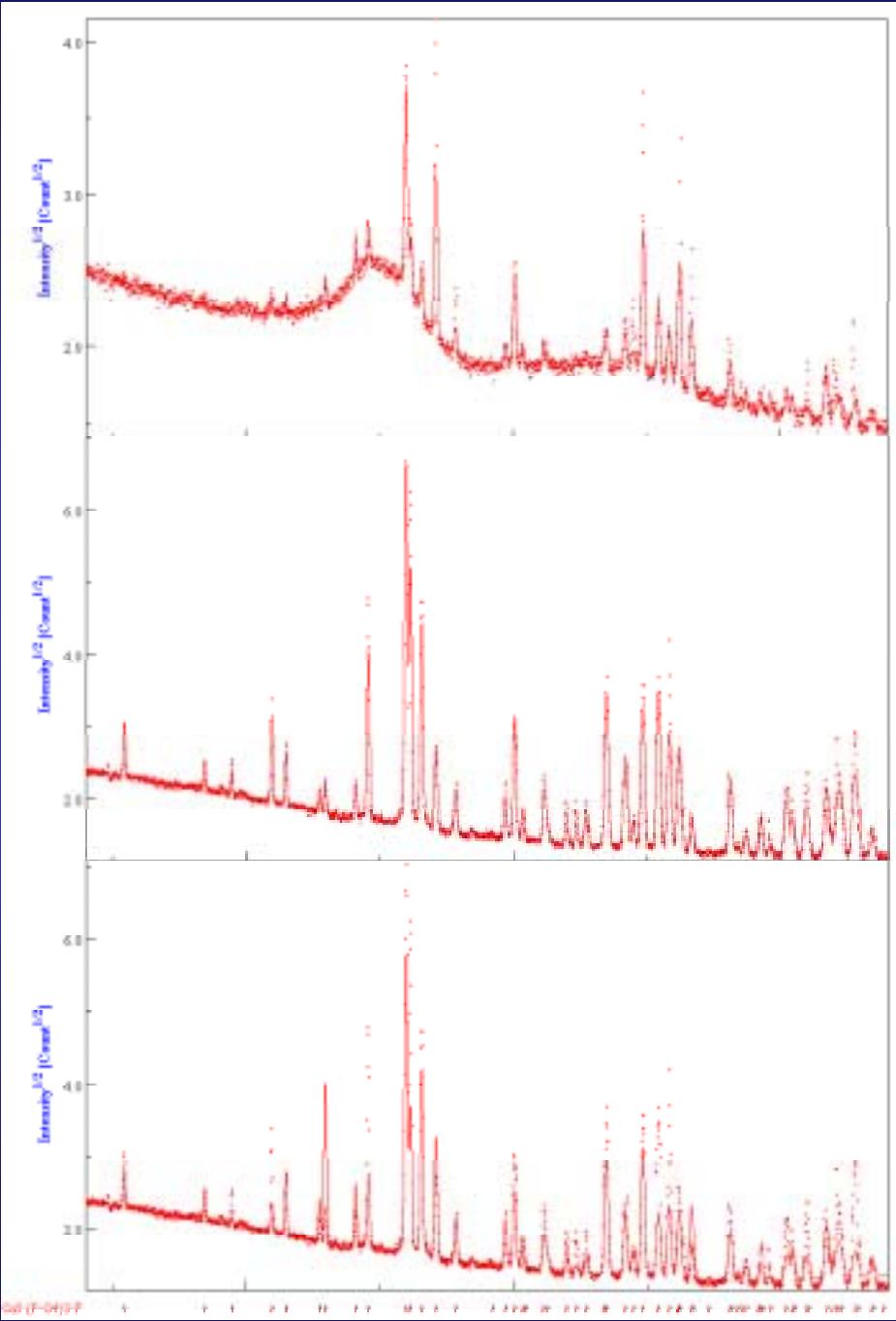
Irradiated FluorApatite (FAp) ceramics

S. Miro, PhD

Self-recrystallisation under irradiation, depending on $\text{SiO}_4 / \text{PO}_4$ ratio (FAp / Nd-Britholite) and on irradiating species



