

**Combined Analysis:** texture, structure, microstructure, phase, stress, reflectivity  
(multiphase bulks and thin films, x-rays and neutron diffraction): some case studies

**Daniel Chateigner**  
*CRISMAT-ENSICAEN (Caen-France)*

**Bi2223  
Superconductors**

**PCT & PMN-PT  
Ferroelectrics**

**Irradiated  
FAp ceramics**

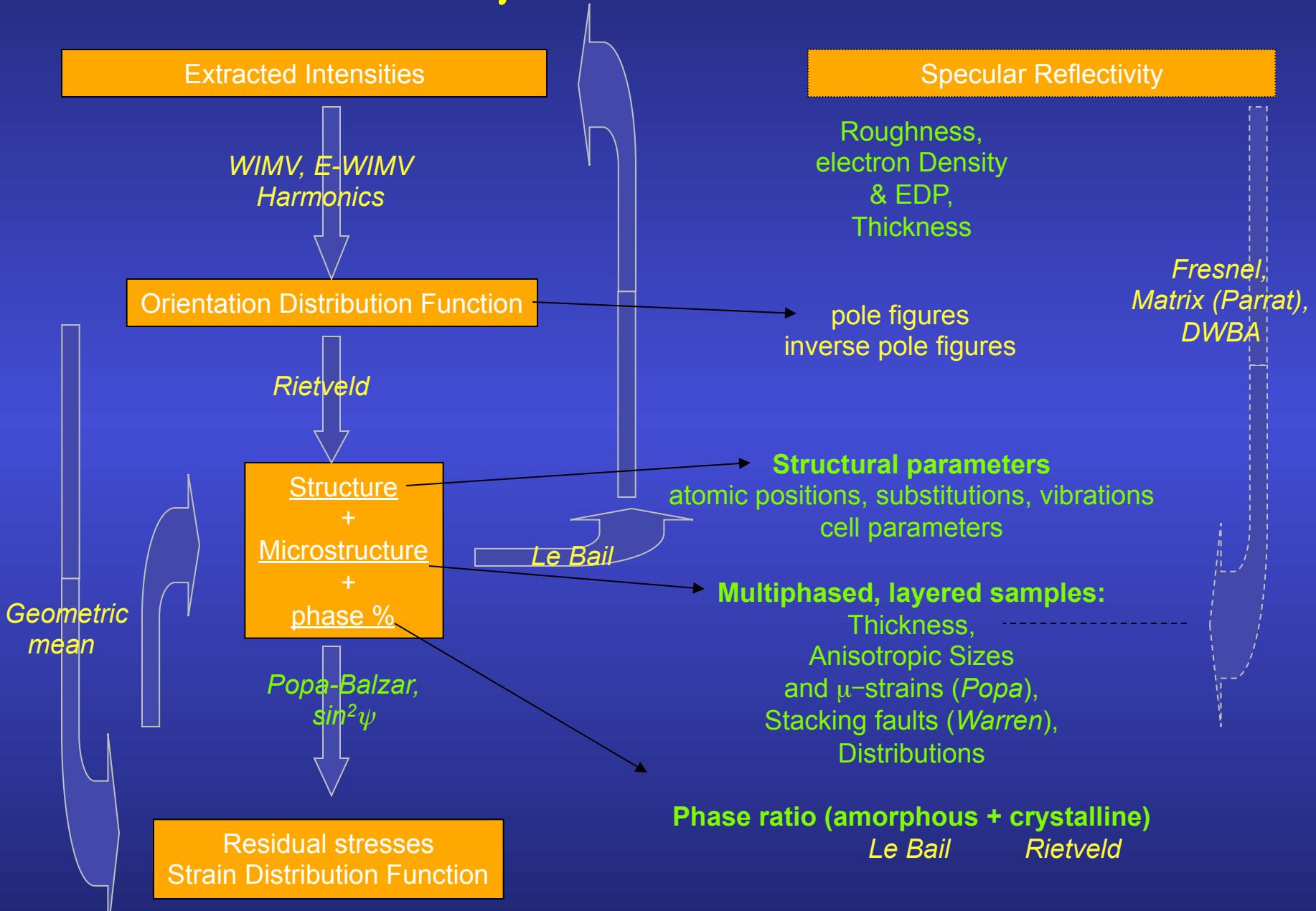


**$\text{Ca}_3\text{Co}_4\text{O}_9$   
Thermoelectrics**

**nano-Si  
thin films**



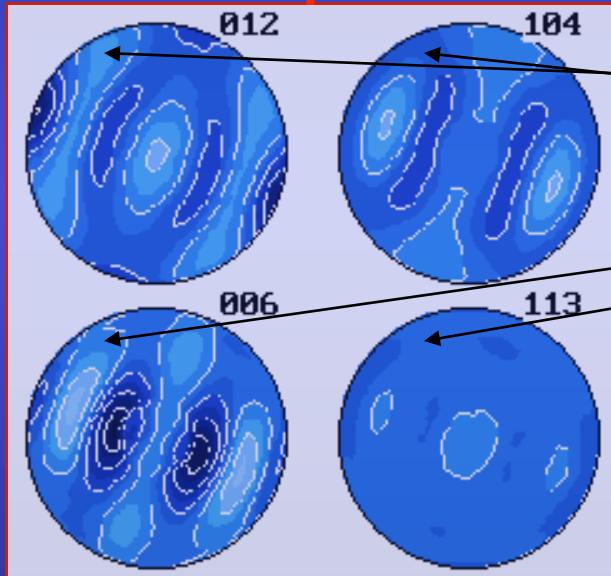
# Implemented codes



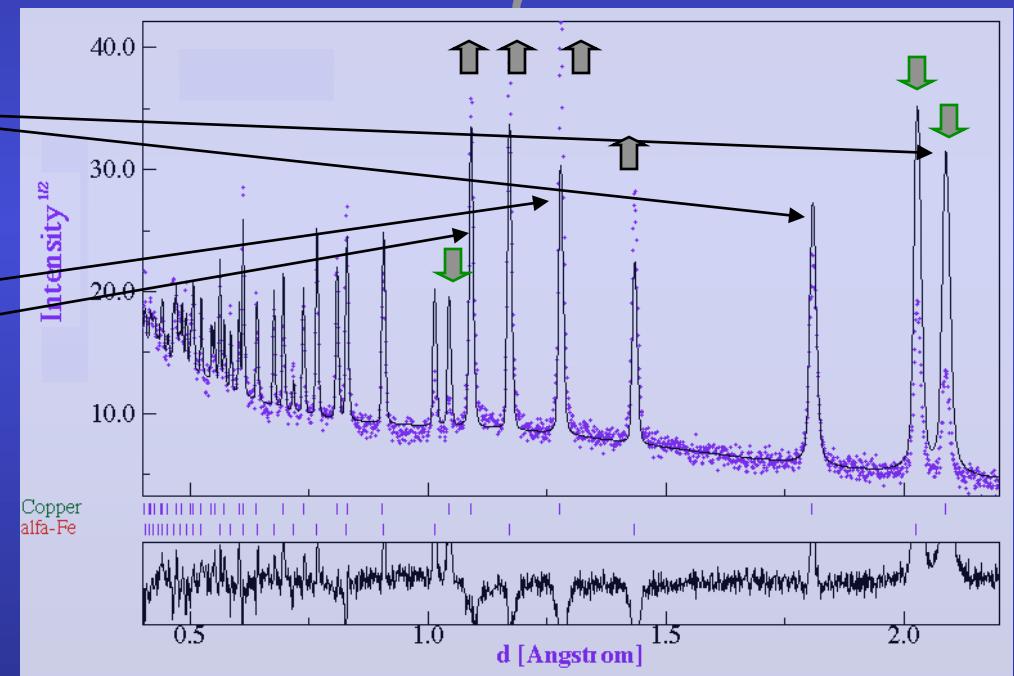
# Texture from Spectra

## Orientation Distribution Function (ODF)

From pole figures



From spectra



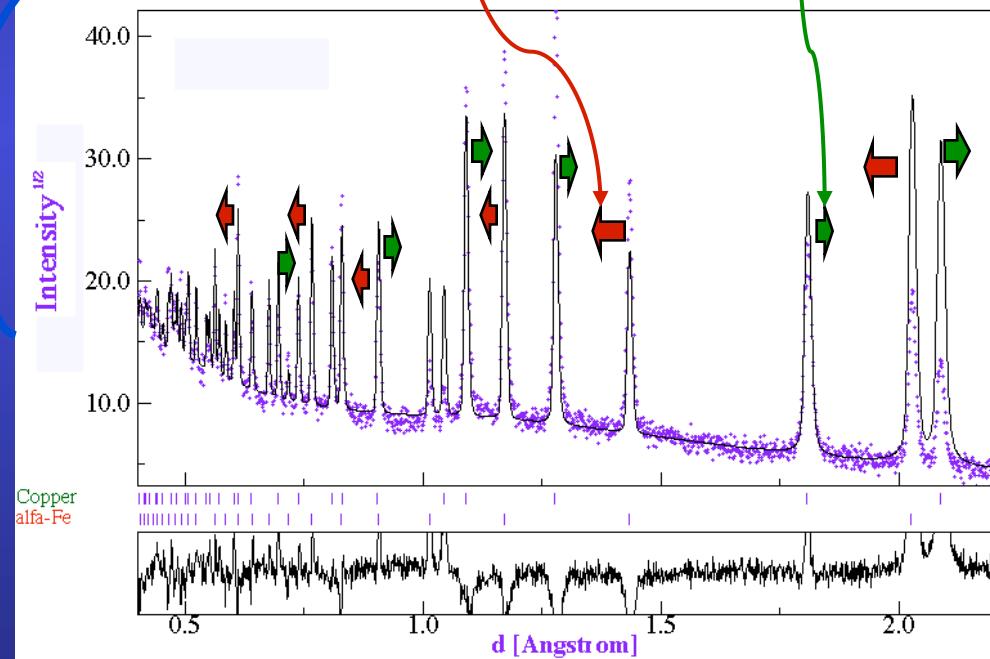
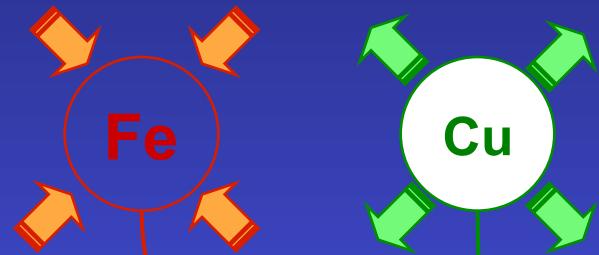
# Residual Stresses and Rietveld

- Macro elastic strain tensor (I kind)
- Crystal anisotropic strains (II kind)

Macro and micro stresses

Applied macro stresses

C



Textured samples: Reuss, Voigt, Hill, Bulk geometric mean approaches

# How it works (Combined)

$$I_i^{calc}(\chi, \phi) = \sum_{n=1}^{Nphases} S_n \sum_k L_k \left| F_{k;n} \right|^2 S(2\theta_i - 2\theta_{k;n}) P_{k;n}(\chi, \phi) A + bkg_i$$

## Texture

$$P_k(\chi, \phi) = \int_{\varphi} f(g, \varphi) d\varphi$$

- from Generalized Spherical Harmonics:

$$P_k(\chi, \phi) = \sum_{l=0}^{\infty} \frac{1}{2l+1} \sum_{n=-l}^l k_l^n(\chi, \phi) \sum_{m=-l}^l C_l^{mn} k_n^{*m}(\Theta_k \phi_k)$$

$$f(g) = \sum_{l=0}^{\infty} \sum_{m,n=-l}^l C_l^{mn} T_l^{mn}(g)$$

- from the WIMV (left) iterative process or entropy maximisation (right):

$$f^{n+1}(g) = N_n \frac{f^n(g) f^0(g)}{\left( \prod_{\mathbf{h}=1}^I \prod_{m=1}^{M_{\mathbf{h}}} P_{\mathbf{h}}^n(\mathbf{y}) \right)^{\frac{1}{IM_{\mathbf{h}}}}}$$

$$f^{n+1}(g) = f^n(g) \prod_{m=1}^{M_{\mathbf{h}}} \left( \frac{P_{\mathbf{h}}(\mathbf{y})}{P_{\mathbf{h}}^n(\mathbf{y})} \right)^{\frac{r_{\mathbf{h}}}{M_{\mathbf{h}}}}$$

# Layering

$$C_{\chi}^{\text{top film}} = g_1 \left( 1 - \exp(-\mu T g_2 / \cos \chi) \right) / \left( 1 - \exp(-2\mu T / \sin \omega \cos \chi) \right)$$

$$C_{\chi}^{\text{cov. layer}} = C_{\chi}^{\text{top film}} \left( \exp \left( -g_2 \sum \mu_i' T_i' / \cos \chi \right) \right) / \left( \exp \left( -2 \sum \mu_i' T_i' / \sin \omega \cos \chi \right) \right)$$

# Popa anisotropic shapes & microstrains

$$\langle R_h \rangle = R_0 + R_1 P_2^0(x) + R_2 P_2^1(x) \cos \varphi + R_3 P_2^1(x) \sin \varphi + R_4 P_2^2(x) \cos 2\varphi + R_5 P_2^2(x) \sin 2\varphi +$$

$$\langle \varepsilon_h^2 \rangle E_h^4 = E_1 h^4 + E_2 k^4 + E_3 \ell^4 + 2E_4 h^2 k^2 + 2E_5 \ell^2 k^2 + 2E_6 h^2 \ell^2 + 4E_7 h^3 k + 4E_8 h^3 \ell + 4E_9 k^3 h + 4E_{10} k^3 \ell + 4E_{11} \ell^3 h + 4E_{12} \ell^3 k + 4E_{13} h^2 k \ell + 4E_{14} k^2 h \ell + 4E_{15} \ell^2 k h$$

# Roughness and/or microabsorption

$$R^{rough}(q_z) = R(q_z) \exp(-q_{z,0} q_{z,1} \sigma^2) \quad \text{Low-angles (reflectivity)}$$

$$S_R = 1 - p \exp(-q) + p \exp\left(\frac{-q}{\sin \theta}\right) \quad \text{high-angle (Suortti)}$$

## Specular reflectivity: $\mathbf{q}=(0,0,z)$

- Fresnel:

$$R(\mathbf{q}) = \left| \frac{q_z - \sqrt{q_z^2 - q_c^2 + \frac{32i\pi^2\beta}{\lambda^2}}}{q_z + \sqrt{q_z^2 - q_c^2 + \frac{32i\pi^2\beta}{\lambda^2}}} \right|^2 \delta q_x \delta q$$

- matrix:

$$R^{flat} = \frac{r_{0,1}^2 + r_{1,2}^2 + 2r_{0,1}r_{1,2} \cos 2k_{z,1}h}{1 + r_{0,1}^2 r_{1,2}^2 + 2r_{0,1}r_{1,2} \cos 2k_{z,1}h}$$

- Born approximation:

$$R(q_z) = r \cdot r^* = R_F(q_z) \left| \frac{1}{\rho_s} \int_{-\infty}^{+\infty} \frac{d\rho(z)}{dz} e^{iq_z z} dz \right|^2$$

# Phase

$$W_{\Phi} = \frac{S_{\Phi} Z_{\Phi} M_{\Phi} V_{\Phi}}{\sum_{i=1}^{N_{\Phi}} S_i Z_i M_i V_i}$$

# Strain-Stress

$$\boldsymbol{\varepsilon}(\mathbf{X}) = \boldsymbol{\varepsilon}^I + \boldsymbol{\varepsilon}^{II}(\mathbf{X}) + \boldsymbol{\varepsilon}^{III}(\mathbf{X})$$

$$\begin{aligned} \langle \varepsilon_h(y) \rangle_{V_d} &= \frac{1}{V_d} \int_{V_d} (\varepsilon'_{33} + \varepsilon''_{33} + \varepsilon'''_{33}) dV \\ &= (\varepsilon'_{11} \cos^2 \phi + \varepsilon'_{12} \sin 2\phi + \varepsilon'_{22} \sin^2 \phi - \varepsilon'_{33}) \sin^2 \psi + \varepsilon'_{33} + \\ &\quad (\varepsilon'_{13} \cos \phi + \varepsilon'_{23} \sin \phi) \sin 2\psi + \frac{1}{V_d} \int_{V_d} (\varepsilon''_{33e} + \varepsilon''_{33t} + \varepsilon''_{33p}) dV \\ &= \frac{\langle d(hkl, \phi, \psi) \rangle_{V_d} - d_0(hkl)}{d_0(hkl)} \end{aligned}$$

*Isotropic samples:*  
Tri-, bi-, uni-axial stress states

*Textured samples:*  
Tri-, bi-, uni- stress states  
+ ODF + SDF + model

$$\begin{aligned} \langle E(\mathbf{g}) \rangle_{V_d} &= \frac{1}{V_d} \int_{V_d} E^{SC}(g) f(g) dg \quad \Rightarrow \quad C_{ijkl}^M \neq \left( S_{ijkl}^M \right)^{-1} \\ &= \left( \prod_{V_d} E^{SC}(g) f(g) dg \right)^{\frac{1}{V_d}} \quad \Rightarrow \quad C_{ijkl}^M = \left( S_{ijkl}^M \right)^{-1} \end{aligned}$$

