

Texture development in Nd-Fe-B and Nd-Fe-V alloys by hot forging in view of improving permanent Magnet properties

D. Chateigner

CRISMAT-ENSICAEN, Caen, France

M. Morales

SIFCOM-ENSICAEN, Caen, France

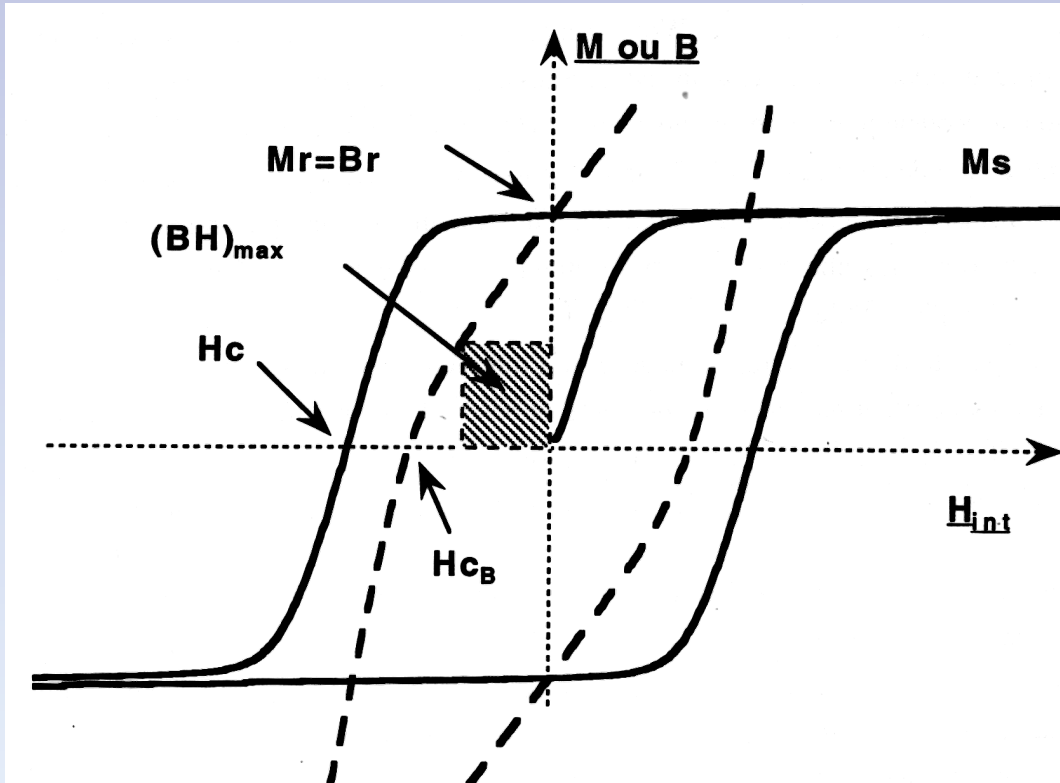
S. Rivoirard, I. Popa, P. de Rango, D. Fruchart
CRETA and Cristallographie-CNRS, Grenoble, France

B. Ouladdiaf

Institut Laue Langevin, Grenoble, France

- Some intrinsic magnetic and extrinsic magnet properties
- QTA and anisotropic magnetisation curves: $\text{ErMn}_4\text{Fe}_8\text{C}$ case
- Nd-Fe-B-Cu, Nd-Fe-V alloys
- conclusions

Permanent magnet characteristics



Intrinsic properties

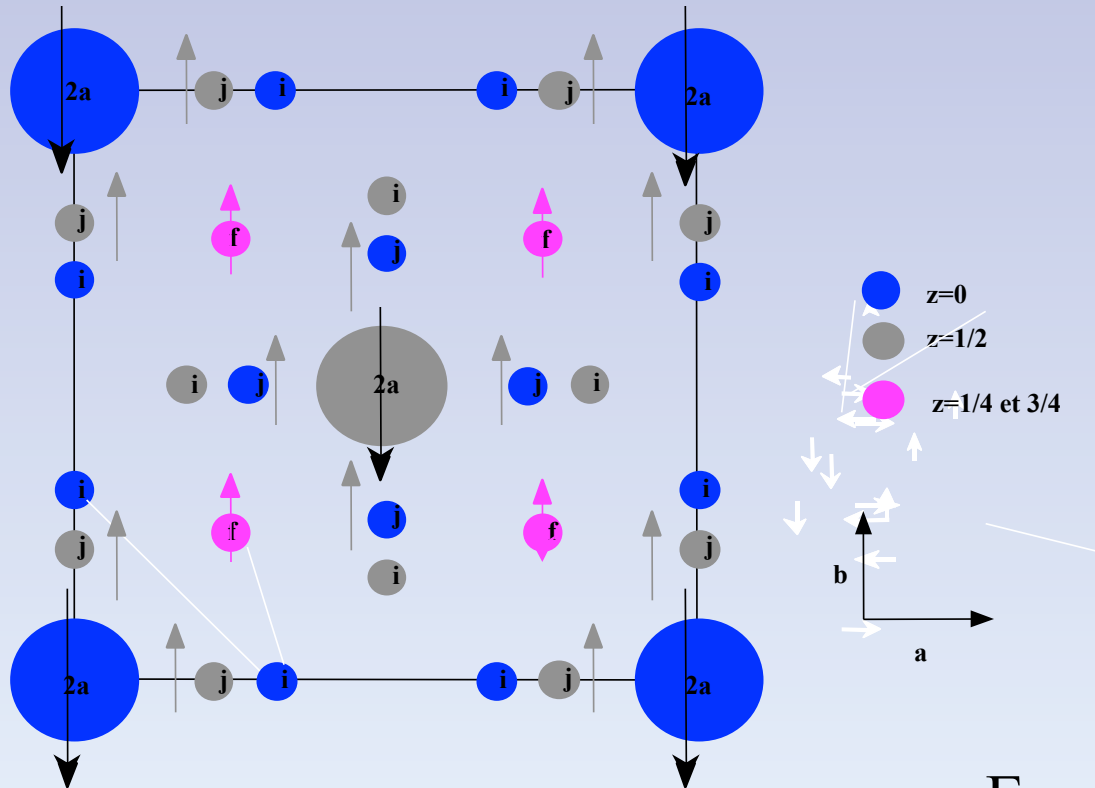
Hard magnetic phase

- Saturation magnetisation, M_s
- Magnetocrystalline anisotropy
- Curie temperature
- Anisotropy field

Extrinsic properties

- Remanence, M_r
- Coercive field, H_c
- Maximum energy product,

BH_{max}



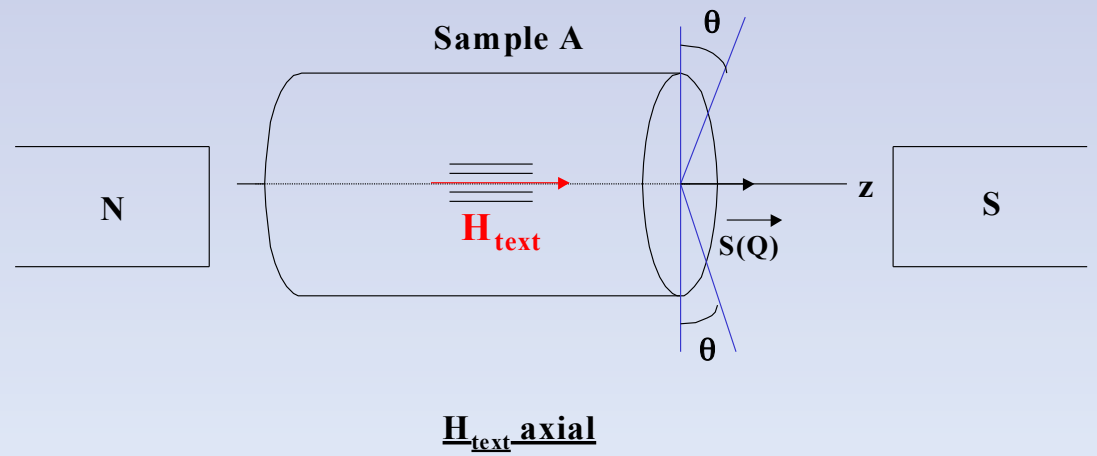
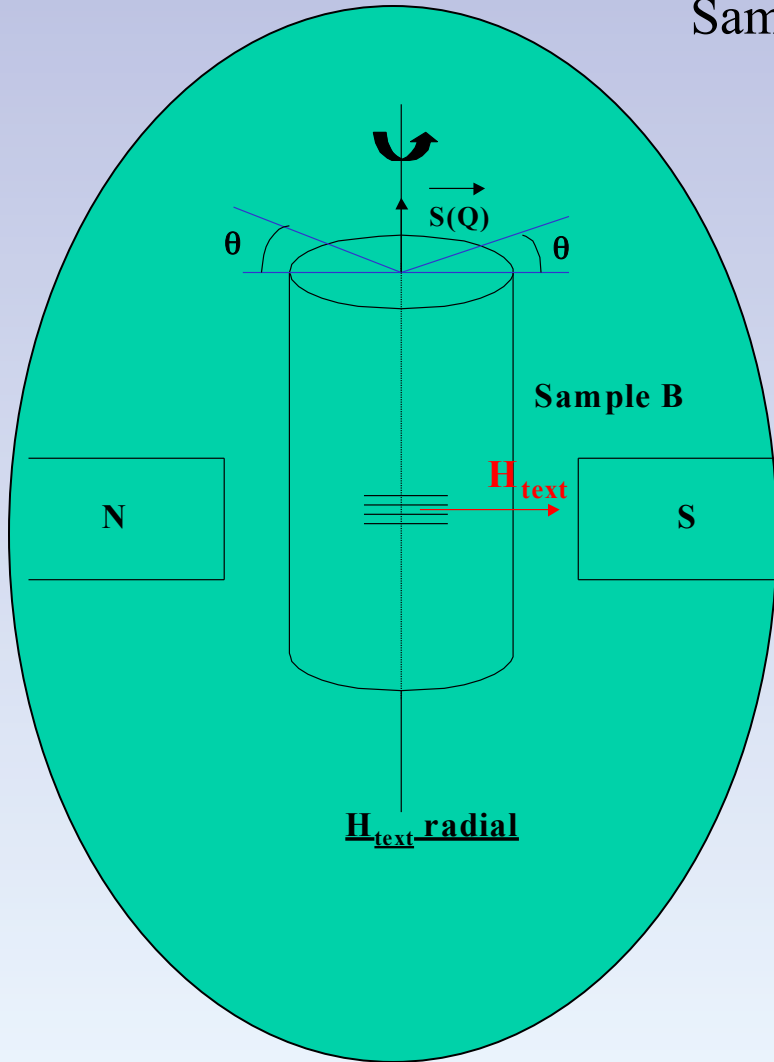
Structural determination:

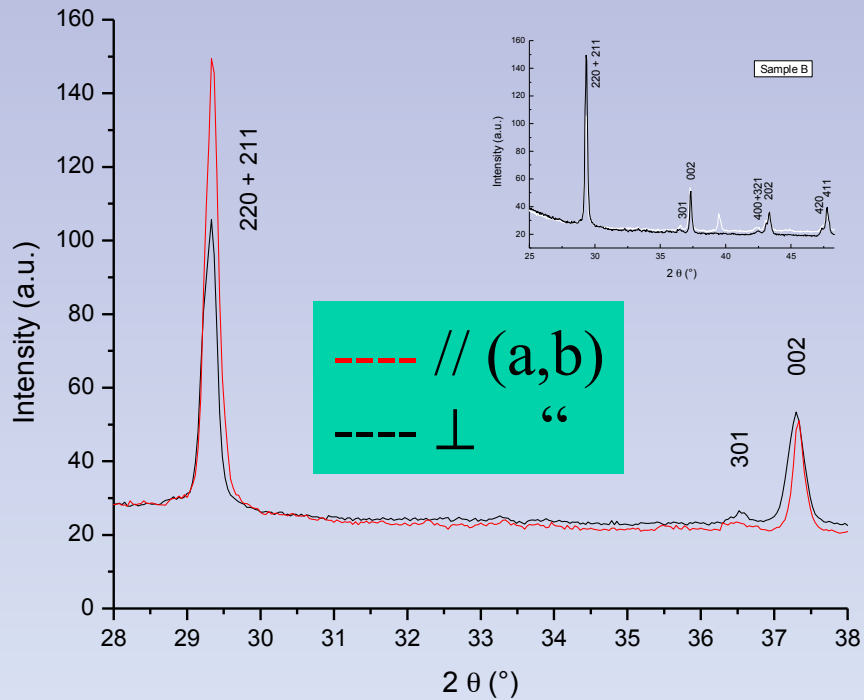
M. Morales et al.: J. Magn. And Magn. Mat. 196 (1999) 703

Easy-plane tetragonal phase
 magnetic moments in the (a,b) planes

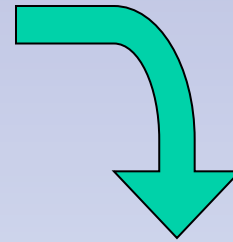
$\perp (a,b)$

$\leftarrow \mathbf{H}_{\text{meas}} \parallel \mathbf{z} \rightarrow \parallel (a,b)$
Same demagnetising factor