TEM of FAp
irradiated with 70
MeV, $10^{12} \text{ Kr cm}^{-2}$
ions



texture corrected,
 $10^{13} \text{ Kr cm}^{-2}$

Virgin, with texture
correction

Virgin, no texture
correction

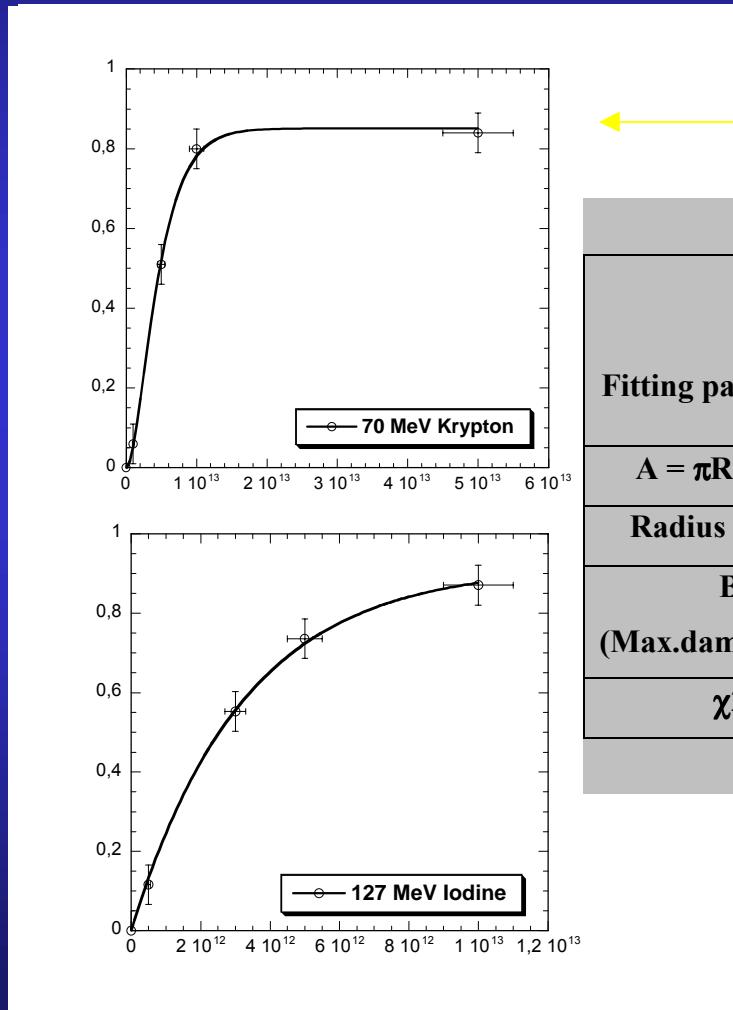
Fluence (ions.cm ⁻²)	Vc/V (%)	A (Å)	c (Å)	$\langle t \rangle$ (nm)	$\Delta a/a_0$ (%)	$\Delta c/c_0$ (%)	R _w (%)	R _B (%)
0	100	9.3365(3)	6.8560(5)	294(22)	-	-	14.6	9.1
Kr								
10^{11}	100	-	-	-	-	-		
10^{12}	100	-	-	-	-	-		
5.10^{12}	49(1)	9.3775(9)	6.8912(8)	294(20)	0.44	0.53	24	15
10^{13}	20(1)	9.4236(5)	6.9105(5)	291(20)	0.94	0.82	9.9	6
5.10^{13}	14(1)	9.3160(4)	6.8402(5)	294(22)	-0.21	-0.22	10.5	5.9
I								
10^{11}	-	-	-	-	-	-		
5.10^{11}	86(2)	9.3603(3)	6.8790(5)	90(10)	0.26	0.35	23.9	15.1
10^{12}	-	-	-	-	-	-		
3.10^{12}	47(2)	9.3645(3)	6.8840(5)	91(6)	0.30	0.42	13.3	9
5.10^{12}	29.2(5)	9.3765(5)	6.8881(6)	77(11)	0.44	0.48	10.4	7.3
10^{13}	13.2(2)	9.3719(4)	6.8857(6)	82(9)	0.38	0.45	6.7	4.9

Single impact model associated to crystal size reduction

Cell parameters and volume increase, then relax

Amorphisation / recrystallisation competition: single or double impact

Amorphous/crystalline volume fraction (damaged fraction $F_d = V_a / V$) as determined by x-ray diffraction



B

Fitting parameters	Krypton		Iodine
	Single impact $F_d = B(1 - \exp(-A\phi t))$	Double impact $F_d = B(1 - (1 + A\phi t) \exp(-A\phi t))$	Single impact $F_d = B(1 - \exp(-A\phi t))$
$A = \pi R^2 (\text{cm}^2)$	$1.85 \pm 0.15 \cdot 10^{-13}$	$4.1 \pm 0.15 \cdot 10^{-13}$	$3.3 \pm 0.15 \cdot 10^{-13}$
Radius R (nm)	2.4 ± 0.2	3.6	3.2
B (Max.damage rate)	0.87	0.85 ± 0.2	0.92 ± 0.2
χ^2	0.013	0.0006	0.0004

Conclusions

- a) Texture affects phase ratio and structure determination
- b) Microstructure (crystallite size) affects texture (go to a)
- c) Stresses shift peaks then affects structure and texture determination
- d) Combined analysis may be a solution, unless you can destroy your sample or are not interested in macroscopic anisotropy ...
- e) If you think you can destroy it, perhaps think twice
- f) more information is always needed: local probes ...
- g) www.ecole.ensicaen.fr/~chateign/texture/combined.pdf