Reuss, Voigt, Hill

Geometric mean, VPSC

# *Minimum experimental requirements*

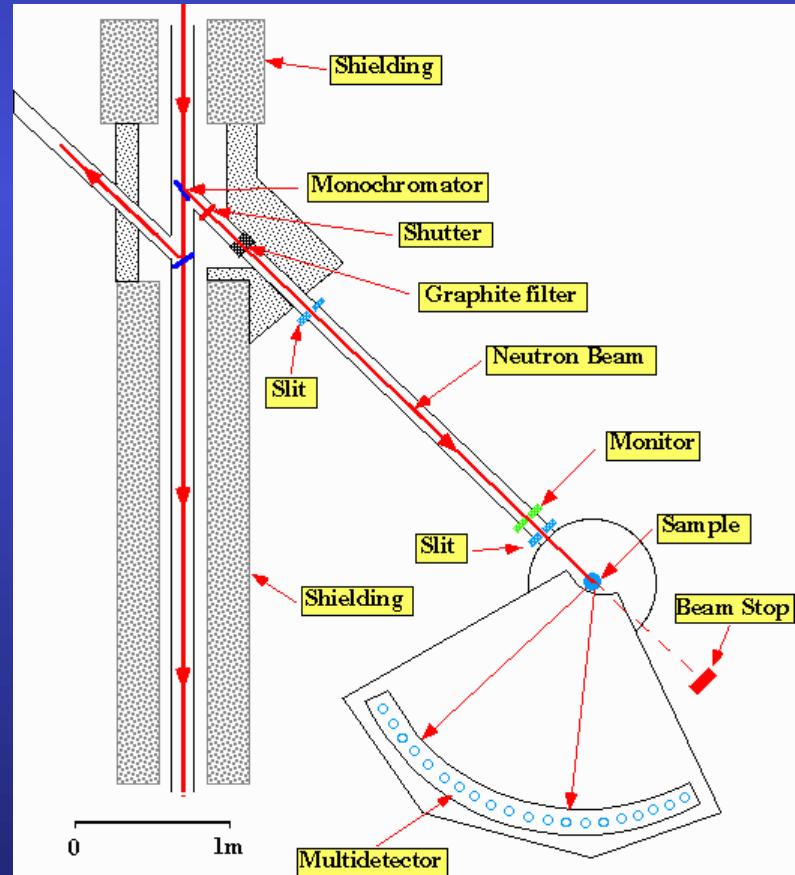
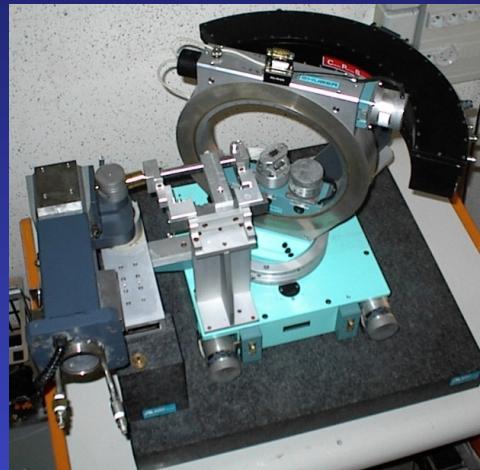
1D or 2D Detector + 4-circle diffractometer  
(X-rays and neutrons)  
CRISMAT, ILL

+

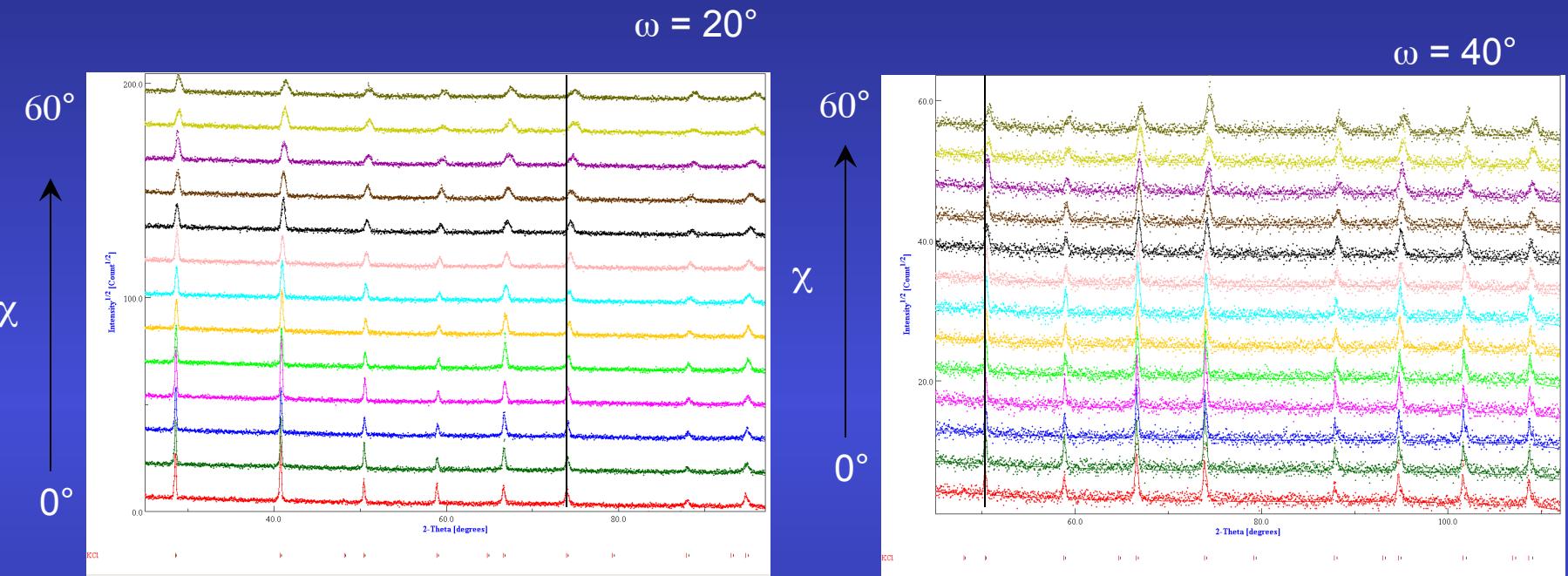
~1000 experiments (2θ diagrams)  
in as many sample orientations

+

Instrument calibration  
(peaks widths and shapes,  
misalignments, defocusing ...)



# Calibration



KCl, LaB<sub>6</sub> ...

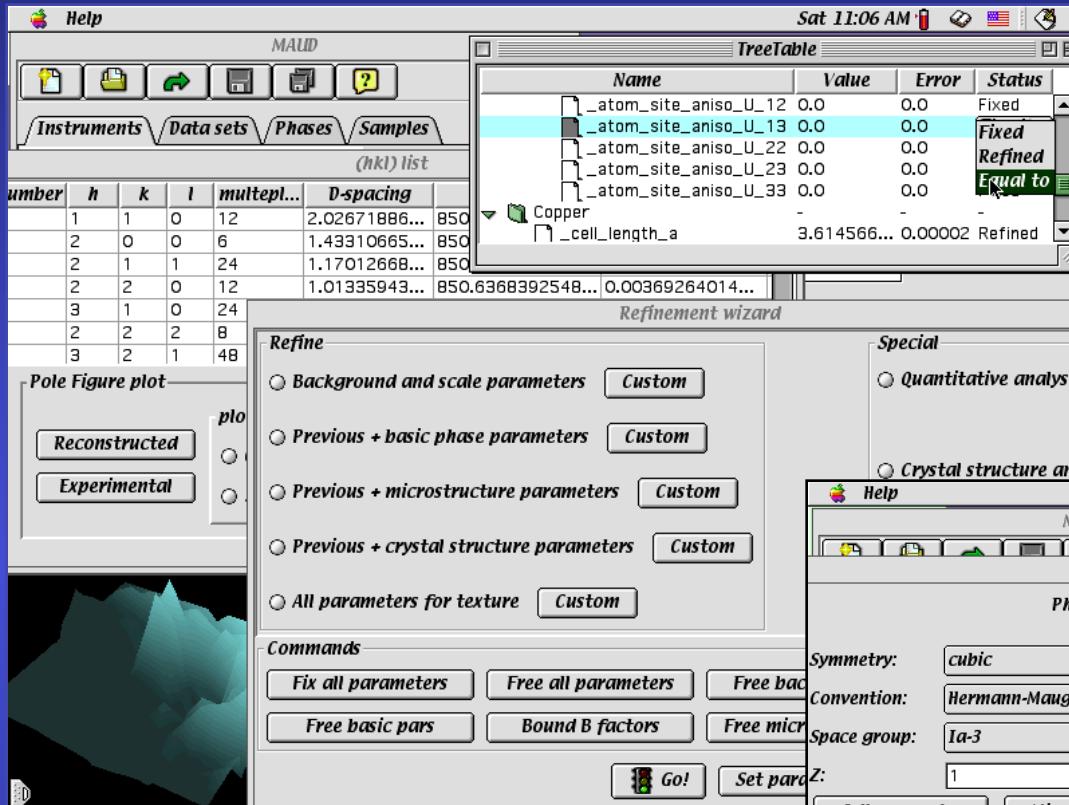


FWHM ( $\omega, \chi, 2\theta \dots$ )  
2 $\theta$  shift  
gaussianity  
asymmetry  
misalignments ...

# Methodology implementation

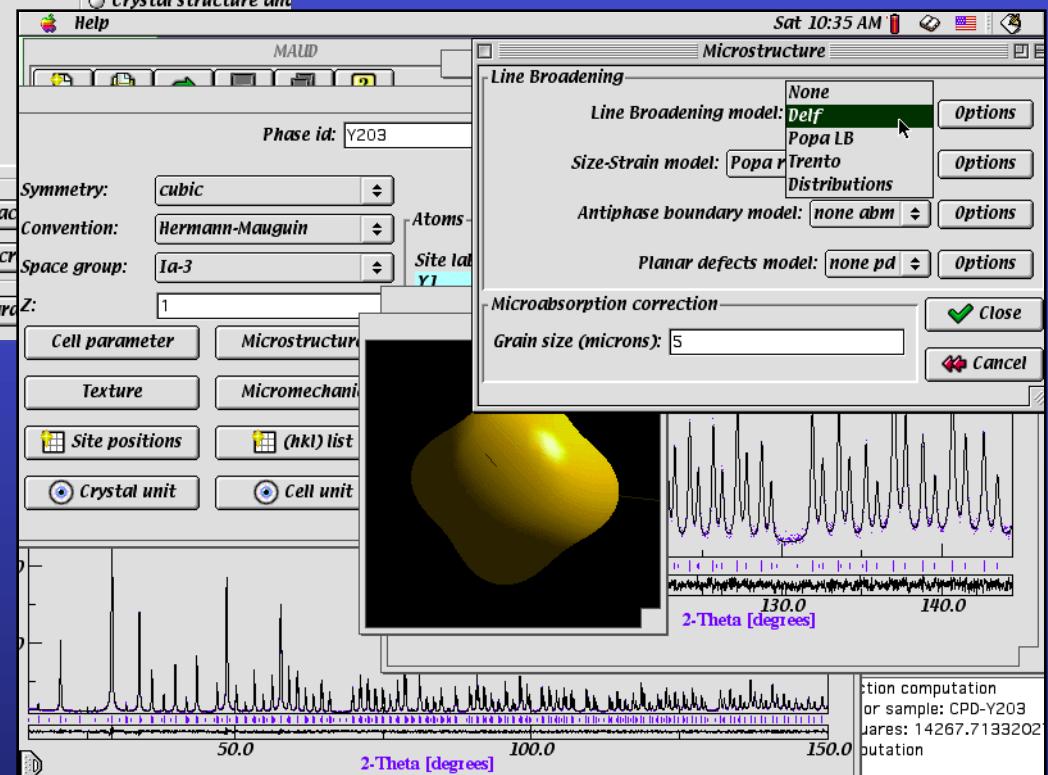
L. Lutterotti, Trento

User friendly interface



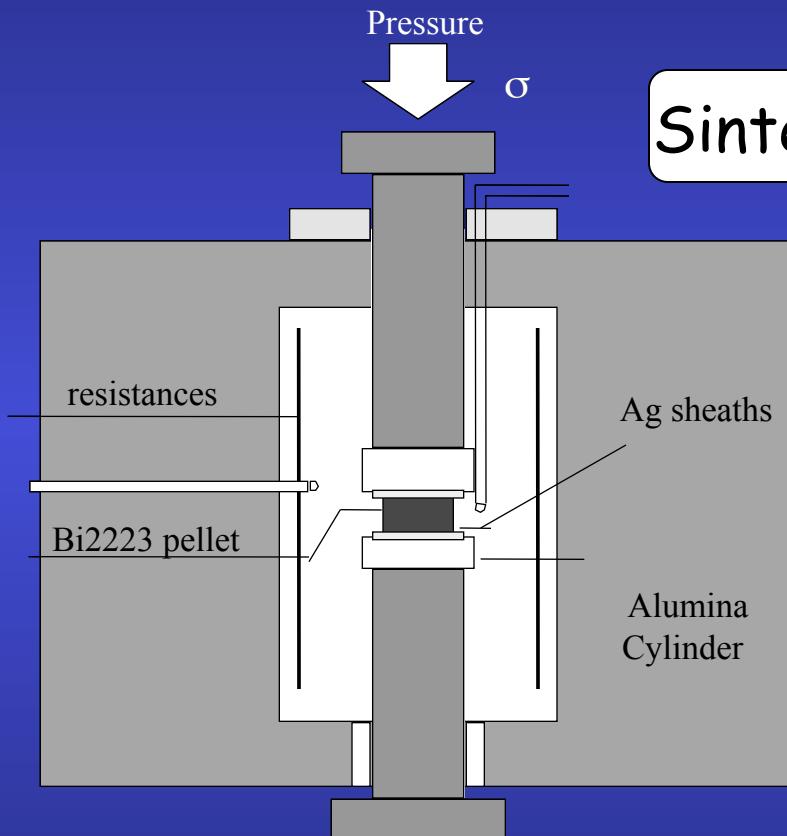
Java codes

Java web start updates

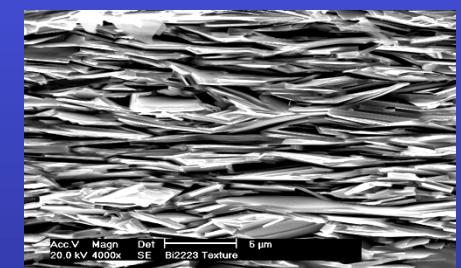
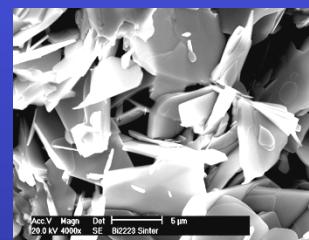
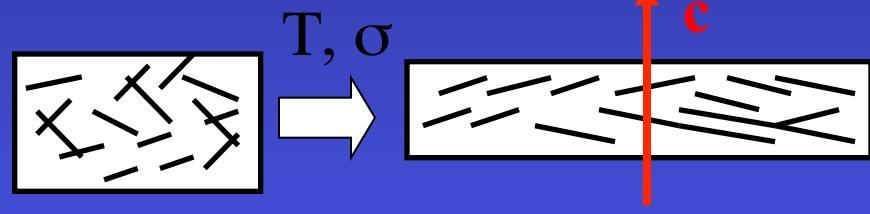