Quantitative Texture Analysis

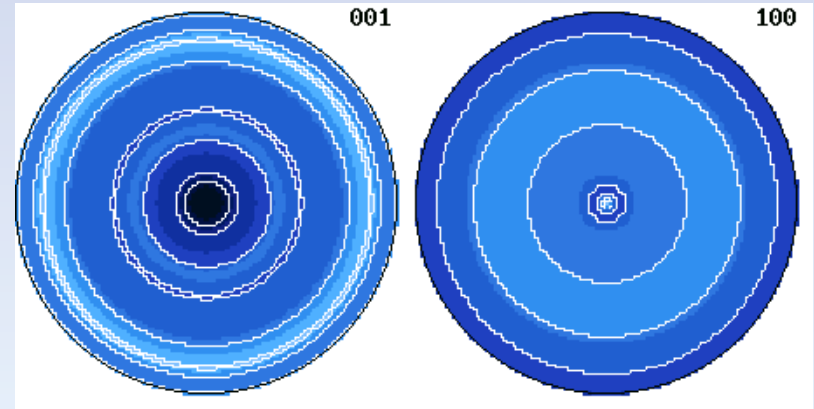


$$RP_0 = 1.2 \%$$

$$F_2 = 1.3 \text{ mrd}^2$$

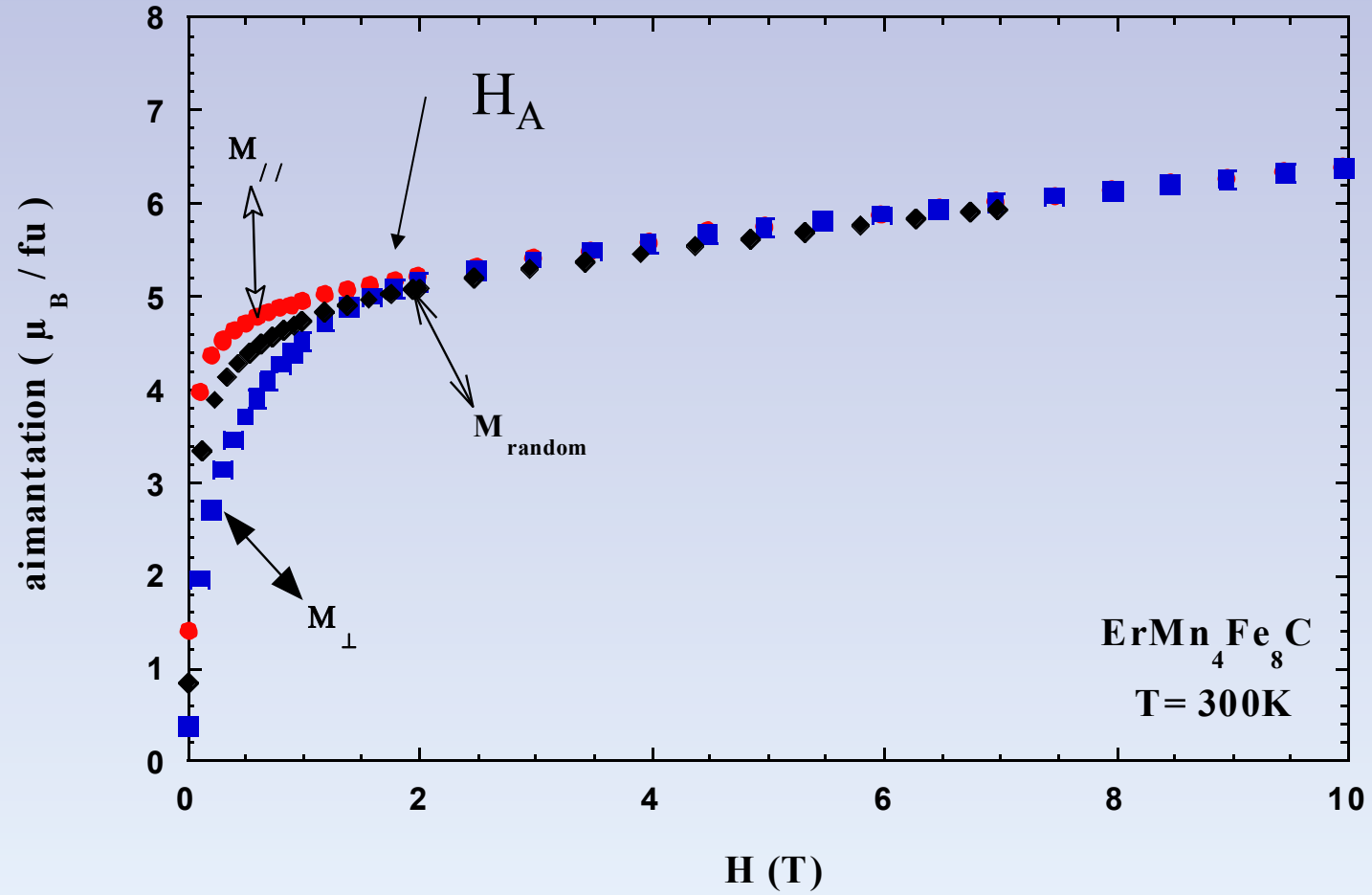
$$S = -0.13$$

max {001}: 3.9 mrd
min: 0.5 mrd

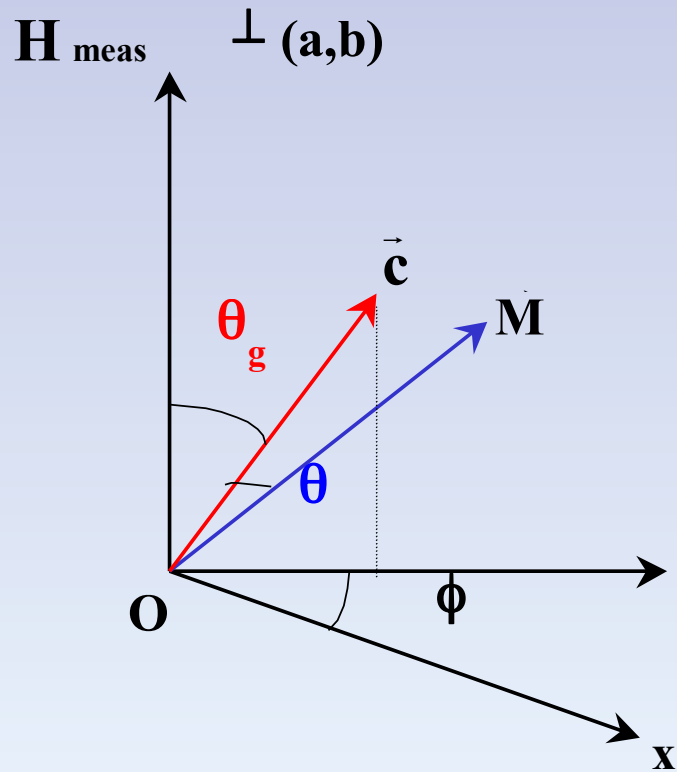


{001} radial distribution: ρ_0 (0.5 mrd) + PV (HWHM = 12°)

Anisotropic magnetisation curves



Model for M_{\perp} :



$$M(H_{\text{meas}}) = M_S \cos(\theta_g - \theta)$$

$$E(H_{\text{meas}}) = K_1 \sin^2 \theta - H M_S \cos(\theta_g - \theta)$$

anisotropy
energy

Zeeman
energy

$$\frac{dE}{d\theta} = 0 \quad \longrightarrow \quad H_{\text{meas}} = \frac{2 K_1 \sin \theta \cos \theta}{M_S \sin(\theta_g - \theta)}$$

$$H_A = 2K_1/M_S$$

$$M_S = 5.24 \mu_B/f_u$$

$$\frac{H_{\text{meas}}}{H_A} = \frac{\sin \theta \cos \theta}{\sin(\theta_g - \theta)}$$

Normalised Probability
function F , to find
c-axes in dy :

$$\int_{\theta_g=0}^{\frac{\pi}{2}} \int_{\varphi=0}^{2\pi} F(\theta_g, \varphi) \sin\theta_g d\theta_g d\varphi = 1$$

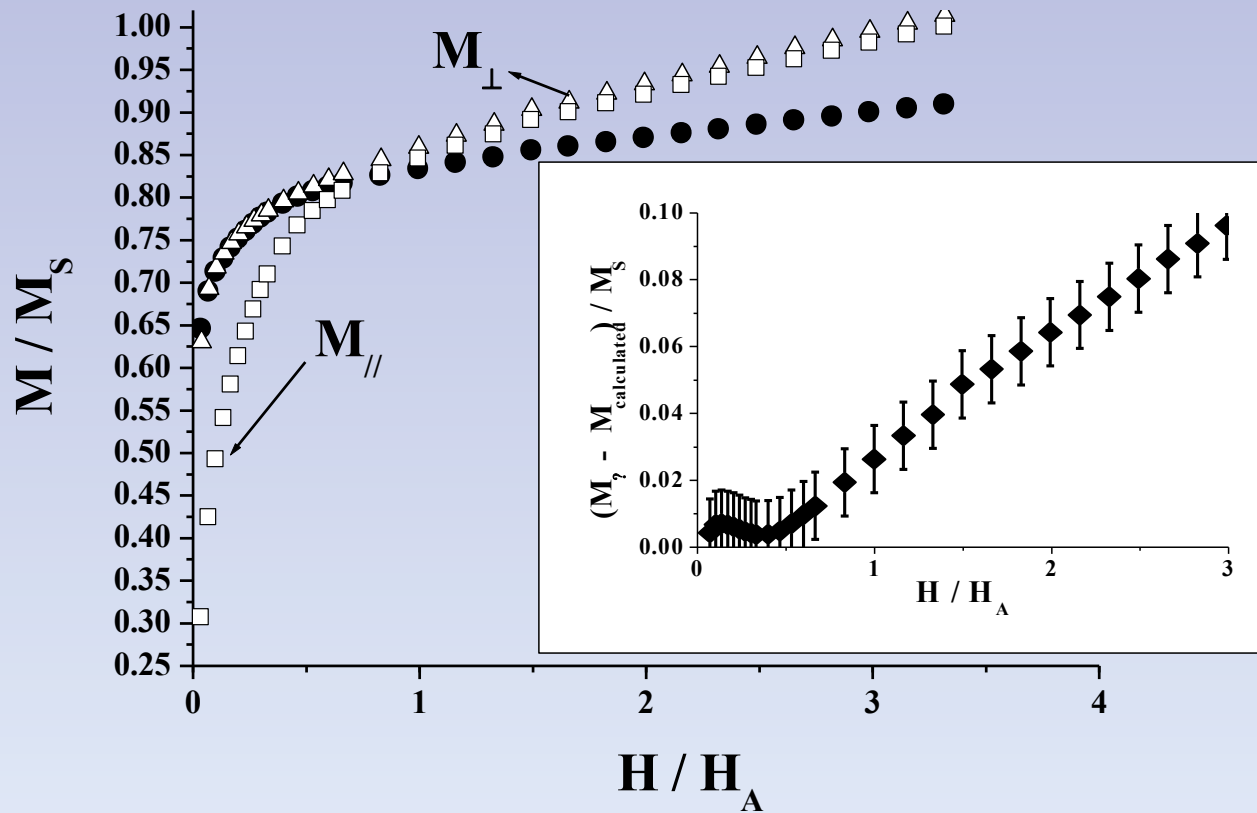
Fibre texture:

$$2\pi \int_{\theta_g=0}^{\frac{\pi}{2}} G(\theta_g) \sin\theta_g d\theta_g = 1$$

$$G(\theta_g) = (1 - \rho_0)PV(\theta_g)$$

Finally:

$$\frac{M_{\perp}}{M_S} = 2\pi \int_0^{\frac{\pi}{2}} (1 - \rho_0) PV(\theta_g) \sin\theta_g \cos(\theta_g - \theta) d\theta_g + \rho_0 M_{\text{random}}$$



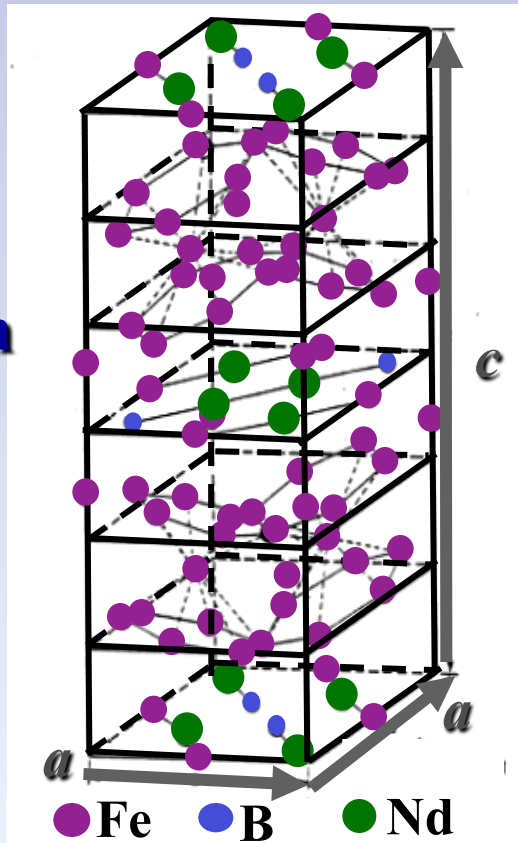
Morales, Chateigner, Fruchart: *J. Magn. Mag. Mat.* 2003

Nd₂Fe₁₄B

Crystallographic structure

Intrinsic magnetic properties: hard magnetic phase

P4₂/mnm



- Uniaxial anisotropy →
c-axis = easy magnetisation
axis
- $H_a = 7\text{T}$
- $M_s = 1.61\text{ T}$
- $T_c = 315^\circ\text{C}$

NdFe_{12-x}V_xN compounds

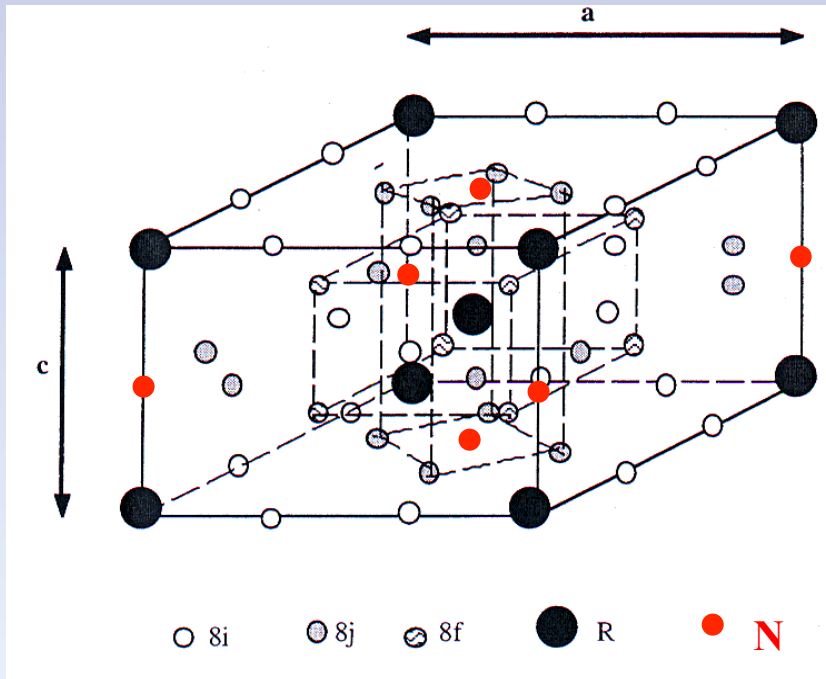
Crystallographic structure

- space group I4/mmm

Nitrogenation



N atoms in 2b sites



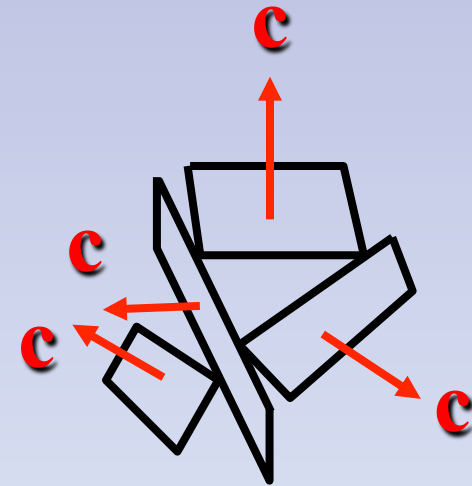
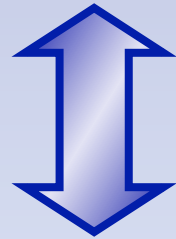
Intrinsic magnetic properties:
hard magnetic phase

- **c-axis = easy magnetisation axis**
- **H_a = 1.5 T → 11 T**
- **M_s = 1.13 T → 1.37 T**
- **T_c = 340°C → 510°C**