# *Bi2223 compounds*

E. Guilmeau, CRISMAT

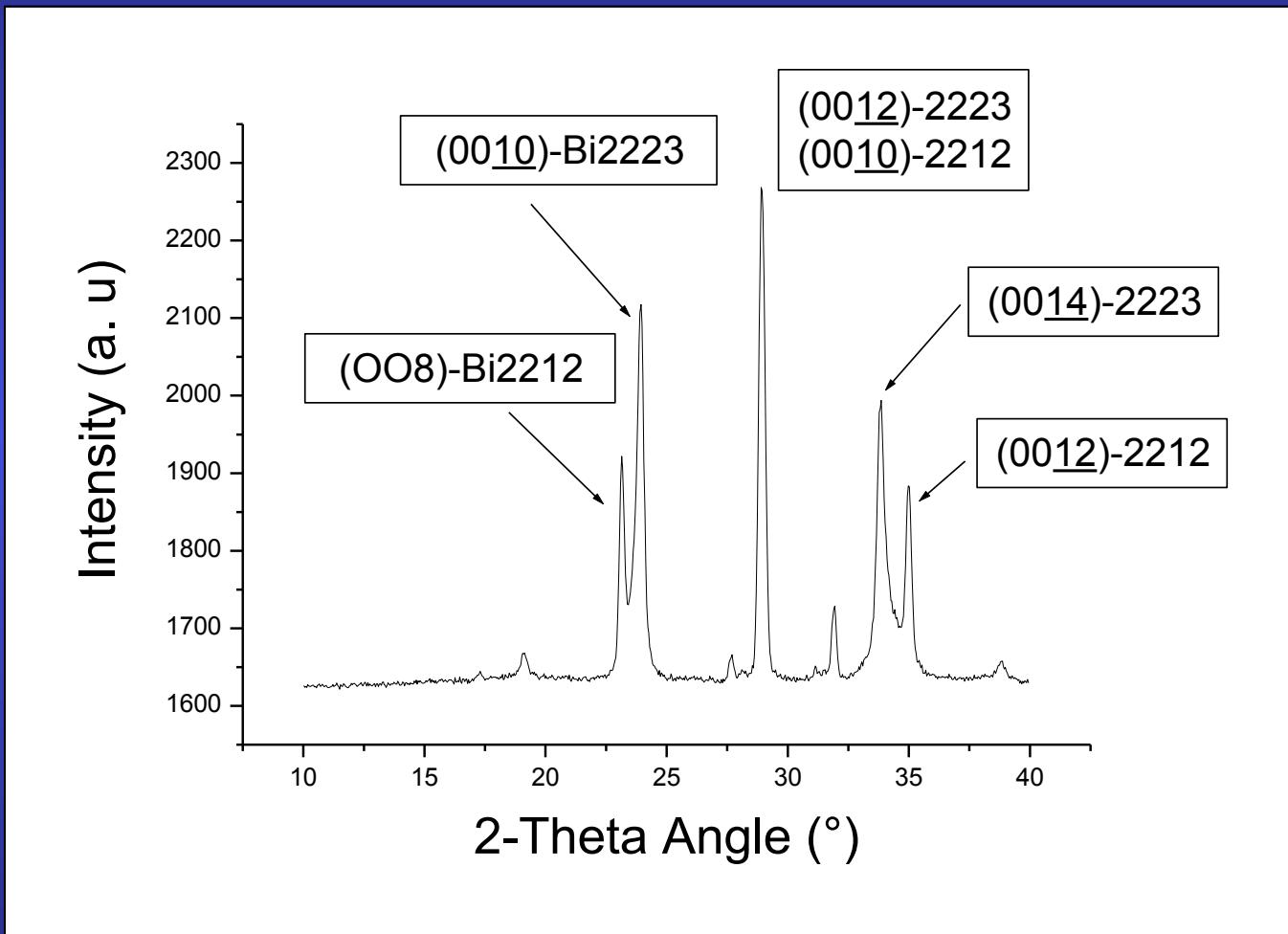


Sinter-Forging

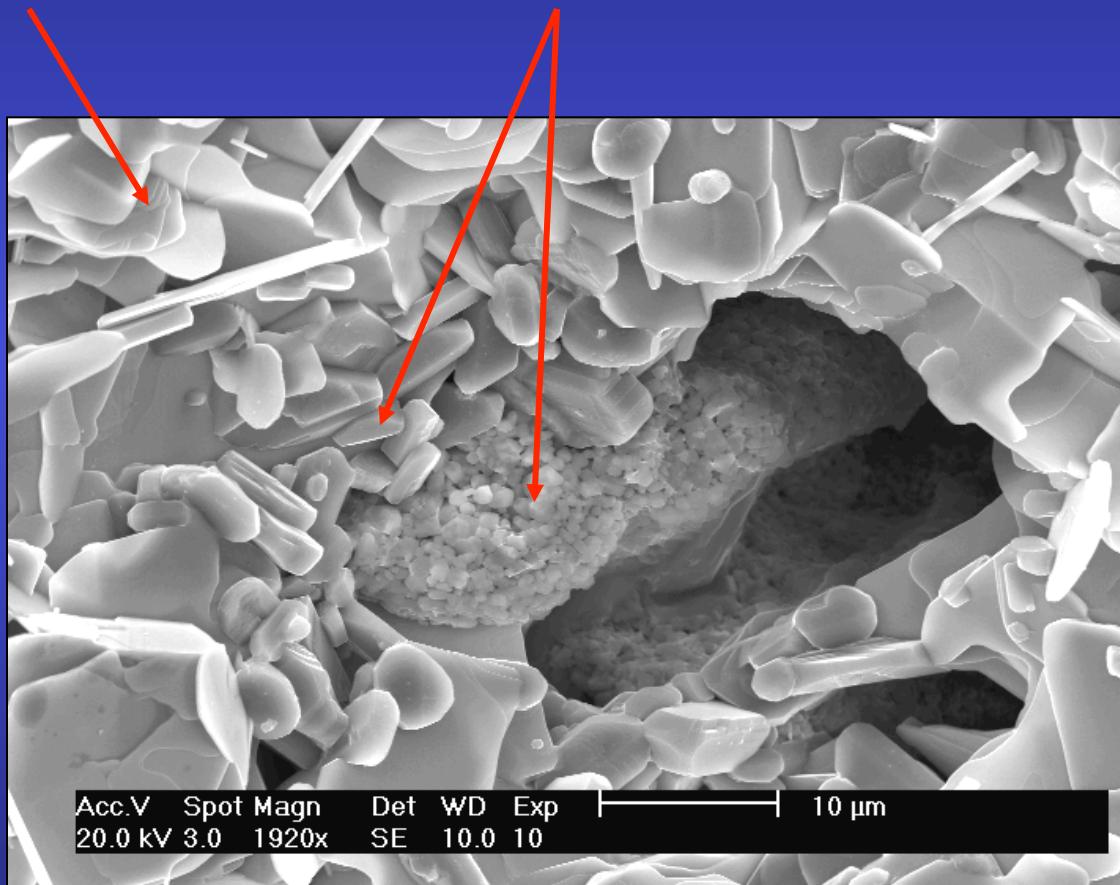


Grain alignment  $\Rightarrow$   $\nearrow J_c$

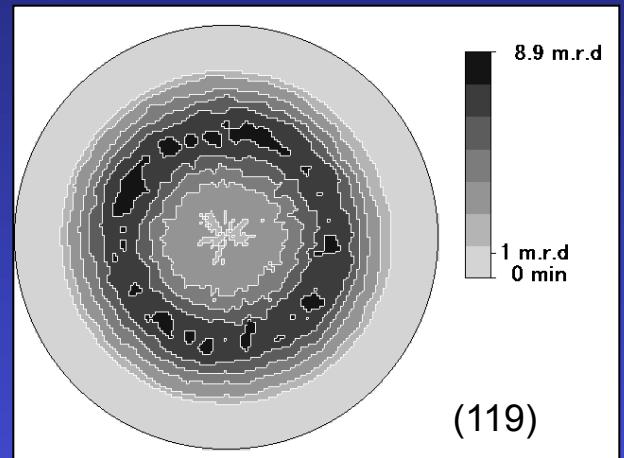
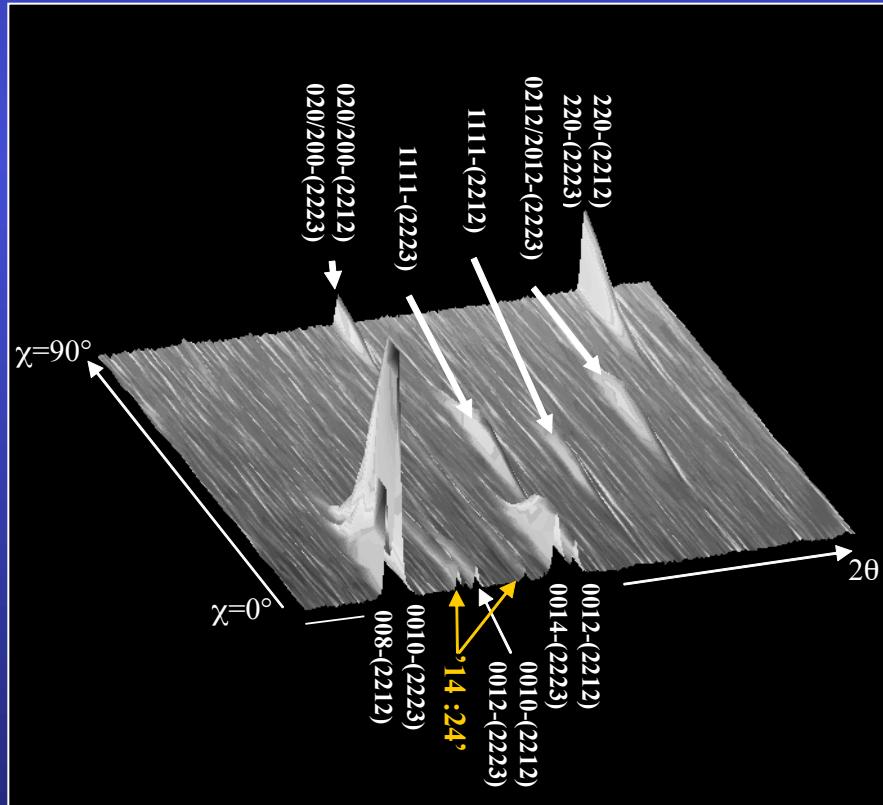
## (00 $\ell$ ) Texture



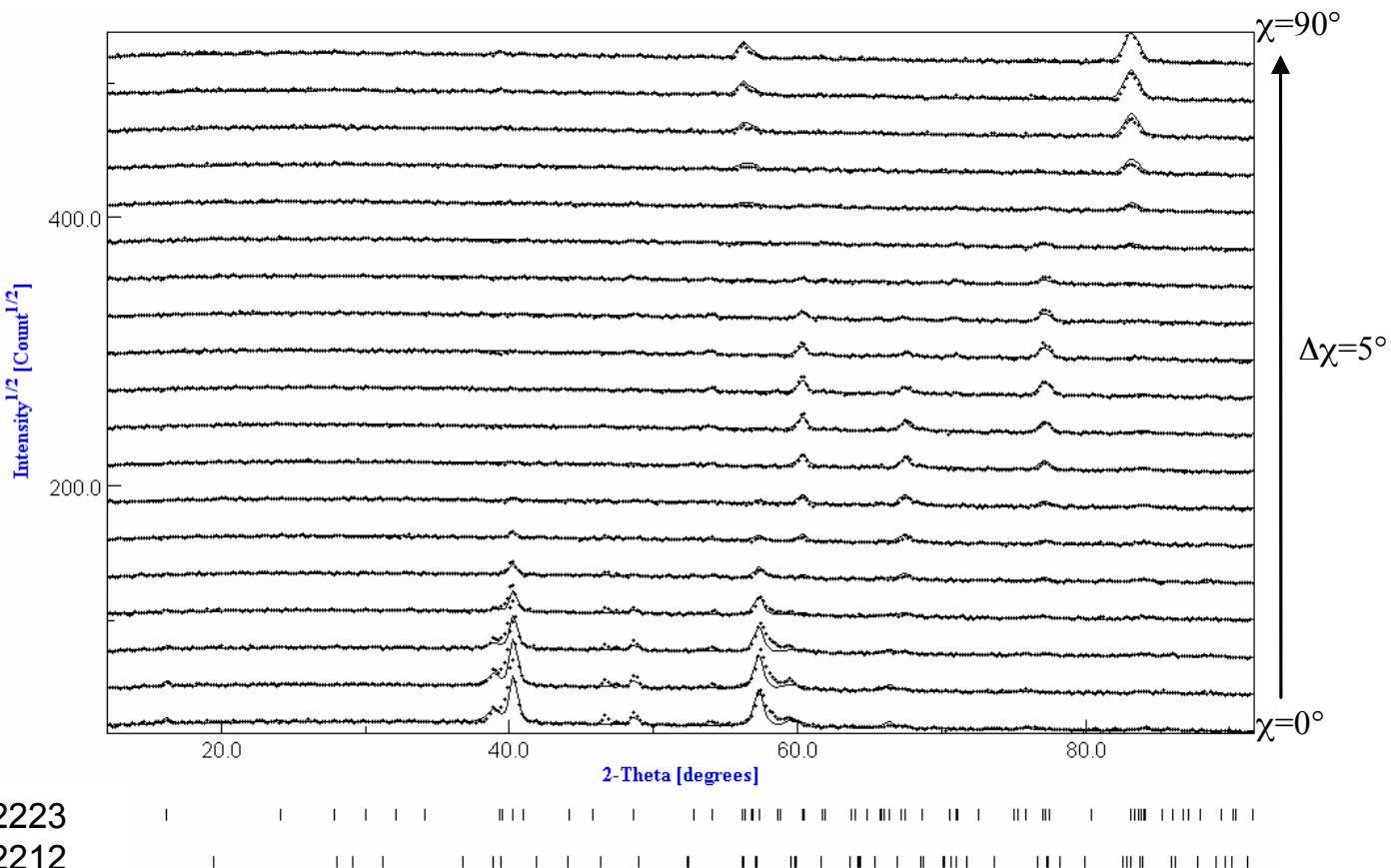
$\text{Bi2212} + \text{Secondary phases} \longrightarrow \text{Bi2223}$



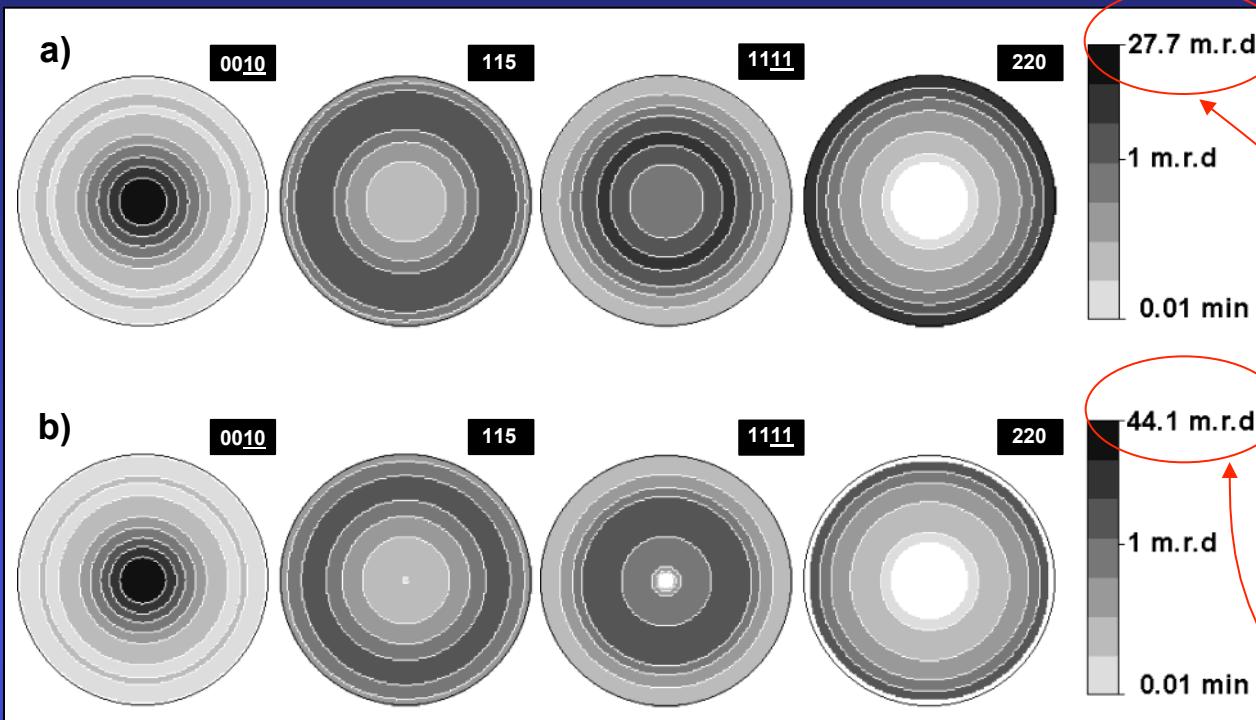
## Combined Analysis



- Neutrons
- Sample:  $\sim 70 \text{ mm}^3$
- $2\theta$  patterns for  $\chi=0^\circ$  to  $90^\circ$
- No  $\varphi$  rotation (fibre texture).



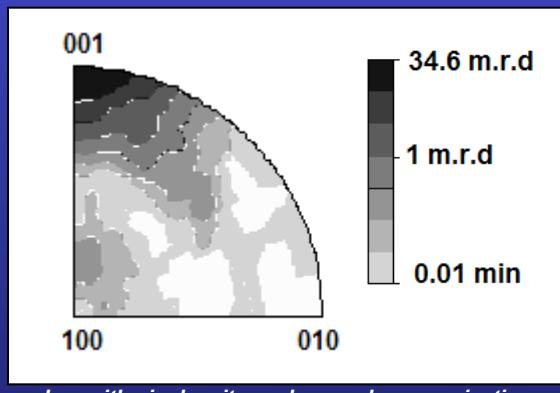
Rw=9.12  
RP=16.24



*Recalculated  
(WIMV)*

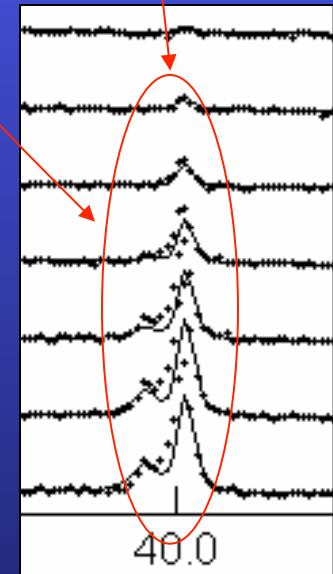
*Extracted  
(Le Bail)*

*Logarithmic density scale, equal area projection*



Stacking faults and/or intergrowth on the c-axis  
→ New periodicities and peaks characterized with intermediate c parameters.