Permanent magnet extrinsic properties: anisotropy

ANISOTROPY

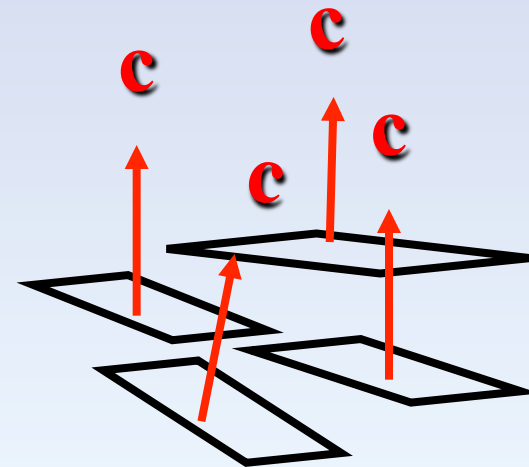
$$\frac{M_r^{//}}{M_r^{\perp}}$$



**common orientation of the easy magnetisation
axes of the crystallites**

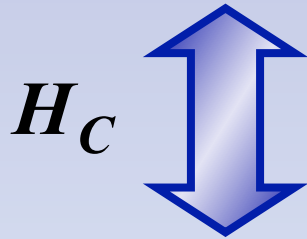
Orientation

of magnetic particles in a non magnetic matrix



Permanent magnet extrinsic properties: coercivity

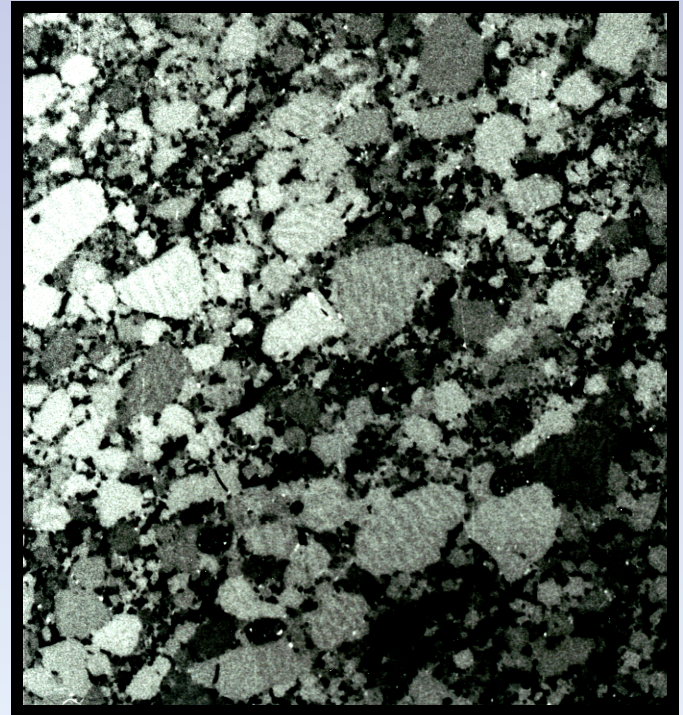
COERCIVITY



**Grain size control
of the hard magnetic phase**

**Intergranular phase distribution
→ Magnetic decoupling**

Secondary phases



10 μm

Preparation route



**Induction
Melting
and
Casting**



Hot forging



Bulk Magnet



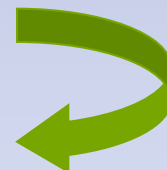
**Powdering
(HD Process)**



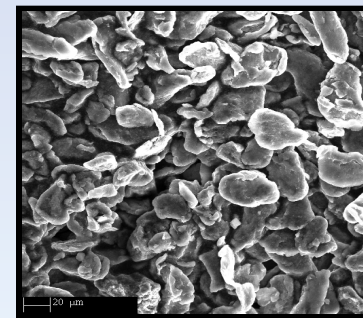
**Nitrogenation
(Nd-Fe-V)**



Magnet Powder



**Anisotropy
+
Coercivity**

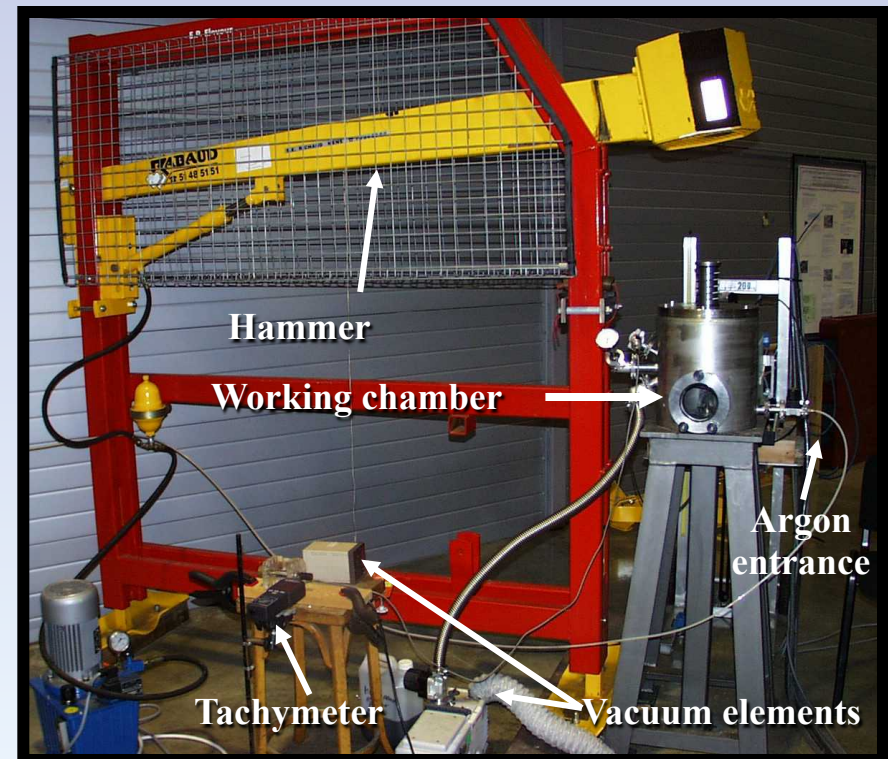
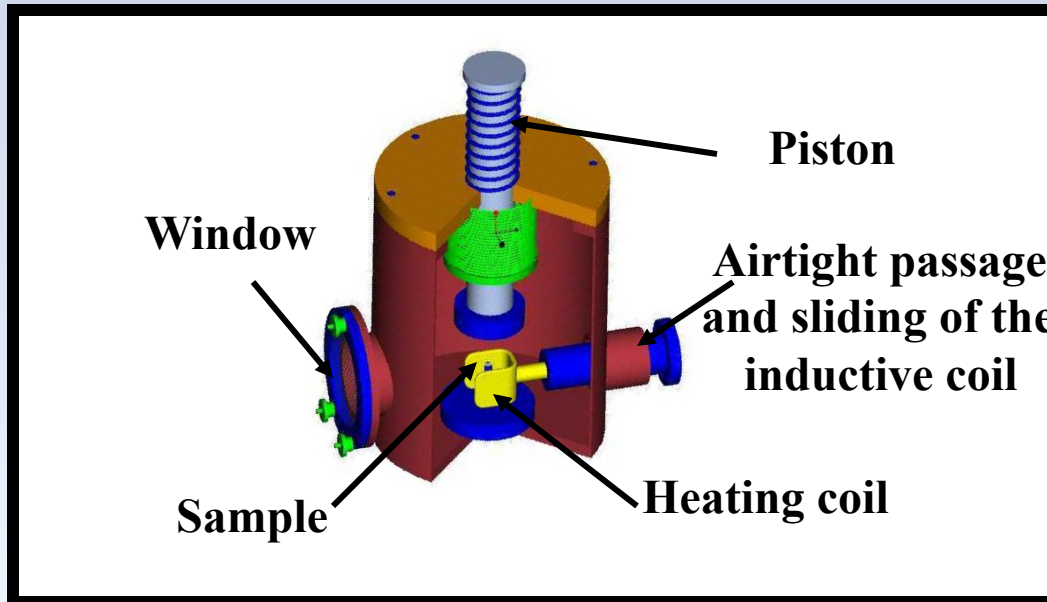


High-speed hot forging

$$\dot{\epsilon} = 125 \text{ s}^{-1}$$

Thermomechanical treatment
of the as-cast alloy
to induce permanent magnet properties

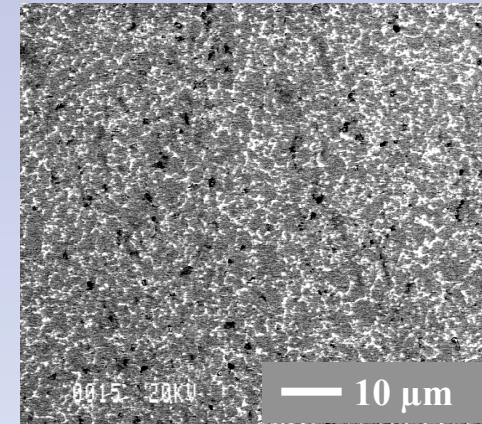
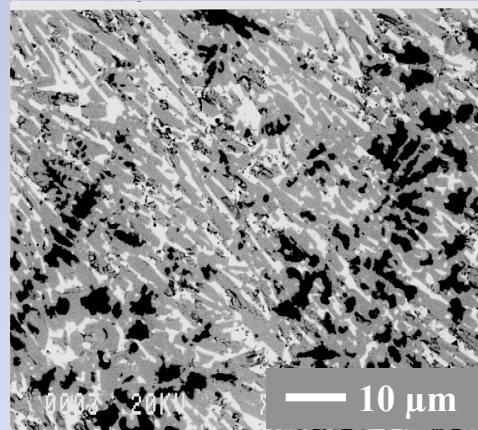
EXPERIMENTAL DEVICE



Microstructures

as-cast alloy

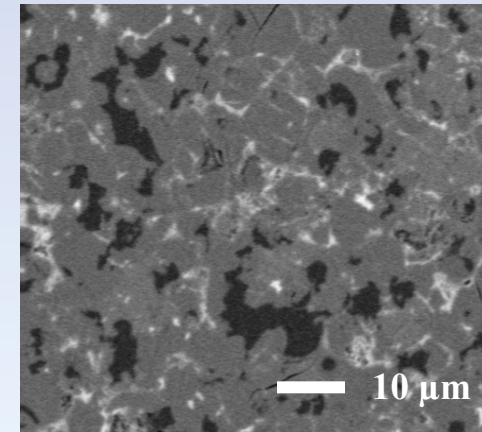
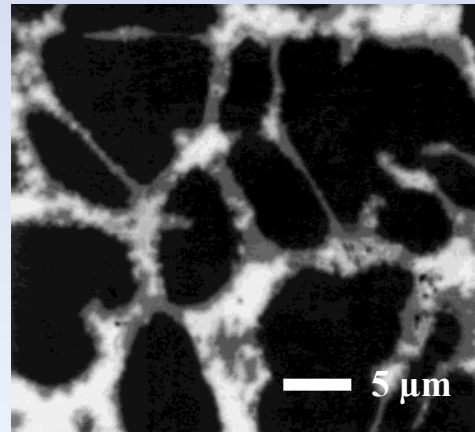
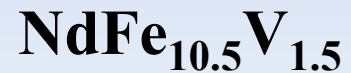
forged sample