However, no algorithm is included to solve intergrowths in the combined approach.



## *Effect of the sinter-forging treatment on the texture development, crystal growth, transport properties*

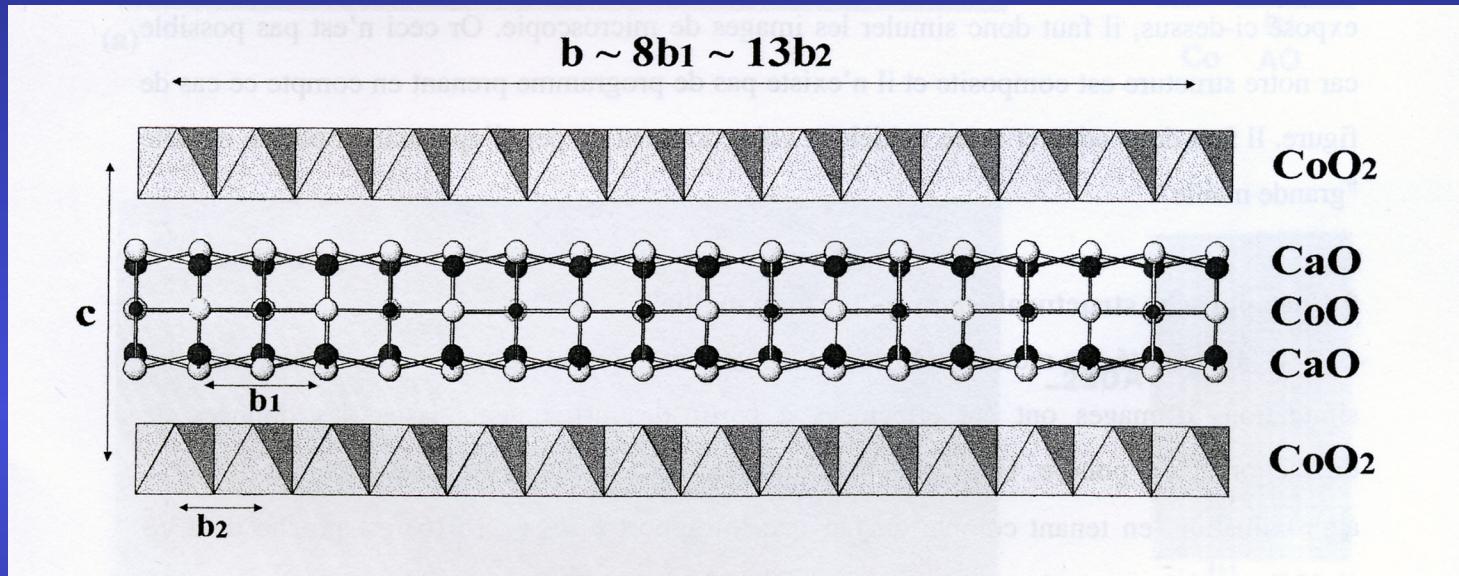
Sinter-forging dwell time (h)	Orientation Distribution Max (m.r.d.)		% Bi2223	Cell parameters ( $\text{\AA}$ )		Crystallite size Bi2223 (nm)	$R_b$ (%)	$R_w$ (%)	$R_{exp}$ (%)	$R_{P0}$ (%)	$R_{P1}$ (%)	$J_c$ ( $\text{A}/\text{cm}^2$ )
	$Bi2212$	$Bi2223$		$Bi2223$	$Bi2212$							
20	21.8	20.7	59.9 $\pm$ 1.3	a=5.419(3) b=5.391(3) c=37.168(3)	a=5.414(3) b=5.393(3) c=30.800(3)	205 $\pm$ 7	7.56	11.1	4.55	17.74	10.56	12500
50	24.1	24.4	72.9 $\pm$ 2.9	a=5.419(3) b=5.408(3) c=37.192(3)	a=5.416(3) b=5.396(3) c=30.806(3)	273 $\pm$ 10	7.54	11.37	4.58	17.05	11.04	15000
100	31.5	25.2	84.4 $\pm$ 4.6	a=5.410(3) b=5.405(3) c=37.144(3)	a=5.412(3) b=5.403(3) c=30.752(3)	303 $\pm$ 10	5.4	8.04	3.69	13.54	9.31	19000
150	65.4	27.2	87.0 $\pm$ 4.1	a=5.417(3) b=5.403(3) c=37.199(3)	a=5.413(3) b=5.407(3) c=30.792(3)	383 $\pm$ 13	6.13	9.12	4.8	16.24	12.25	20000



# *Ca<sub>3</sub>Co<sub>4</sub>O<sub>9</sub> thermoelectrics*

M. Prevel, CRISMAT

*Ca<sub>3</sub>Co<sub>4</sub>O<sub>9</sub>: Misfit lamellar and modulated Structure, with high thermopower*



*Two monoclinic sub-systems:*

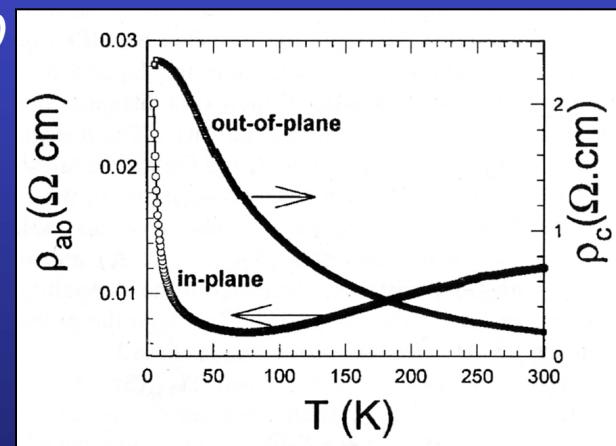
*S1 with  $a \sim 4.8\text{\AA}$ ,  $b_1 \sim 4.5\text{\AA}$ ,  $c \sim 10.8\text{\AA}$  et  $\beta \sim 98^\circ$  (NaCl-type)*

*S2 with  $a \sim 4.8\text{\AA}$ ,  $b_2 \sim 2.8\text{\AA}$ ,  $c \sim 10.8\text{\AA}$  et  $\beta \sim 98^\circ$  (CdI<sub>2</sub>-type)*

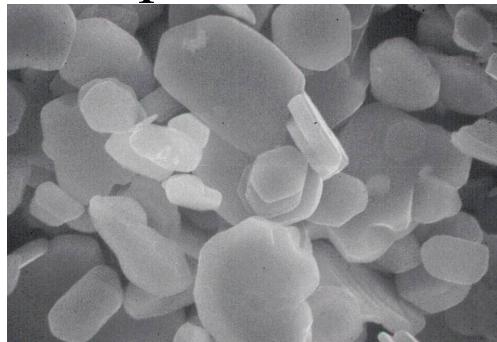
$$\Gamma = \sigma_{ab}/\sigma_c \sim 10$$



Texture

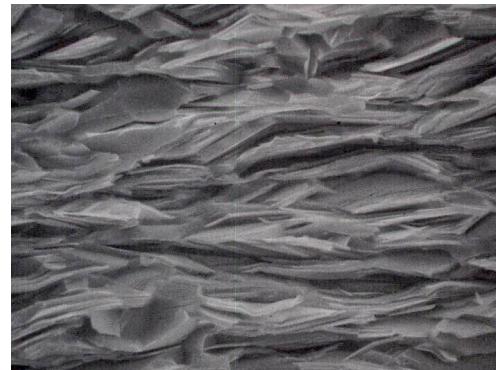


powder



10 μm

Textured bulk

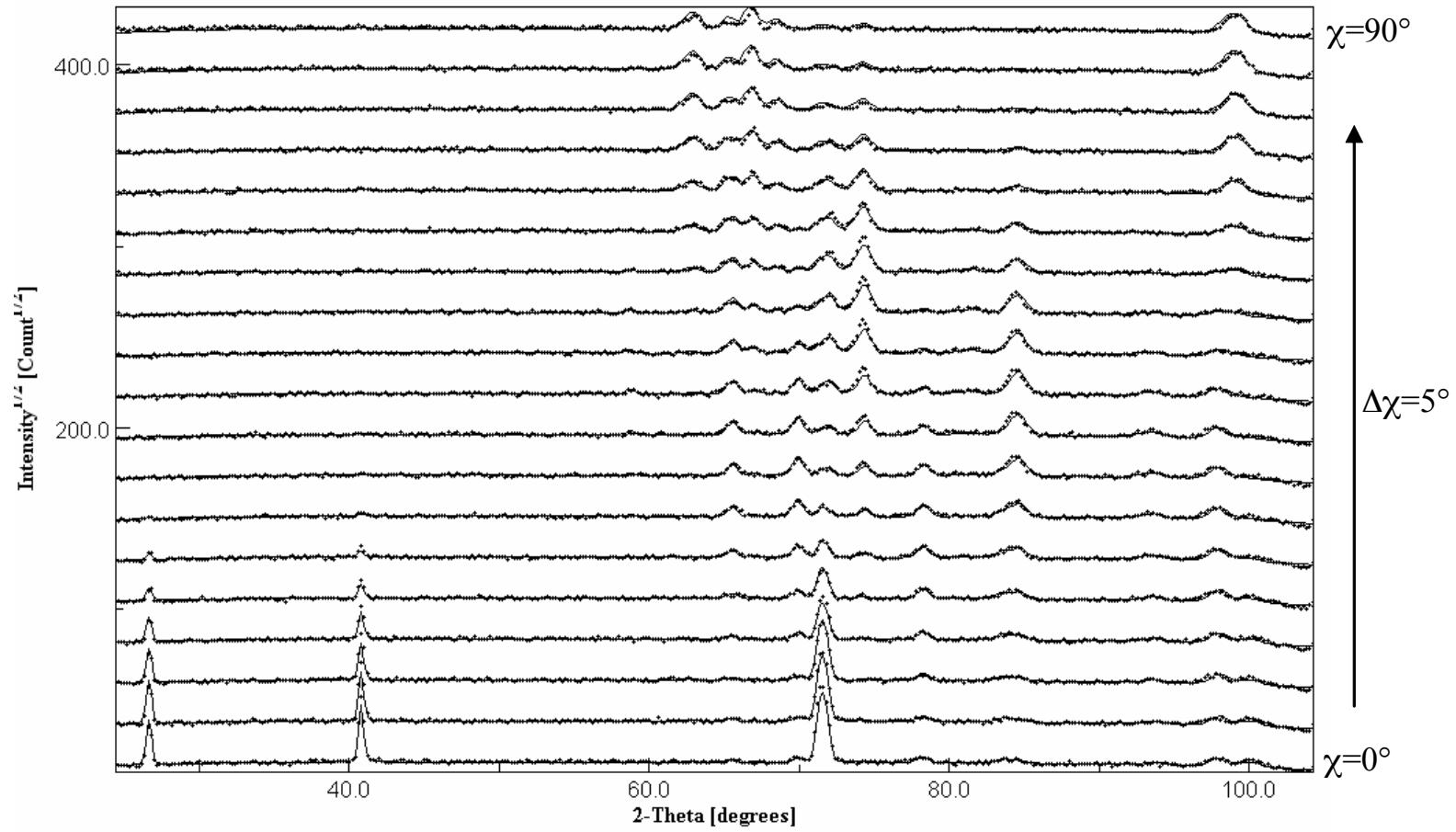


10 μm

*Magnetic alignment  
and  
Templated Growth  
method*

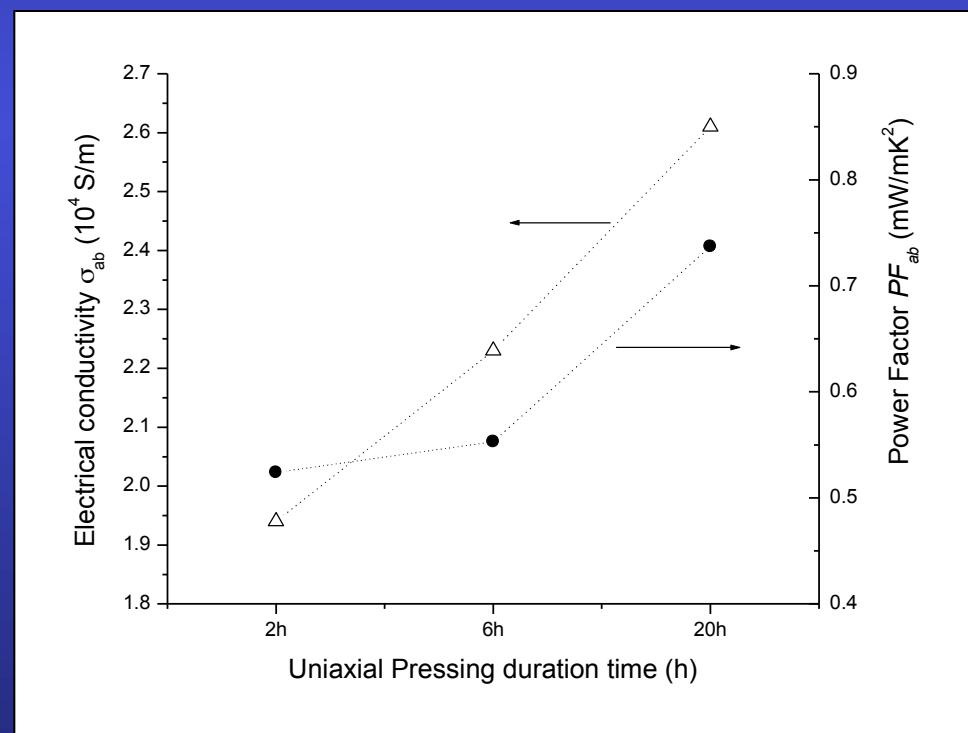
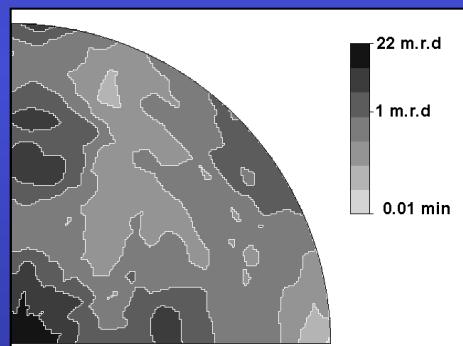
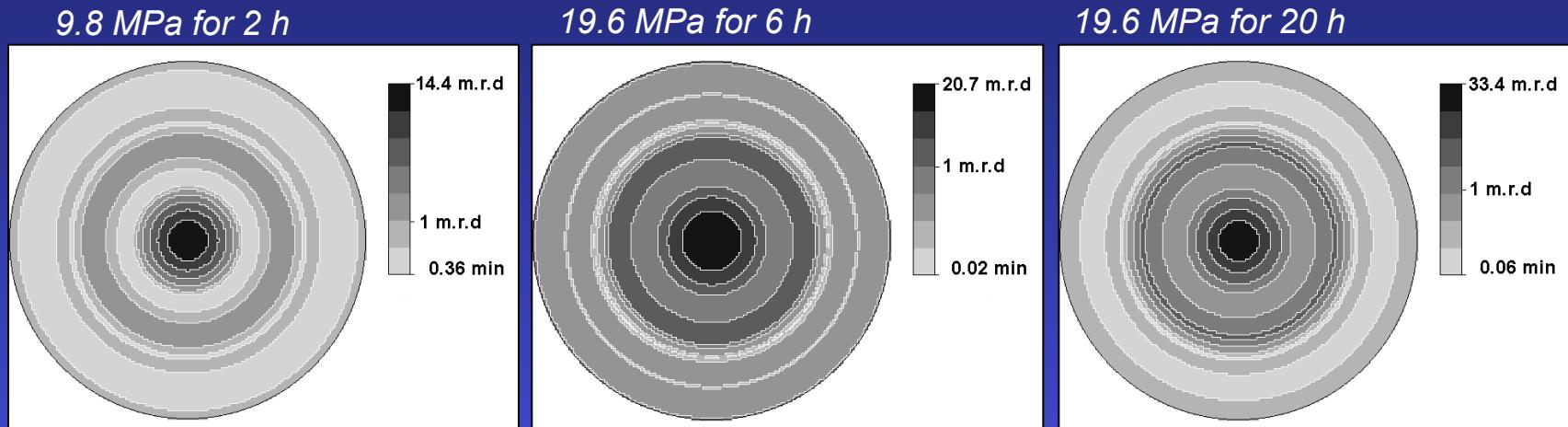
### **Analysis:**