Black: iron

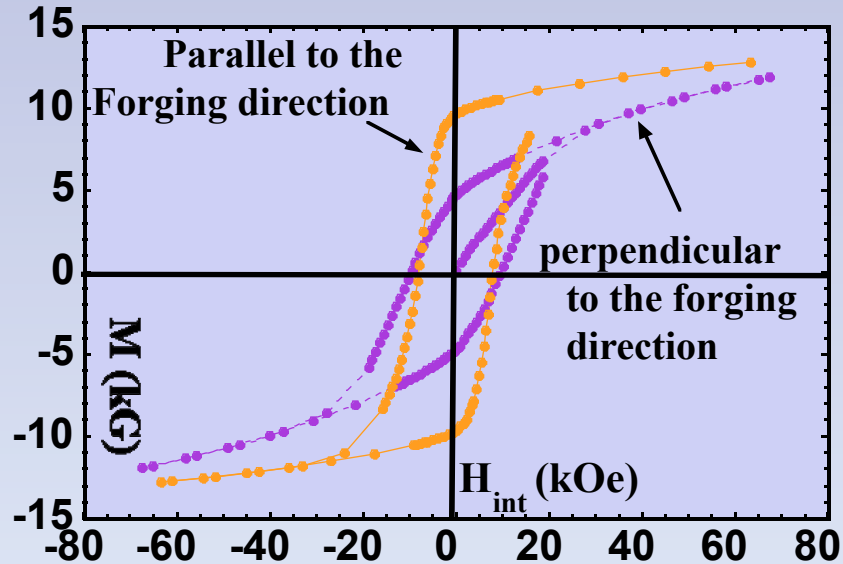
White intergranular phase

Grey: hard magnetic phase



Permanent magnet properties

Nd_{15,5}Fe₇₈B₅Cu_{1,5} alloys

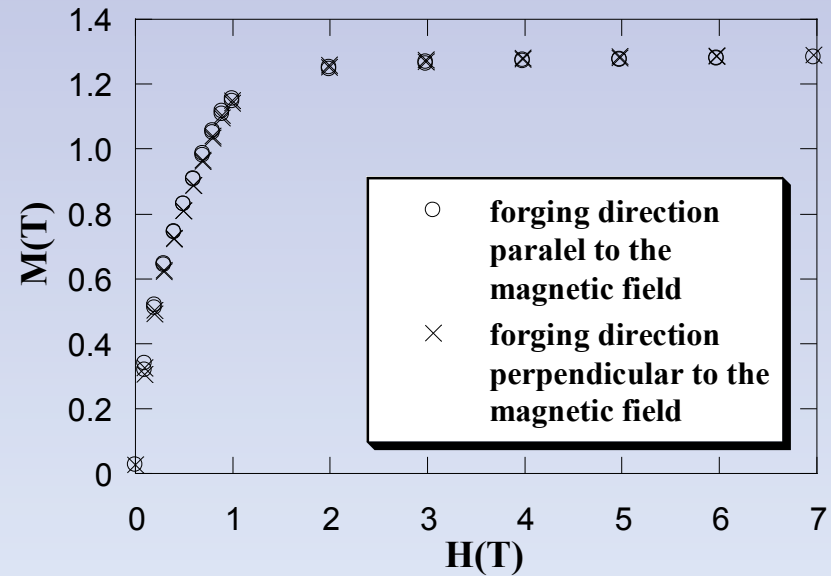


$$H_c = 10 \text{ kOe (795 kA/m)}$$

$$B_r = 10 \text{ kG (1 T)}$$

$$BH_{max} = 24 \text{ MGOe (191 kJ/m}^3\text{)}$$

NdFe_{10,5}V_{1,5}N+10% Nd alloys

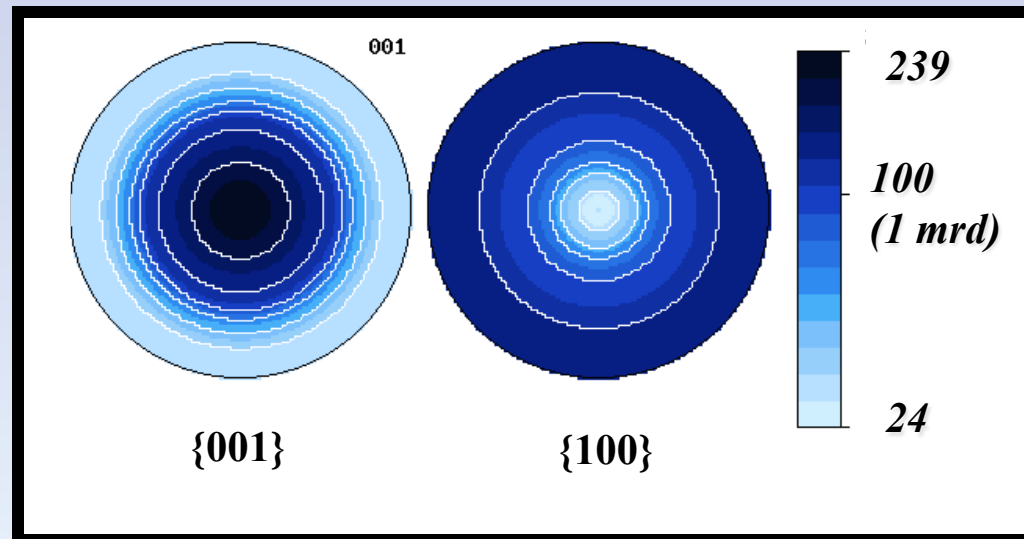


Isotropic magnet

Texture development in the Nd₂Fe₁₄B phase

ILL, D1B

⇒ **Fibre texture of Nd₂Fe₁₄B**
⇒ **c-axes // forging direction Y**



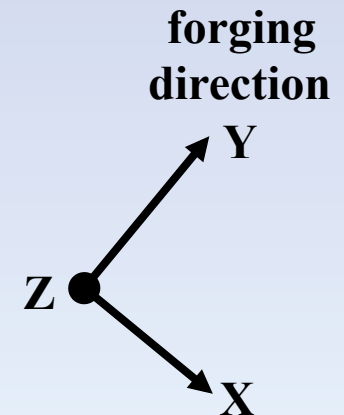
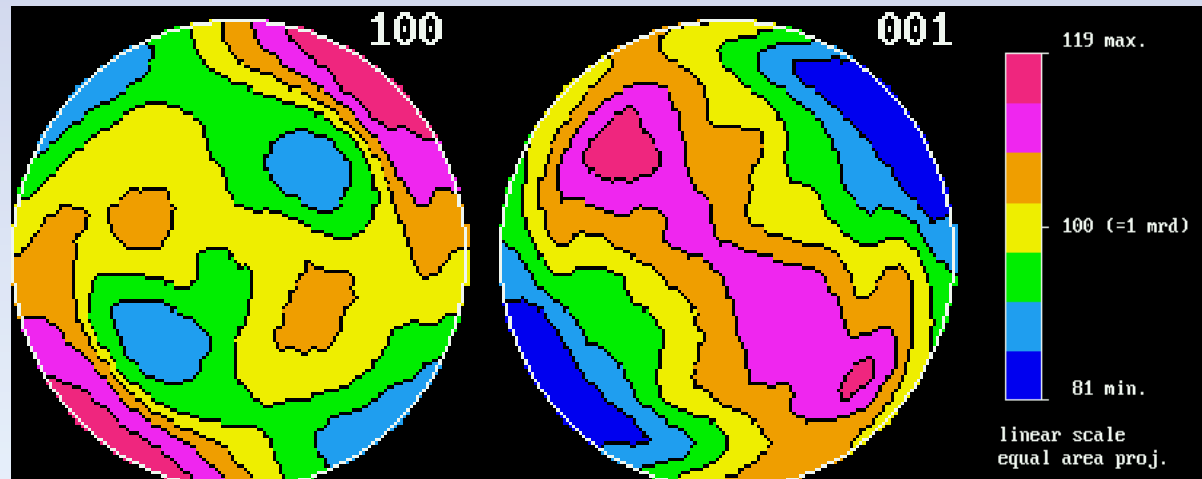
Crystallographic texture ⇒ extrinsic anisotropy

Texture investigation of the NdFe_{10.5}V_{1.5} phase

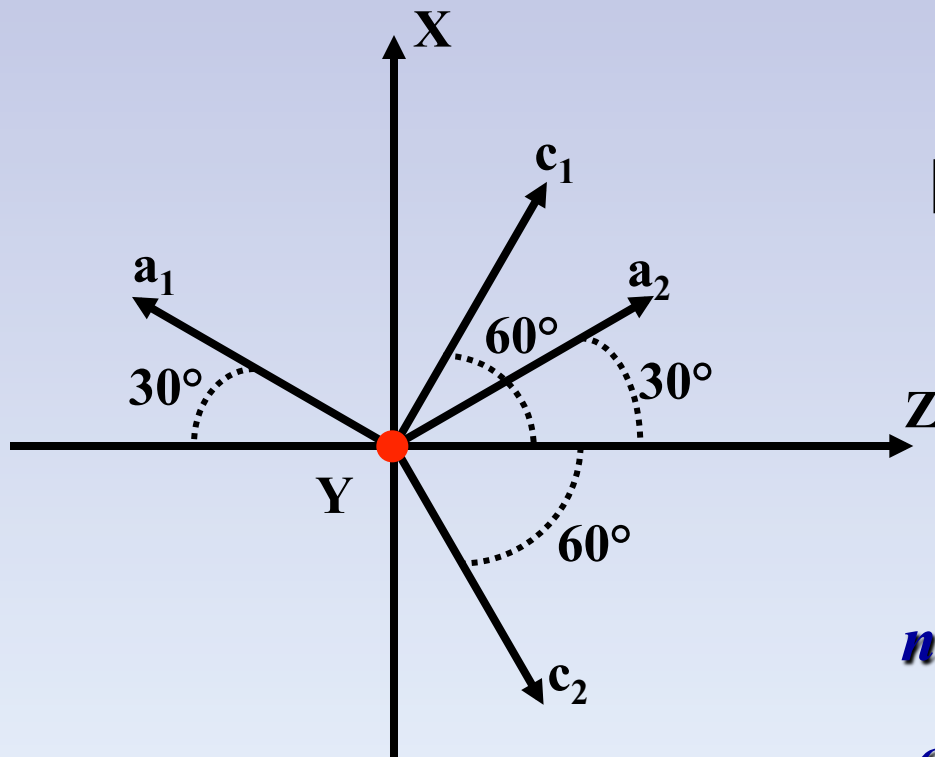
ILL, D20



**texture with $\langle 100 \rangle$ axes // forging direction Y
2 components, \approx fibre**



Texture development of the $\text{NdFe}_{10.5}\text{V}_{1.5}$ phase



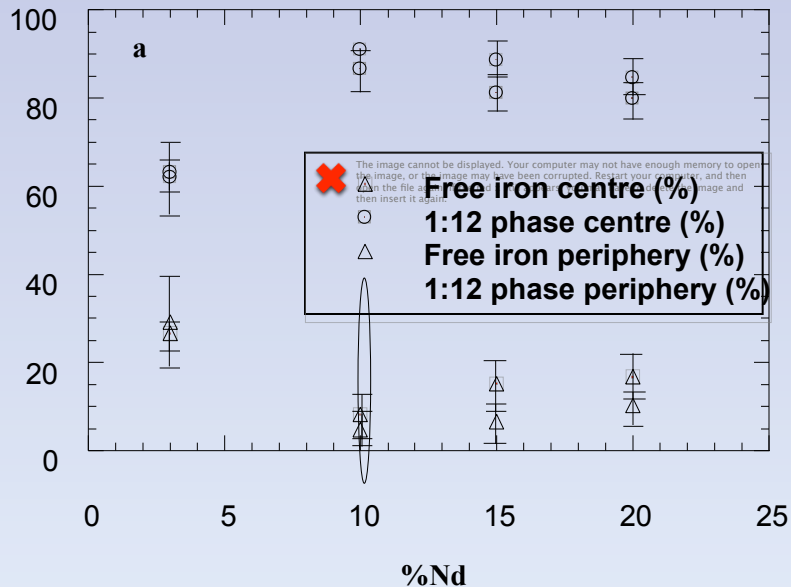
$[010] // Y$ \longleftrightarrow

$[001]$ in (X,Z) plane \perp forging
direction Y



*no extrinsic magnetic anisotropy
can be observed on forged bulks*

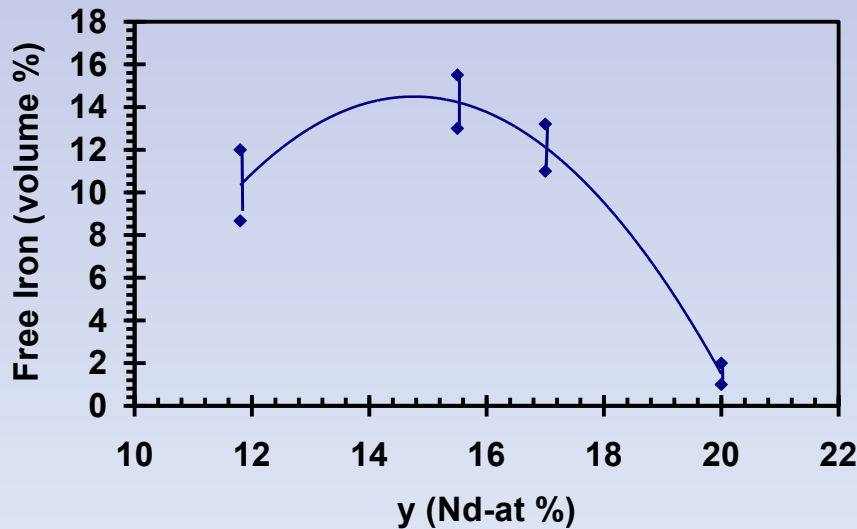
Influence of primary iron on the NdFe_{10,5}V_{1,5} phase stabilisation and texturing



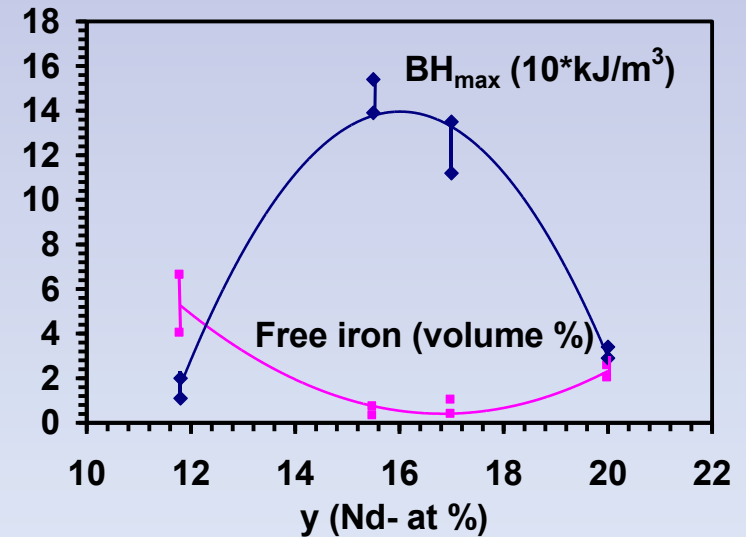
NdFeV alloys
Nd-rich phase + (Fe, V) → NdFe_{10,5}V_{1,5}

**NdFe_{10,5}V_{1,5} phase stabilisation:
optimised microstructure for Nd=10%**

Influence of primary iron on the Nd₂Fe₁₄B phase texturing



NdFeBCu as cast alloys

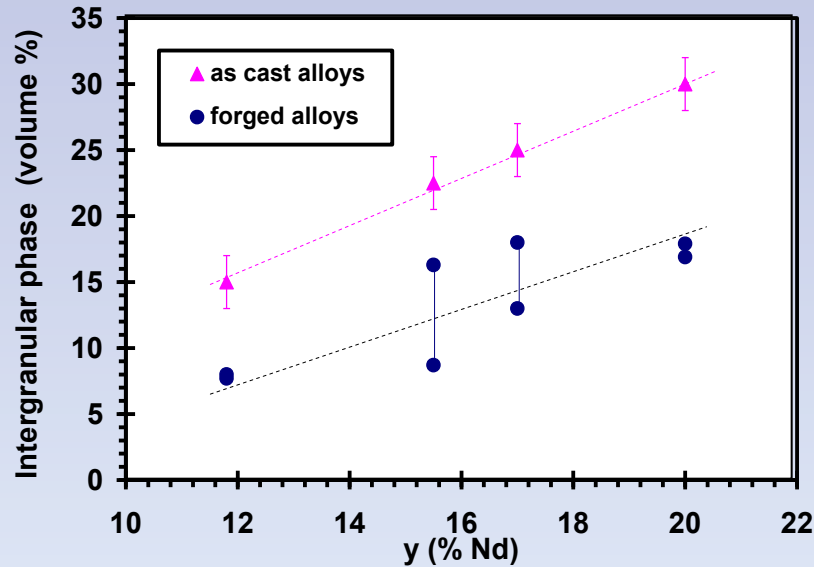


NdFeBCu forged alloys

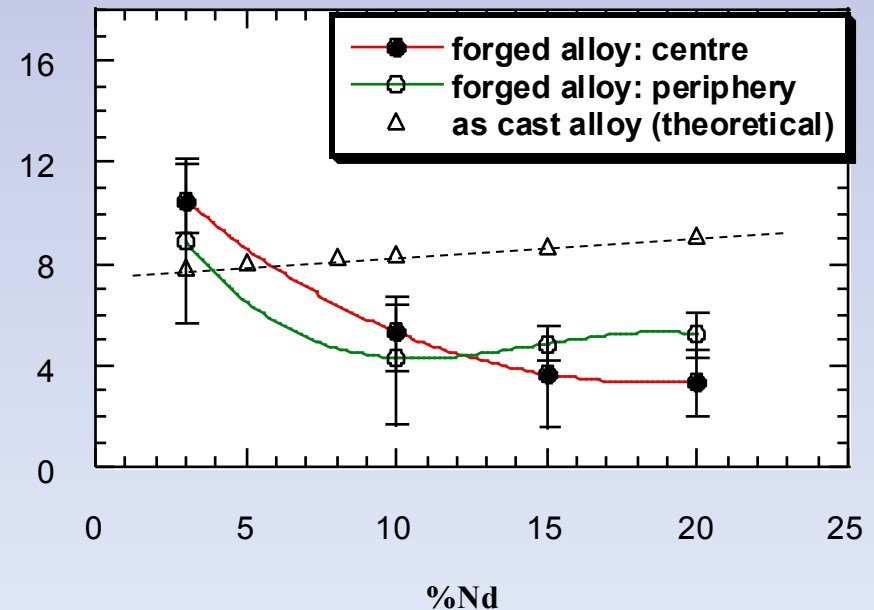
Optimised microstructure and magnetic properties
for Nd=15,5%