- neutrons
- 3D Supercell:  $a=4.8309\text{\AA}$ ,  $b\sim8b_1\sim13b_2\sim36.4902\text{\AA}$ ,  $c=10.8353\text{\AA}$ ,  $\beta=98.13^\circ$   
 $174 \text{ atoms/cell}$
- Sample :  $0.6 \text{ cm}^3$



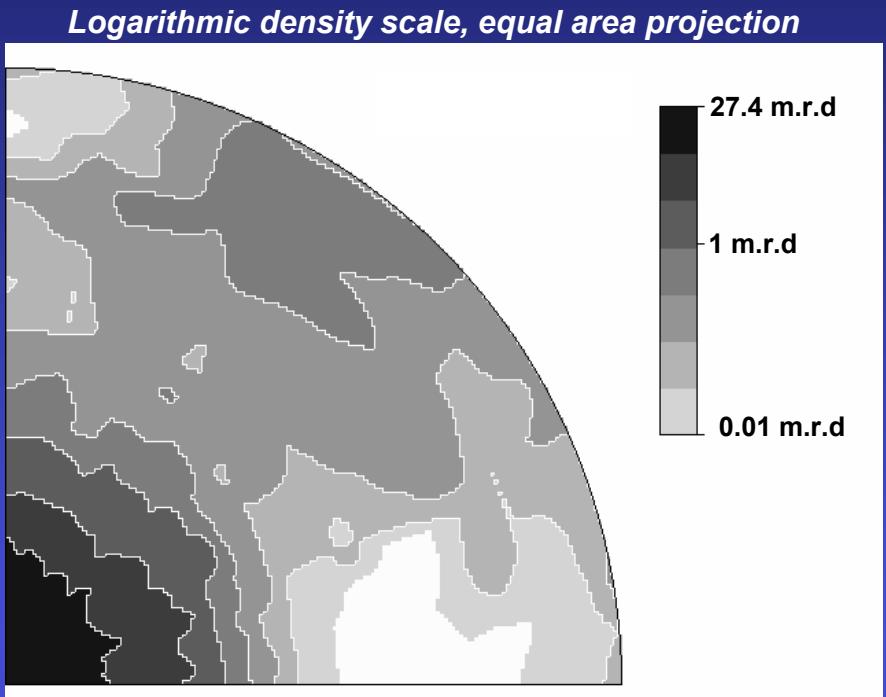
Supercell

RP=19.7%, Rw=11.9%



*Templated Growth Method*

## *Magnetic Alignment*



- *magnetic alignment really efficient to obtain strong textures*
- *combined analysis of modulated structures possible*

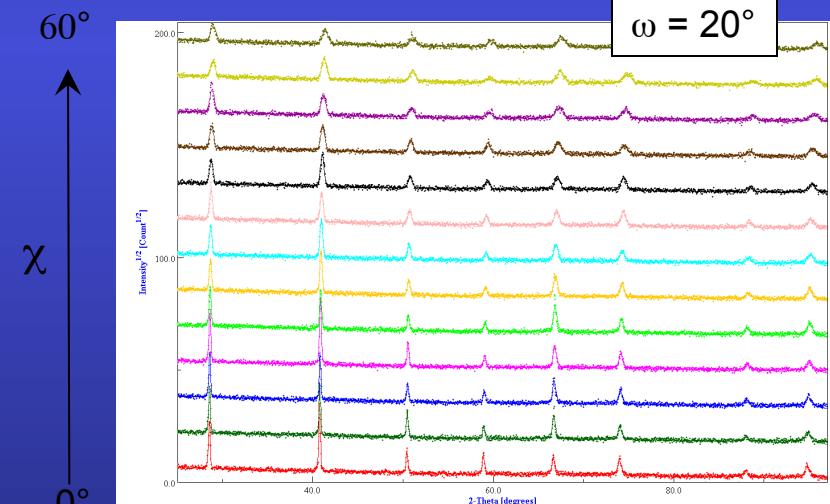
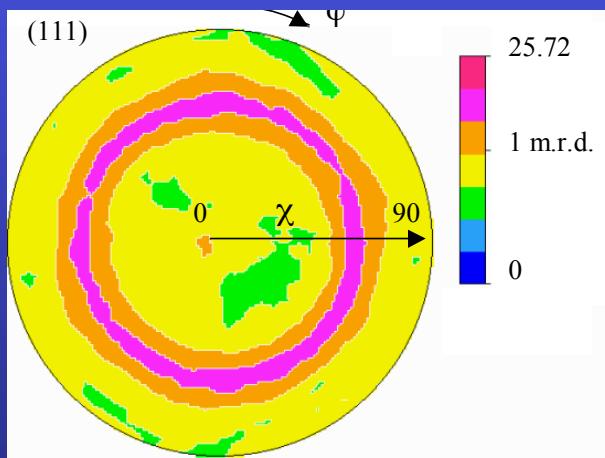
# Ferroelectric PCT films

J. Ricote, DMF-Madrid

## thin films:

$(\text{Ca}_{0.24}\text{Pb}_{0.76})\text{TiO}_3$  sol-gel synthesised solutions deposited by spin coating on a substrate of Pt/TiO<sub>2</sub>/Si, with and without a treatment at 650°C for 30 min.

All films are crystallised at 700°C for 50 s by Rapid Thermal Processing (RTP; 30°C/s). A series is also recrystallised at 650°C for 1 to 3 h.

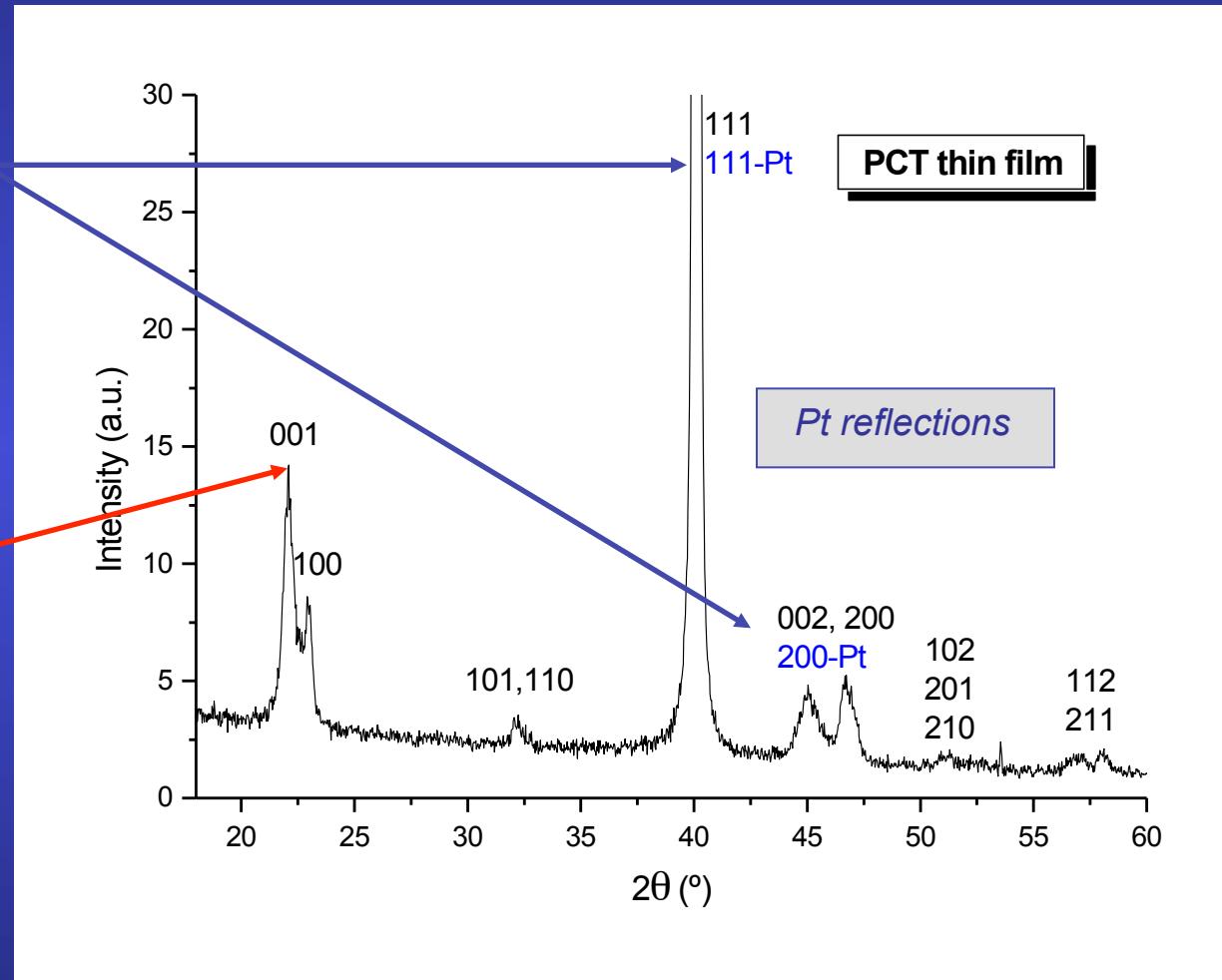


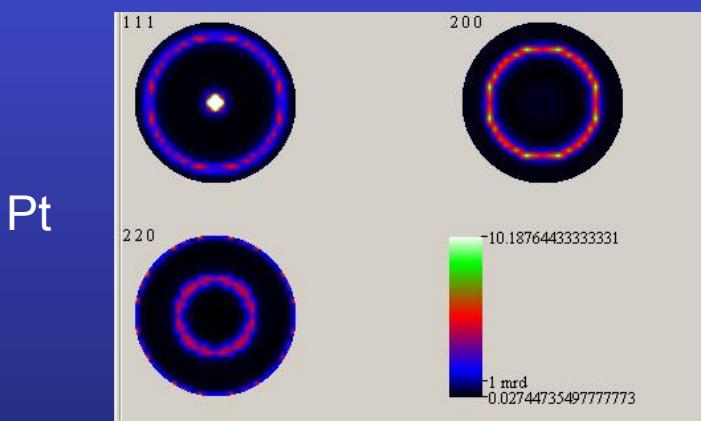
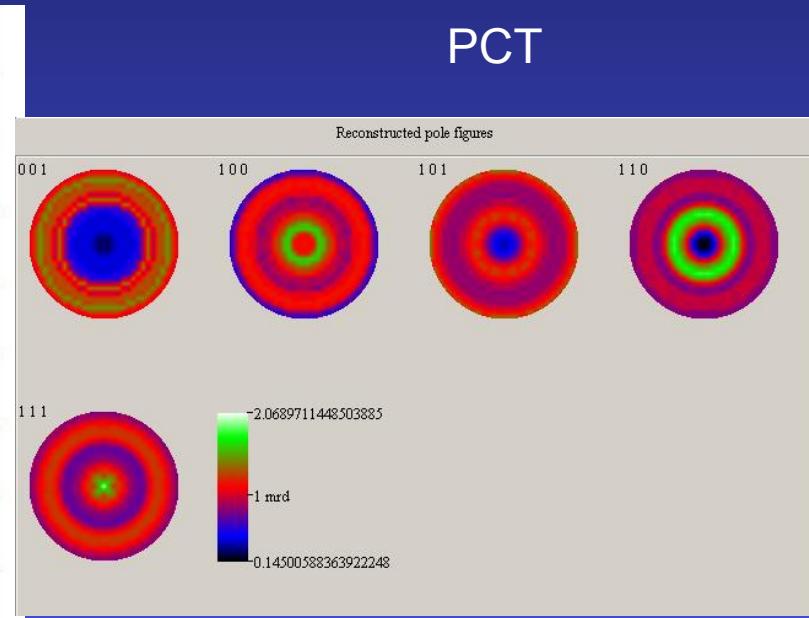
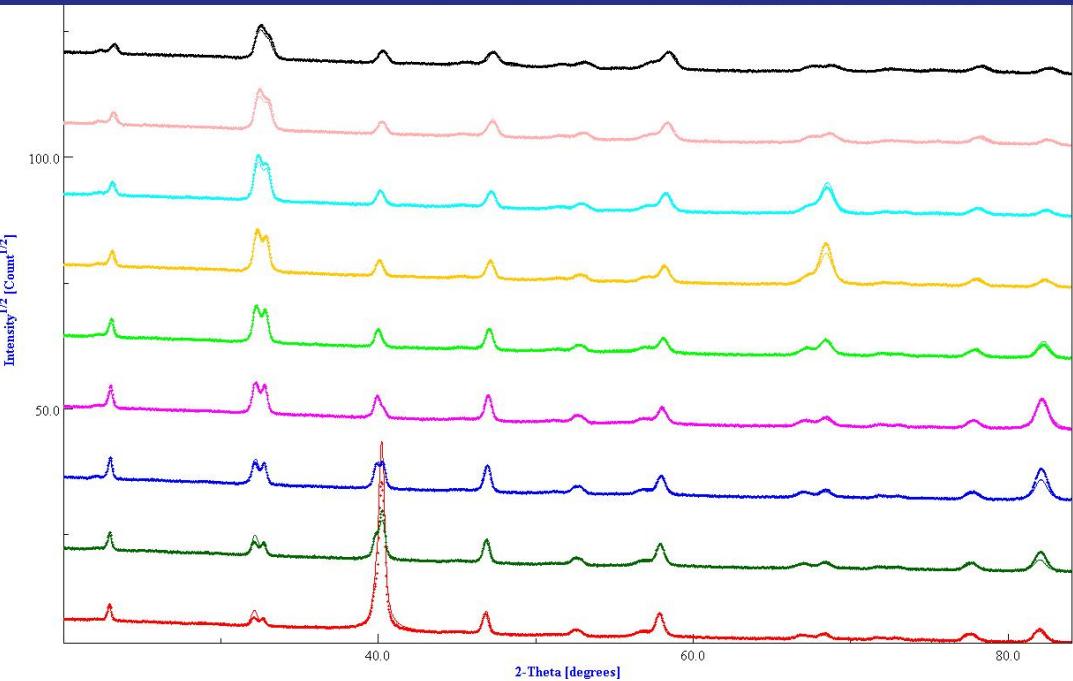
# Limitations of the simple Quantitative Texture Analysis

Structural parameters are difficult to obtain due to:

**Substrate influence:**  
overlapping of reflections  
from the film and the  
substrate

**TEXTURE effects:**  
peaks that do not appear at  
low  $\chi$  angles



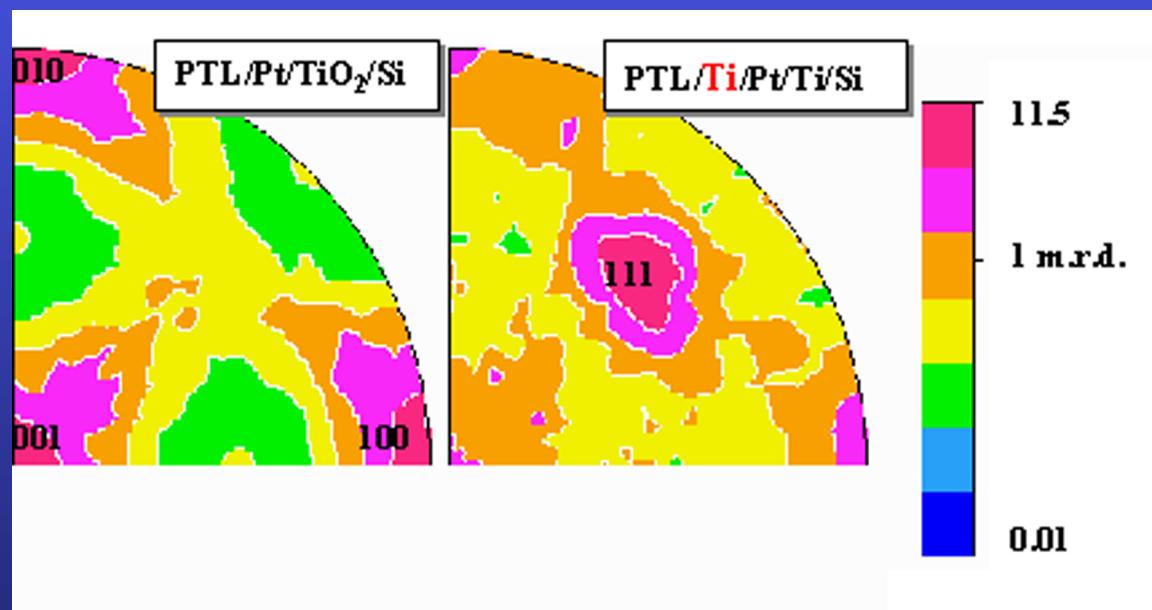


$a = 3.9108(1) \text{ \AA}$   
 $T = 457(3) \text{ \AA}$   
 $t_{\text{iso}} = 458(3) \text{ \AA}$   
 $\varepsilon' = 0.0032(1) \text{ rms}$

$a = 3.9156(1) \text{ \AA}$   
 $c = 4.0497(3) \text{ \AA}$   
 $T = 2525(13) \text{ \AA}$   
 $t_{\text{iso}} = 390(7) \text{ \AA}$   
 $\varepsilon = 0.0067(1) \text{ rms}$

$R_w = 13\%; R_B = 12\%; R_{\text{exp}} = 22\% \text{ (Rietveld)}$   
 $R_w = 5\%; R_B = 6\% \text{ (E-WIMV)}$

Atom	Occupancy	x	y	z
Pb	0.76	0.0	0.0	0.0
Ca	0.24	0.0	0.0	0.0
Ti	1.0	0.5	0.5	0.477(2)
O1	1.0	0.5	0.5	0.060(2)
O2	1.0	0.0	0.5	0.631(1)



## Structural parameters

### Pt layer

	a (Å)	thickness (nm)	R factors (%)
non-treated substrate			
Pt	3.9108(1)	45.7(3)	$R_w=13, R_B=12, R_{exp}=22$
annealed substrate			
Pt	3.9100(4)	46.4(3)	$R_w=8, R_B=14, R_{exp}=21$
Pt (Recryst. 1h)	3.9114(2)	47.8(3)	$R_w=9, R_B=20, R_{exp}=21$
Pt (Recryst. 2h)	3.9068(1)	46.9(3)	$R_w=9, R_B=14, R_{exp}=22$
Pt (Recryst. 3h)	3.9141(4)	47.5(9)	$R_w=27, R_B=12, R_{exp}=21$

*Annealing of the substrate does not introduce significant variations on the structure of the Pt layer*

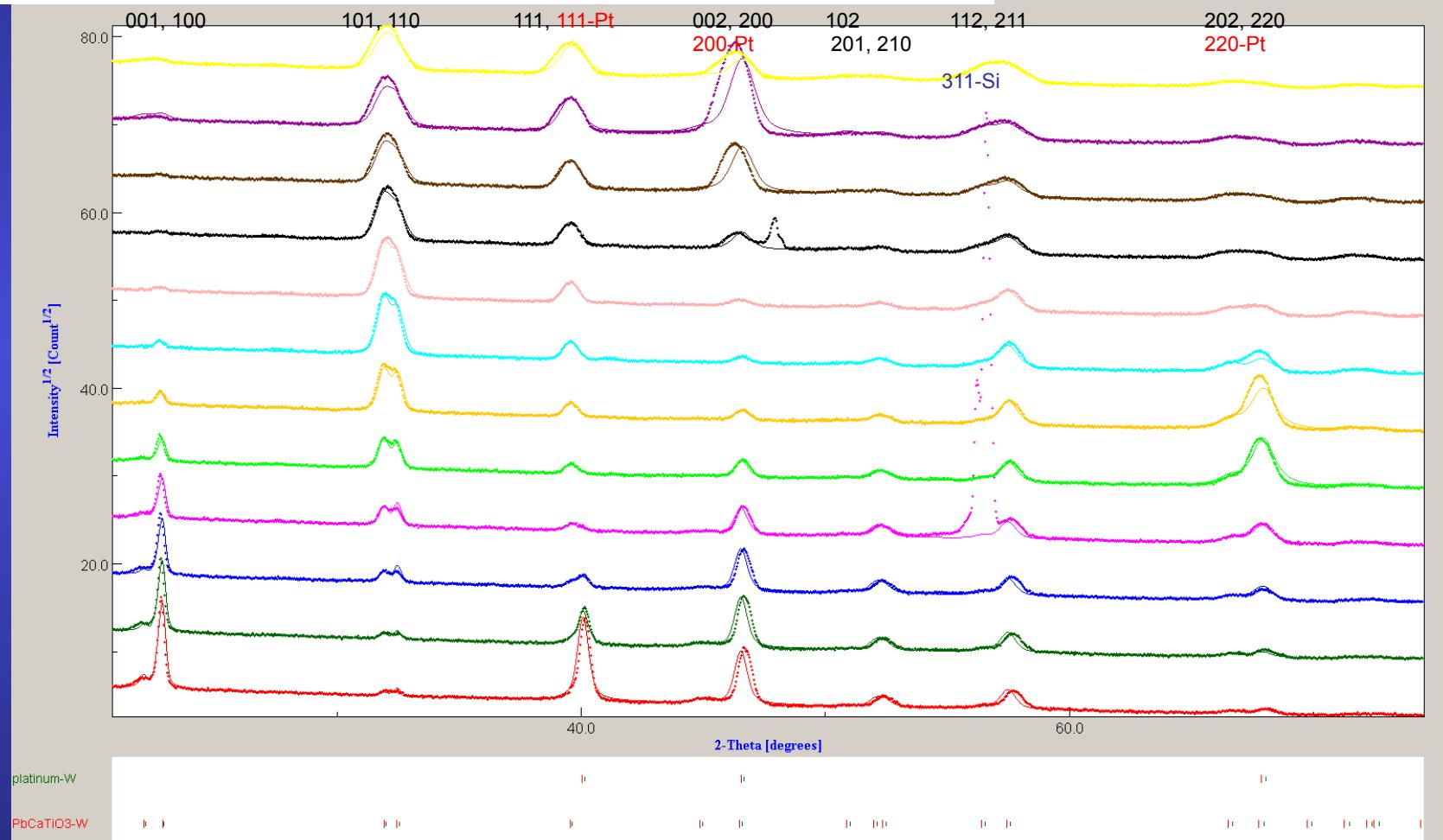
### PTC film

	a (Å)	c (Å)	thickness (nm)
on non-treated substrate			
PCT	3.9156(1)	4.0497(6)	272.5(13)
on annealed substrate			
PCT	3.8920(6)	4.0187(8)	279.0(9)
PCT (Recryst. 1h)	3.8929(2)	4.0230(4)	266.1(11)
PCT (Recryst. 2h)	3.8982(2)	4.0227(4)	258.4(9)
PCT (Recryst. 3h)	3.9001(4)	4.0228(11)	253.6(29)

*Recrystallisation reduces the stress on the film, and, increases the lattice parameters*

# Structural, microstructural and texture quantitative characterisation of ferroelectric thin films by the combined method

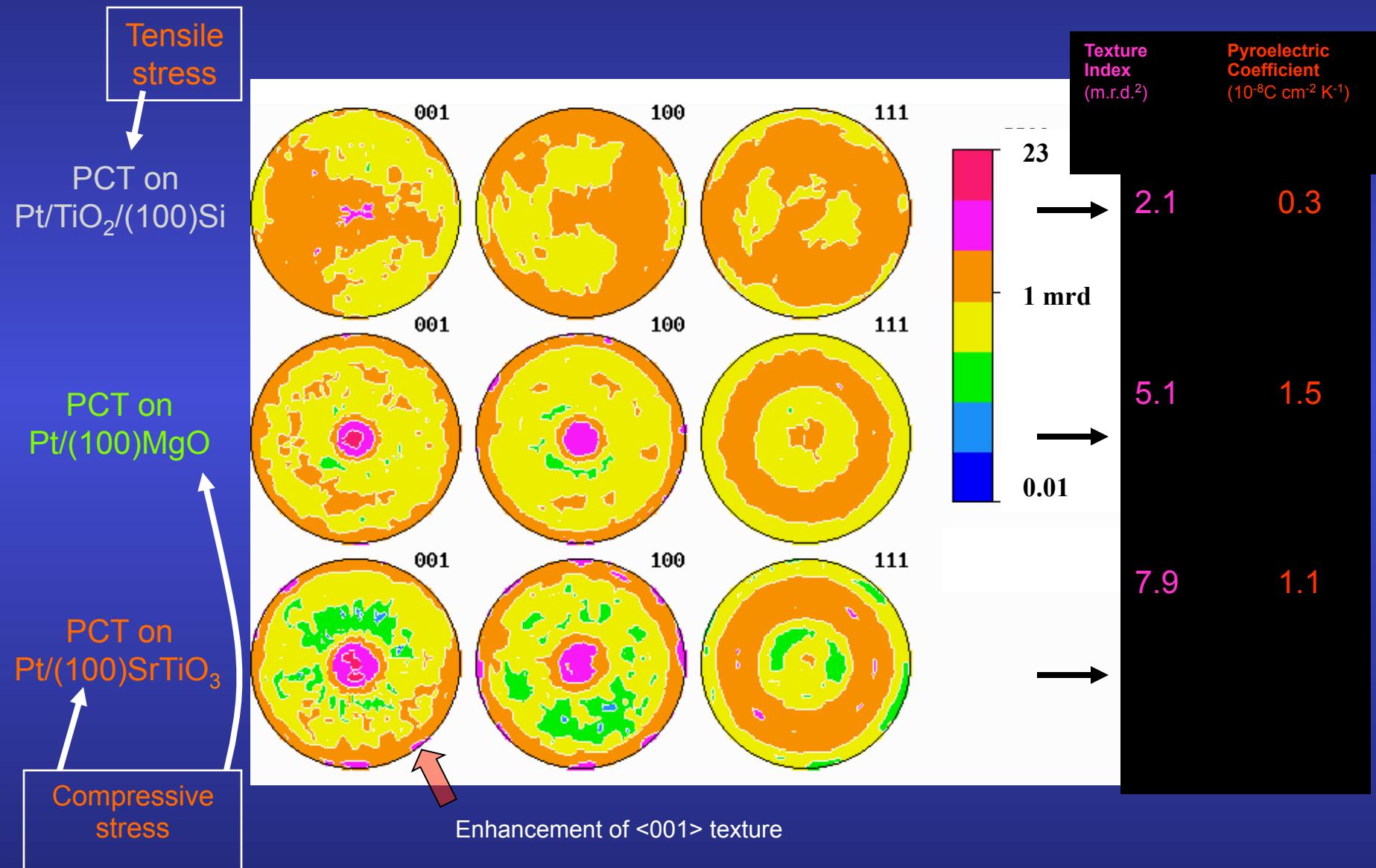
Analysis of the X-ray diffraction diagrams of a PCT film on Pt/TiO<sub>2</sub>/Si



$$R_W = 13\%; R_B = 12\%; R_{exp} = 22\%. \text{(Rietveld)}$$

$$R_W = 5\%; R_B = 6\% \text{ (E-WIMV)}$$

# Substrate influence on Residual Stress and Texture

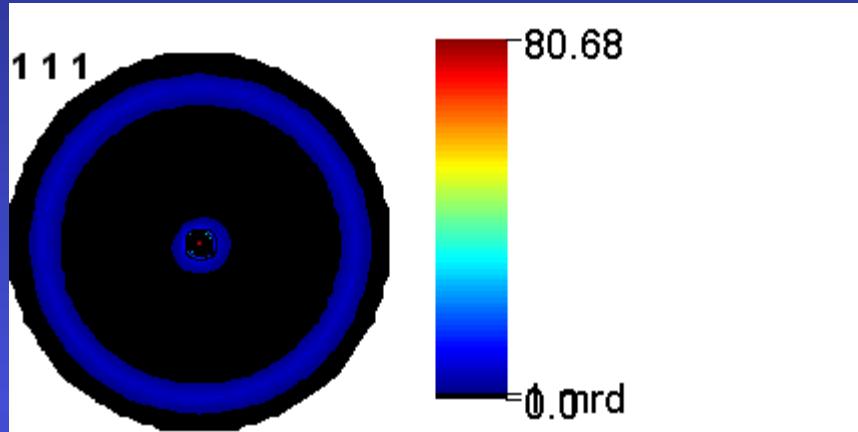


Compliance coefficients [ $10^{-3}$ GPa $^{-1}$ ]	PbTiO <sub>3</sub> single crystal (data set A)	Film random orientation	PCT-Si <001> contrib. $\approx$ 17%	PLT <001> contrib. $\approx$ 49%	PCT-Mg <001> contrib. $\approx$ 68%
S <sub>11</sub>	6.5	10.1	10.5	10.0	9.7
S <sub>22</sub>	6.5	10.0	10.5	10.0	9.7
S <sub>33</sub>	33.3	9.8	9.0	10.3	11.3
S <sub>44</sub>	14.5	13.2	12.8	12.9	13.1
S <sub>55</sub>	14.5	13.2	12.8	13.0	13.1
S <sub>66</sub>	9.6	13.4	14.0	13.5	12.7
S <sub>12</sub>	-0.35	-3.3	-3.5	-3.2	-3.0
S <sub>21</sub>	-0.35	-3.3	-3.5	-3.2	-3.0
S <sub>13</sub>	-7.1	-3.2	-3.1	-3.4	-3.6
S <sub>31</sub>	-7.1	-3.2	-3.1	-3.4	-3.6
S <sub>23</sub>	-7.1	-3.2	-3.1	-3.4	-3.6
S <sub>32</sub>	-7.1	-3.2	-3.1	-3.4	-3.6
S <sub>33</sub> /S <sub>11</sub>	5.1	0.97	0.86	1.03	1.16
S <sub>13</sub> /S <sub>12</sub>	20.3	0.97	0.89	1.06	1.20

Geometric mean average + biaxial stress state

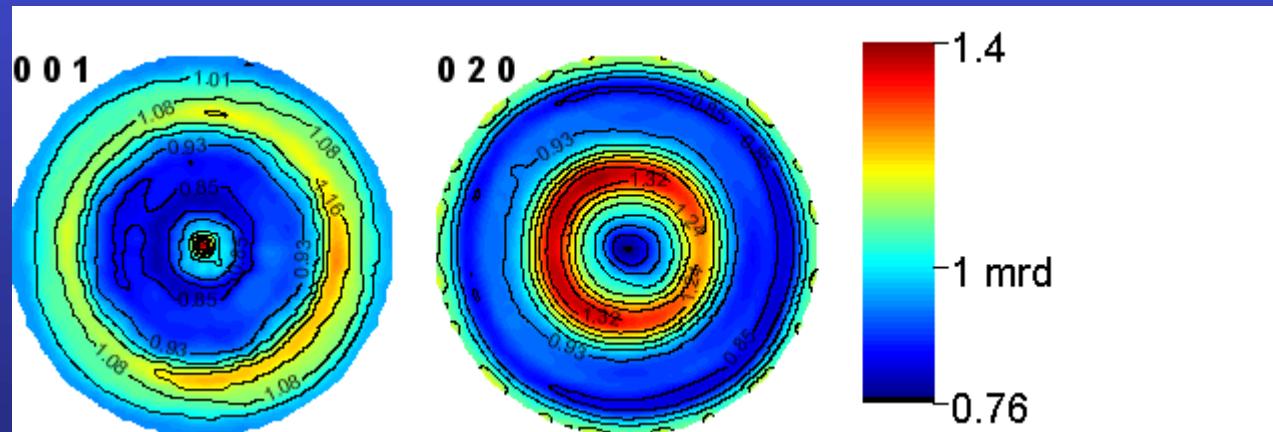
# Ferroelectric PMN-PT films

J. Ricote, DMF-Madrid



Pt  
 $a = 3.91172(1)$  Å  
 $T = 583(5)$  Å  
 $t_{iso} = 960(1)$  Å  
 $\varepsilon = 0.0032(1)$  rms  
 $\sigma_{11} = 0.639(1)$  GPa  
 $\sigma_{22} = 0.651(1)$  GPa  
 $\sigma_{12} = -0.009(1)$  GPa

$\text{Pb}_{0.7}(\text{Mg}_{1/3}\text{Nb}_{2/3})\text{O}_3-\text{Pb}_{0.3}\text{TiO}_3/\text{TiO}_2/\text{Pt/Si-(100)}$



$a = 5.67858(9)$  Å  
 $b = 5.69038(9)$  Å  
 $c = 3.99558(4)$  Å  
 $\beta = 90.392(1)$  Å  
 $T = 1322(9)$  Å  
 $t_{iso} = 1338(2)$  Å  
 $\varepsilon = 0.0067(1)$  rms

# *Si nanocrystalline thin films*

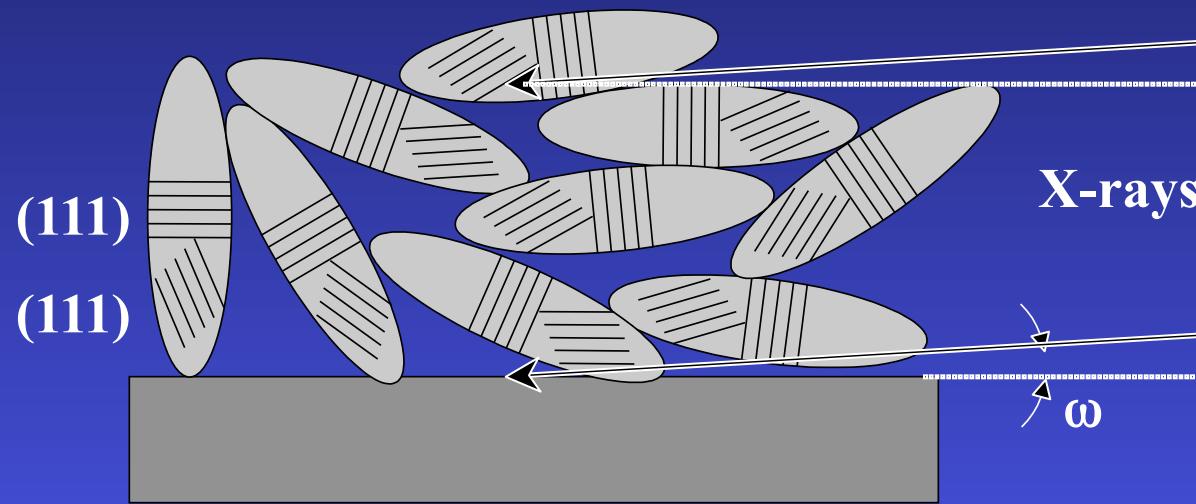
M. Morales, SIFCOM-Caen

## **Silicon thin films deposition by reactive magnetron sputtering:**

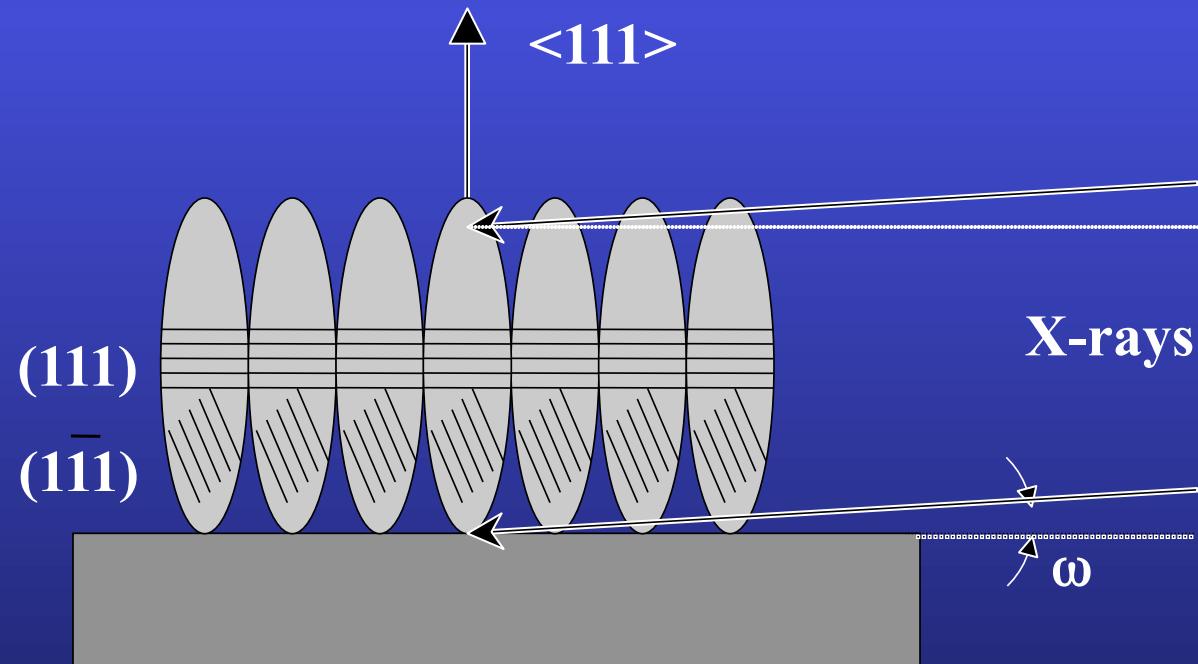
- ↳ power density 2W/cm<sup>2</sup>
- ↳ total pressure:  $p_{\text{total}} = 10^{-1}$  Torr
- ↳ plasma mixture: H<sub>2</sub> / Ar, pH<sub>2</sub> / p<sub>total</sub> = 80 %
- ↳ temperature: 200°C
- ↳ substrates: amorphous SiO<sub>2</sub> (a-SiO<sub>2</sub>)  
(100)-Si single-crystals
- ↳ target-substrate distance (d)
  - a-SiO<sub>2</sub> substrates: d = 4, 6, 7, 8, 10, 12 cm  
films A, B, C, D, E, F
  - (100)-Si: d = 6, 12 cm  
films G, H

Aim: quantum confinement, photoluminescence properties

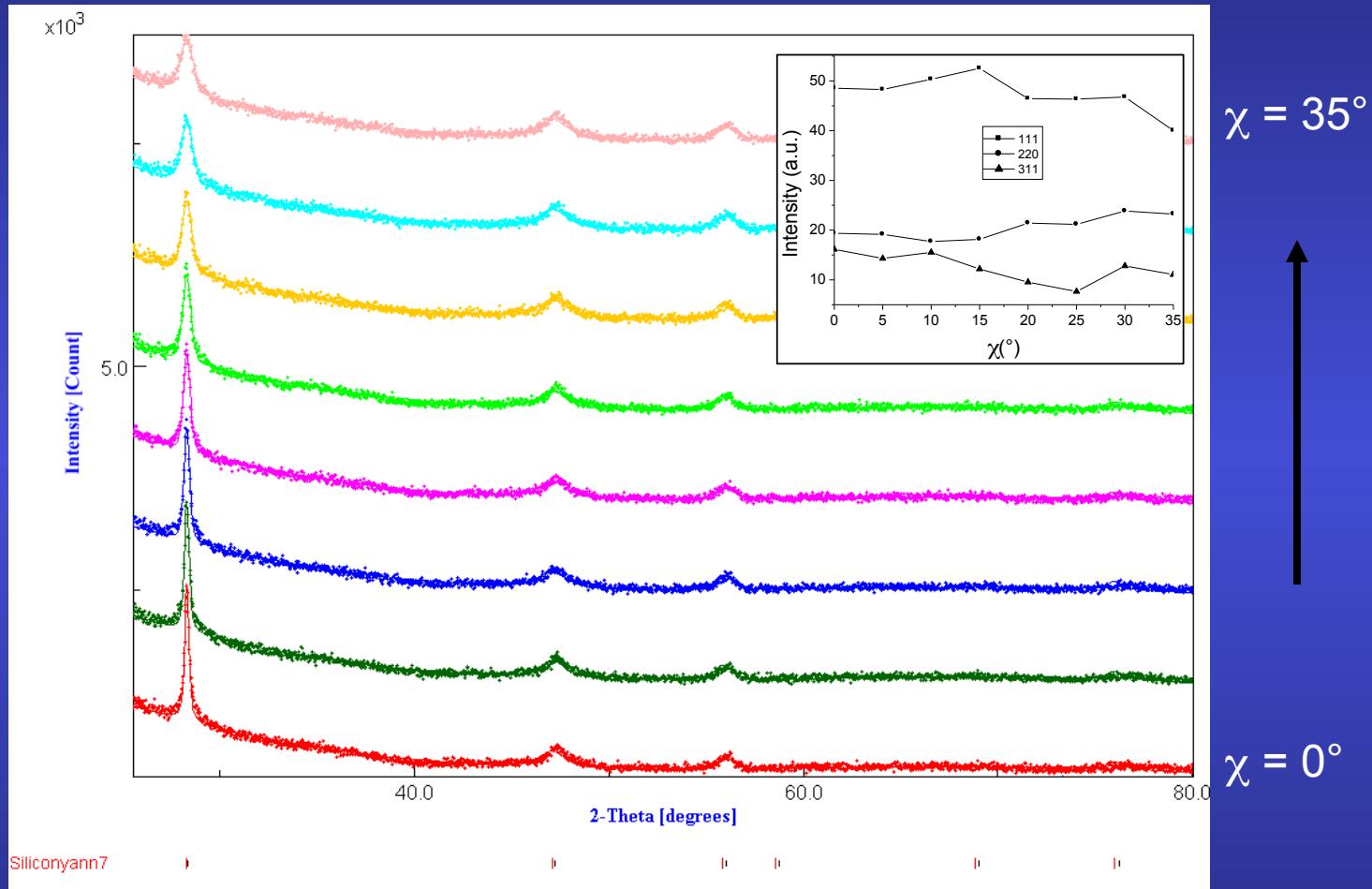
Isotropic



Textured



# Typical refinement

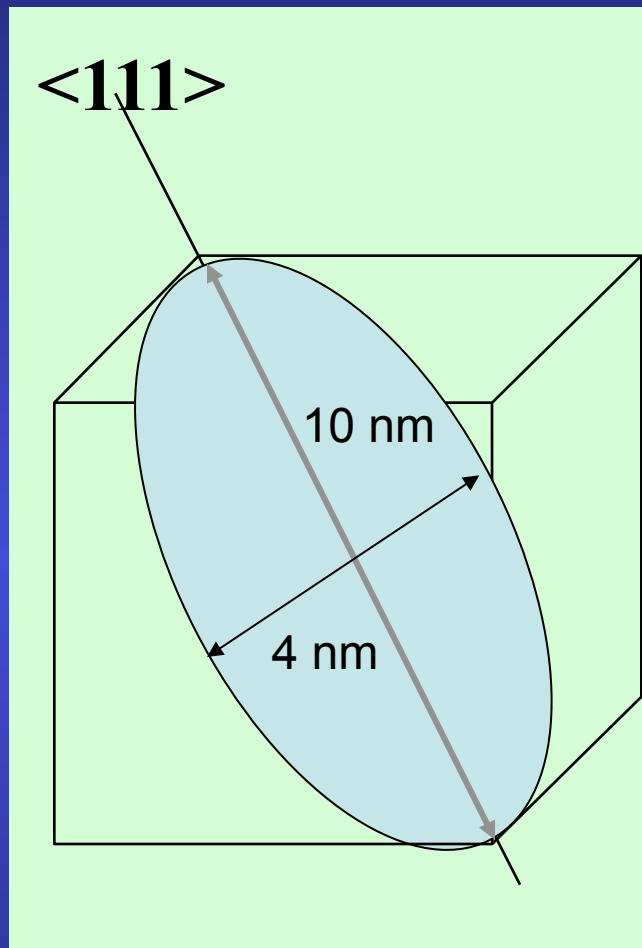


broad, anisotropic diffracted lines, textured samples

# Refinement Results

Sample	d (cm)	a (Å)	RX thickness (nm)	Anisotropic sizes (Å)			Texture parameters			Reliability factors (%)			
				<111>	<220>	<311>	Maximum (m.r.d.)	minimum (m.r.d.)	Texture index F <sup>2</sup> (m.r.d <sup>2</sup> )	RP <sub>0</sub>	R <sub>w</sub>	R <sub>B</sub>	R <sub>exp</sub>
A	4	5.4466 (3)	—	94	20	27	1.95	0.4	1.12	1.72	4.0	3.7	3.5
B	6	5.4439 (2)	711 (50)	101	20	22	1.39	0.79	1.01	0.71	4.9	4.3	4.2
C	7	5.4346 (4)	519 (60)	99	40	52	1.72	0.66	1.05	0.78	4.3	4.0	3.9
D	8	5.4461 (2)	1447 (66)	100	22	33	1.57	0.63	1.04	0.90	5.5	4.6	4.5
E	10	5.4462 (2)	1360 (80)	98	20	25	1.22	0.82	1.01	0.56	5.0	3.9	4.0
F	12	5.4452 (3)	1110 (57)	85	22	26	1.59	0.45	1.05	1.08	4.2	3.5	3.7
G	6	5.4387 (3)	1307 (50)	89	22	28	1.84	0.71	1.01	1.57	5.2	4.7	4.2
H	12	5.4434 (2)	1214 (18)	88	22	24	2.77	0.50	1.12	2.97	5.0	4.5	4.3

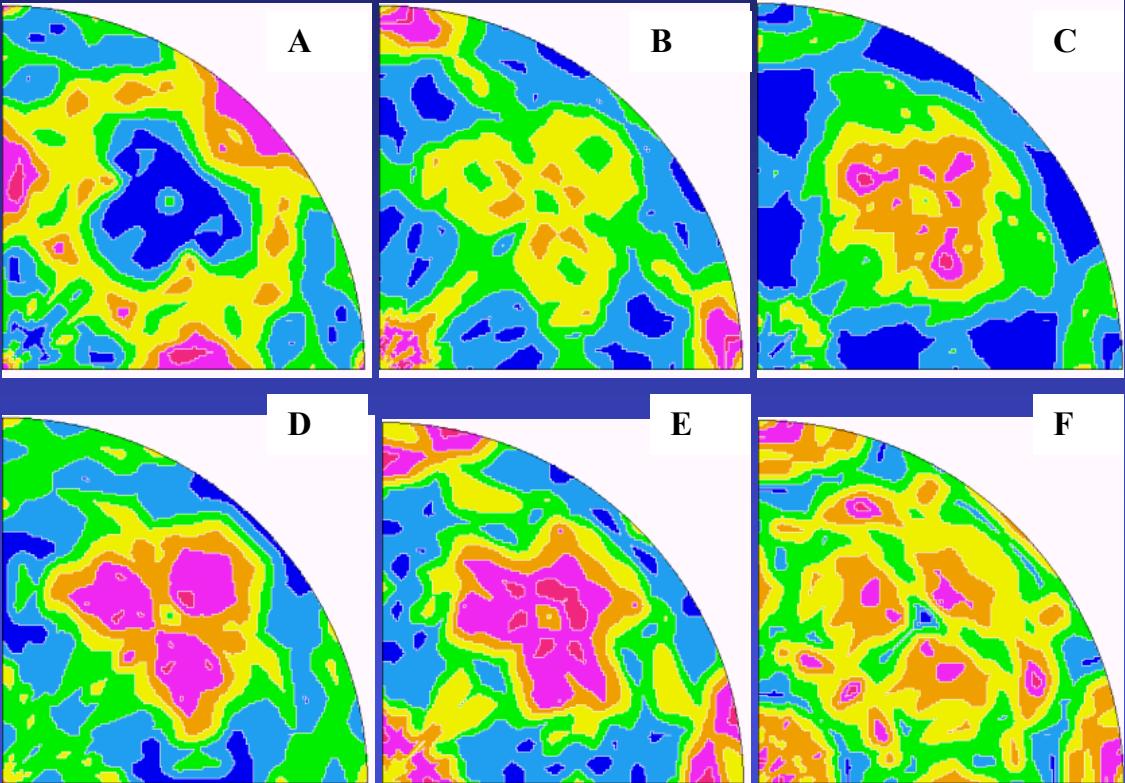
# Mean anisotropic shape



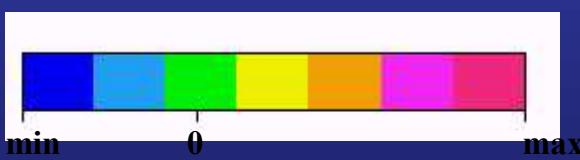
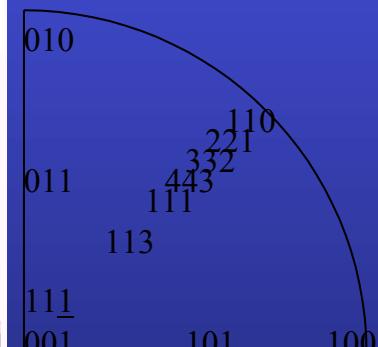
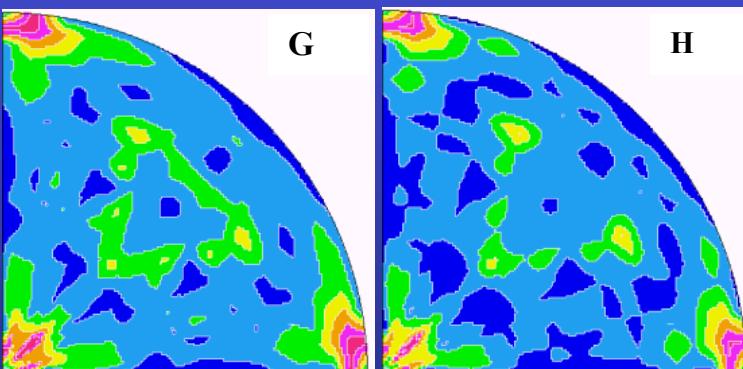
Schematic of the mean crystallite shape for Sample D represented in a cubic cell, as refined using the Popa approach and exhibiting a strong elongation along  $<111>$ , and TEM image

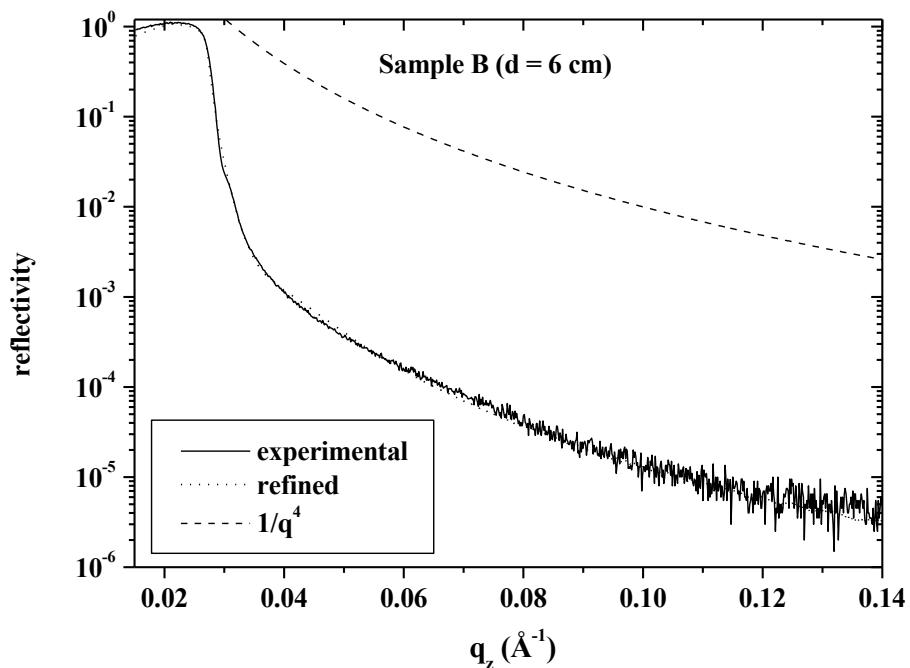
# 001 Inverse Pole Figures

a-SiO<sub>2</sub>



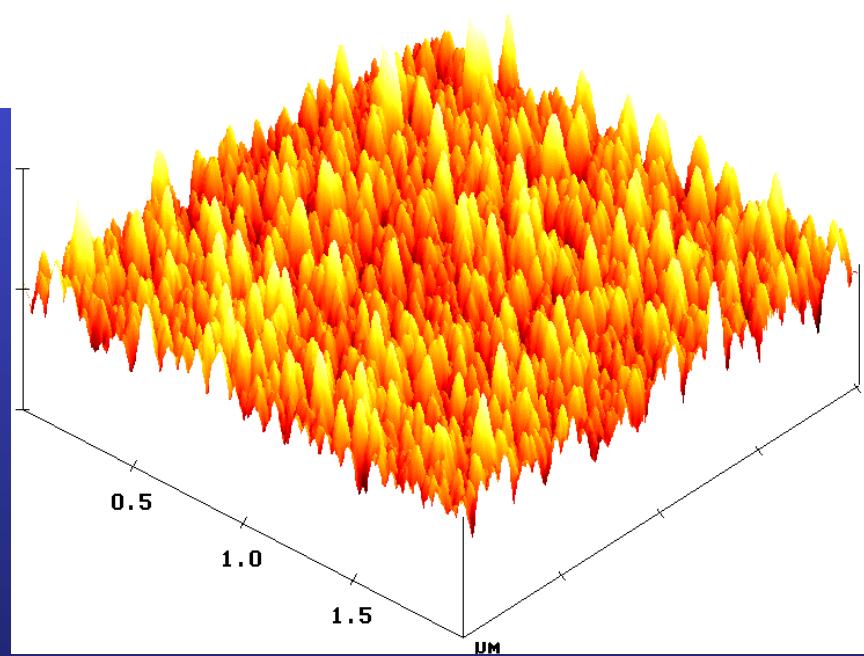
(100)-Si

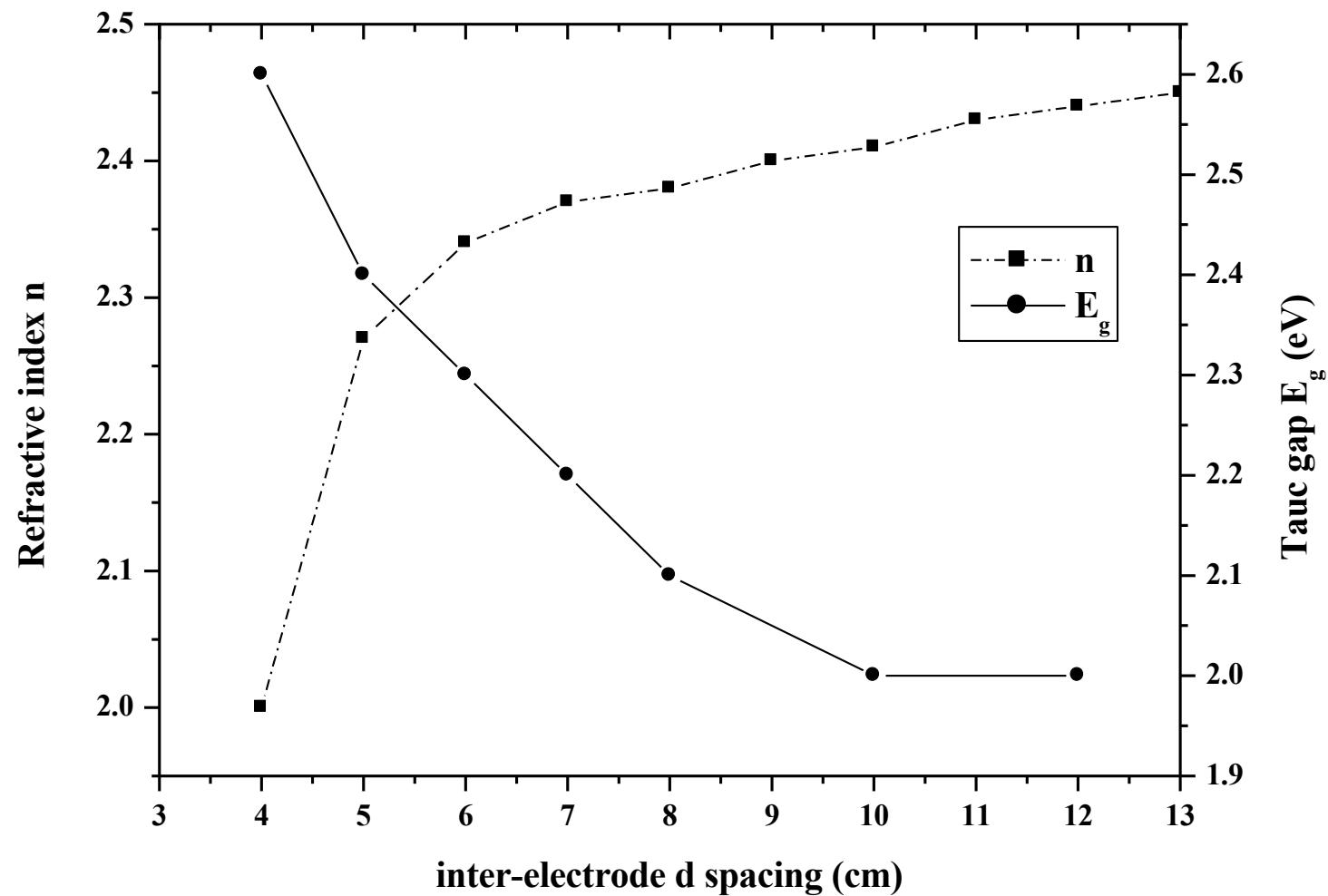




XRR:  
Roughness  
governed

AFM:  
homogeneous  
roughness

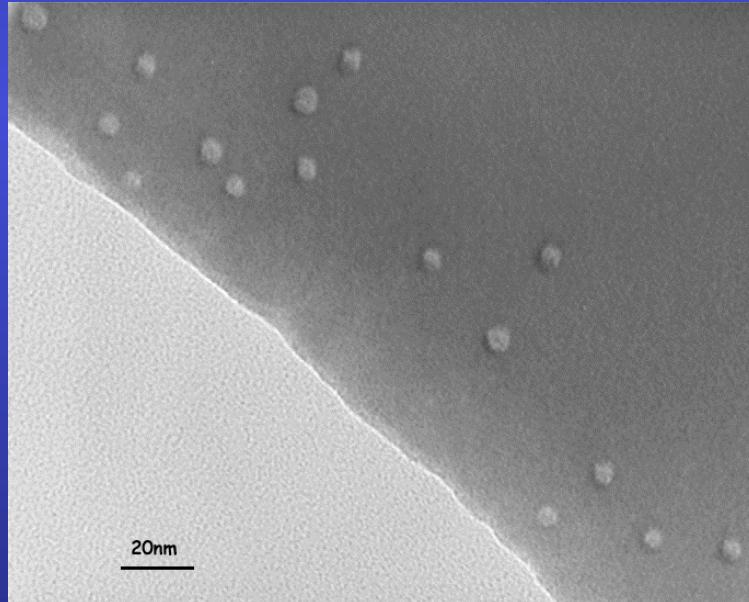




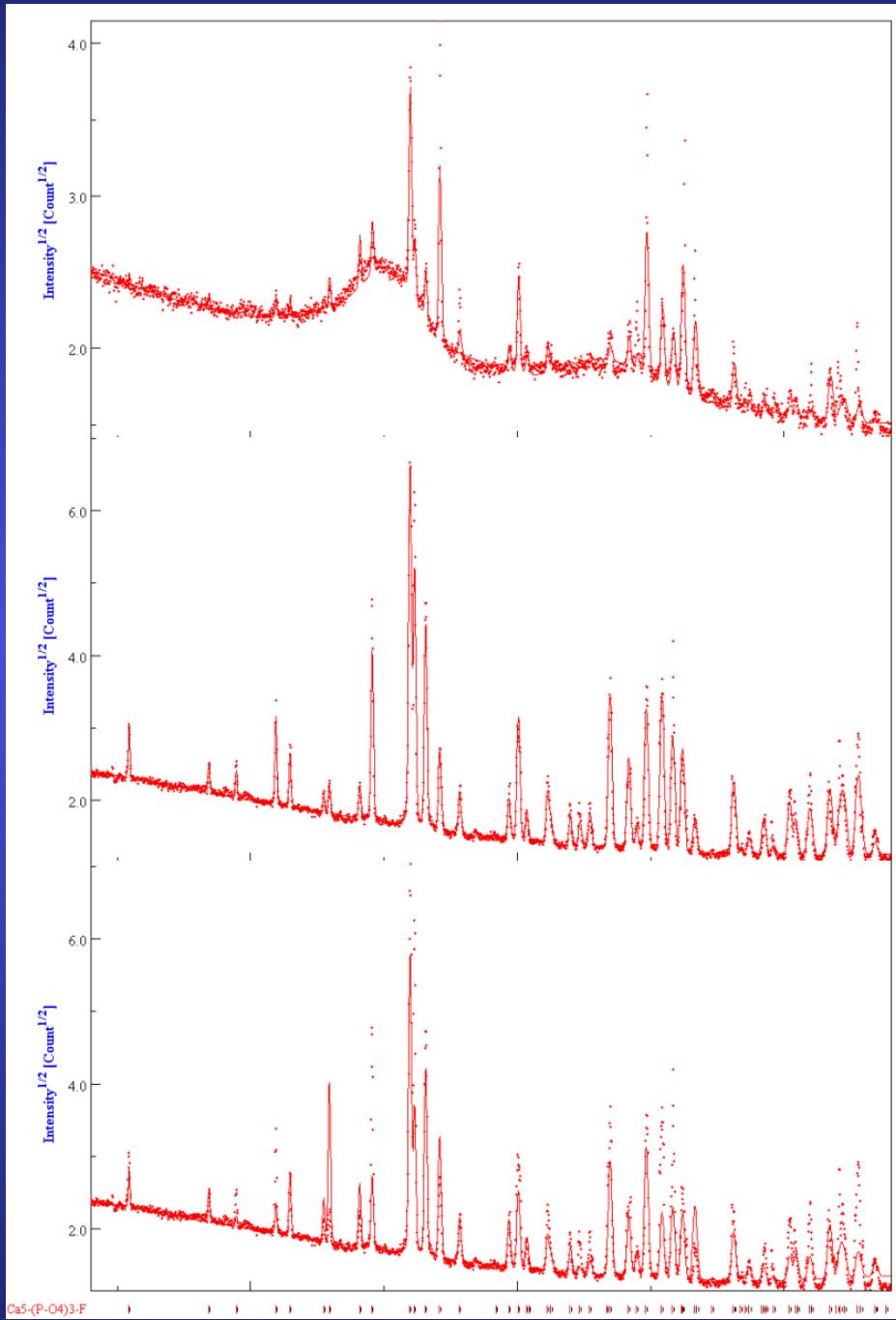
# *Irradiated FluorApatite (FAp) ceramics*

S. Miro, PhD CRISMAT

Self-recrystallisation under irradiation, depending on  $\text{SiO}_4$  /  $\text{PO}_4$  ratio (FAp / Nd-Birtholite) and on irradiating species



TEM of FAp  
irradiated with 70  
MeV,  $10^{12}$  Kr cm $^{-2}$   
ions



texture corrected,  
 $10^{13}$  Kr cm<sup>-2</sup>

Virgin, with texture  
correction

Virgin, no texture  
correction

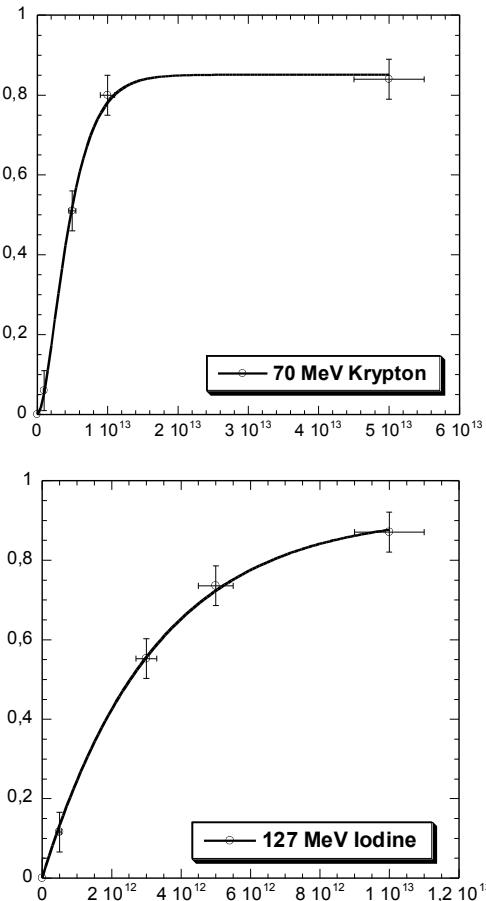
Fluence (ions.cm <sup>-2</sup> )	Vc/V (%)	A (Å)	c (Å)	$\langle t \rangle$ (nm)	$\Delta a/a_0$ (%)	$\Delta c/c_0$ (%)	R <sub>w</sub> (%)	R <sub>B</sub> (%)
0	100	9.3365(3)	6.8560(5)	294(22)	-	-	14.6	9.1
<b>Kr</b>								
$10^{11}$	100	-	-	-	-	-		
$10^{12}$	100	-	-	-	-	-		
$5.10^{12}$	49(1)	9.3775(9)	6.8912(8)	294(20)	0.44	0.53	24	15
$10^{13}$	20(1)	9.4236(5)	6.9105(5)	291(20)	0.94	0.82	9.9	6
$5.10^{13}$	14(1)	9.3160(4)	6.8402(5)	294(22)	-0.21	-0.22	10.5	5.9
<b>I</b>								
$10^{11}$	-	-	-	-	-	-		
$5.10^{11}$	86(2)	9.3603(3)	6.8790(5)	90(10)	0.26	0.35	23.9	15.1
$10^{12}$	-	-	-	-	-	-		
$3.10^{12}$	47(2)	9.3645(3)	6.8840(5)	91(6)	0.30	0.42	13.3	9
$5.10^{12}$	29.2(5)	9.3765(5)	6.8881(6)	77(11)	0.44	0.48	10.4	7.3
$10^{13}$	13.2(2)	9.3719(4)	6.8857(6)	82(9)	0.38	0.45	6.7	4.9

Single impact model associated to crystal size reduction

Cell parameters and volume increase, then relax

Amorphisation / recrystallisation competition: single or double impact

# Amorphous/crystalline volume fraction (damaged fraction $F_d = V_a / V$ ) as determined by x-ray diffraction



Fitting parameters	Krypton		Iodine
	Single impact $F_d = B(1 - \exp(-A\Phi_t))$	Double impact $F_d = B(1 - (1 + A\Phi_t) \exp(-A\Phi_t))$	Single impact $F_d = B(1 - \exp(-A\Phi_t))$
$A = \pi R^2 (\text{cm}^2)$	$1.85 \pm 0.15 10^{-13}$	$4.1 \pm 0.15 10^{-13}$	$3.3 \pm 0.15 10^{-13}$
Radius R (nm)	$2.4 \pm 0.2$	3.6	3.2
B (Max.damage rate)	0.87	$0.85 \pm 0.2$	$0.92 \pm 0.2$
$\chi^2$	0.013	0.0006	0.0004

← B

## *Conclusions*

- a) Texture affects phase ratio and structure determination
- b) Microstructure (crystallite size) affects texture (go to a)
- c) Stresses shift peaks then affects structure and texture determination
- d) Combined analysis may be a solution, unless you can destroy your sample or are not interested in macroscopic anisotropy ...
- e) If you think you can destroy it, perhaps think twice
- f) more information is always needed: local probes ...
- g) [www.ecole.ensicaen.fr/~chateign/texture/combined.pdf](http://www.ecole.ensicaen.fr/~chateign/texture/combined.pdf)