Influence of the intergranular volume fraction on texturing

NdFeBCu alloys



NdFeV alloys



volume of intergranular phase = volume of liquid at T_f

NdFeBCu alloys

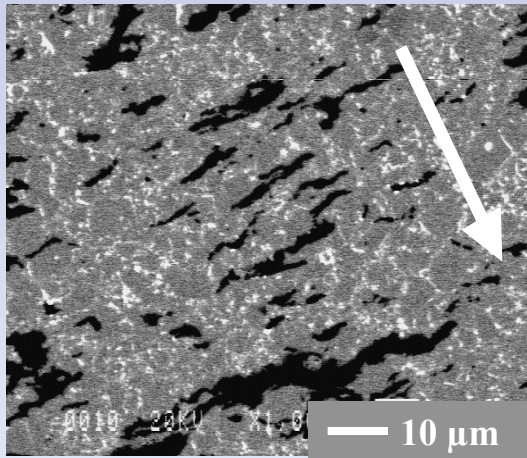
volume fraction \uparrow with %Nd

NdFeV alloys

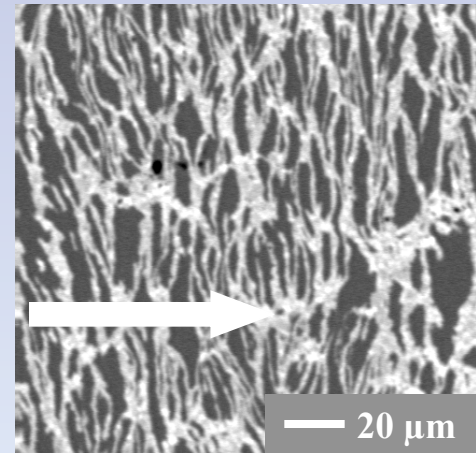
%Nd > 10%: liquid phase segregation

Effect of iron on the hot deformation process

$\text{Nd}_{15,5}\text{Fe}_{78}\text{B}_5\text{Cu}_{1,5}$



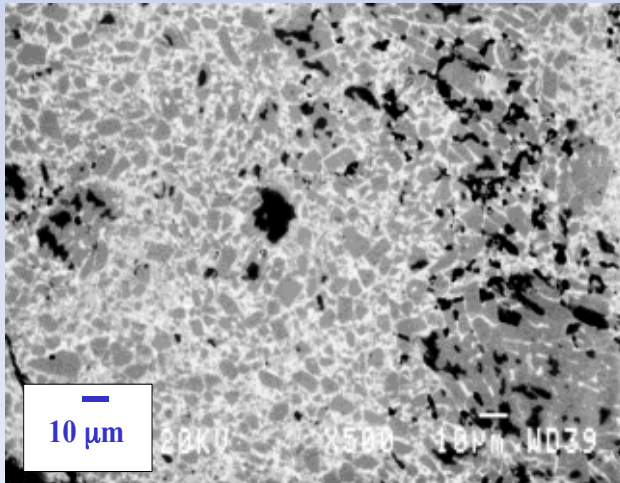
$\text{NdFe}_{10,5}\text{V}_{1,5} + 10\%\text{Nd}$



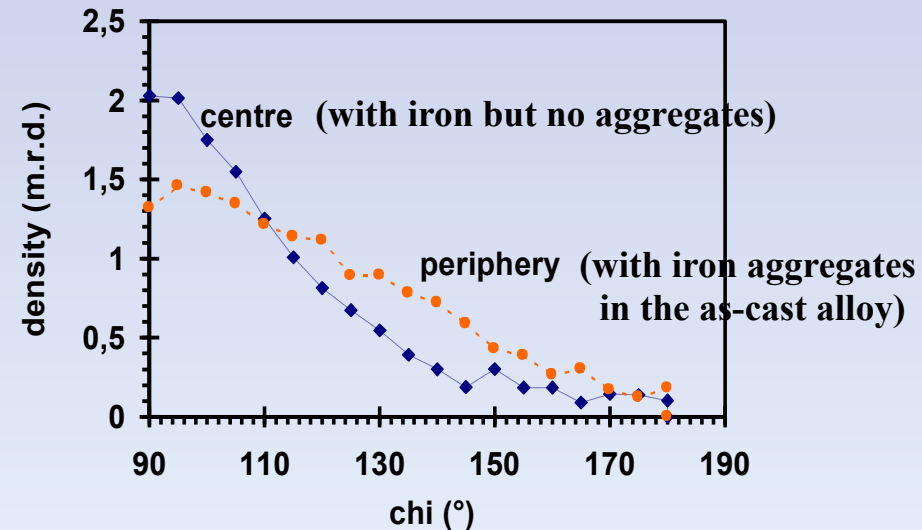
**Forging energy mainly used
for the plastic deformation of iron**

Effect of iron on the hot deformation process

**Inhomogeneous microstructure
with non deformed areas
in the periphery of the Nd_{15,5}Fe₇₈B₅Cu_{1,5} alloy**



**weaker Nd₂Fe₁₄B texture
in the presence of iron aggregates**

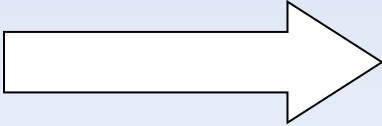


**Large amount of iron or non homogeneous distribution
detrimental to the alloy deformation process**

On the texturing mechanism of the hard magnetic phase...

Some similitudes of the Nd-Fe-V and Nd-Fe-B alloys :

- **TM-RE alloys**
- **Similar microstructures: nature of phases, proportions, distribution...**
- **At Tf: solid main phase, liquid intergranular phase**
- **At Tf: solid main phase in the brittle state**

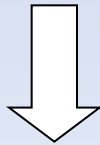
Uniaxial hot forging  **Fibre texture in both cases**

On the texturing mechanism of the hard magnetic phase...

... *But different texturing mechanisms of the Nd-Fe-V and Nd-Fe-B alloys*

NdFeBCu

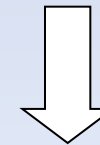
-At T_f , deformation behaviour of an alloy in the semi-solid state



Fiber texture with $\langle 001 \rangle$ axis parallel to the forging direction

NdFeV

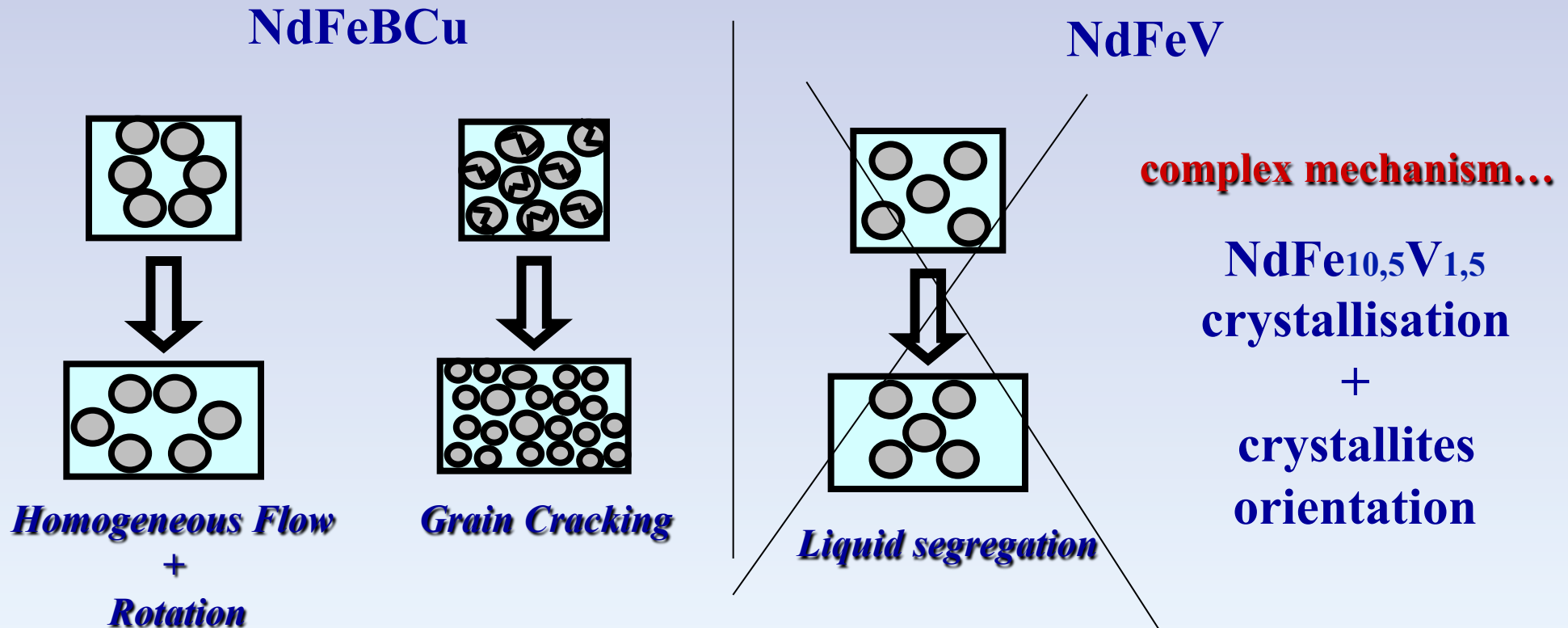
-At T_f , low liquid volume fraction
→ liquid not responsible for the main deformation process



Fiber texture with $\langle 010 \rangle$ axis parallel to the forging direction Y + 2 three-dimensional components

On the texturing mechanism of the hard magnetic phase...

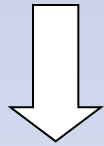
... and different deformation behaviours



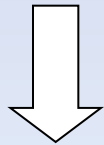
Conclusion

NdFeBCu

- $T_f = 930^\circ\text{C}$, Nd=15,5% (fl= 10%)
 $\dot{\varepsilon} = 125 \text{ s}^{-1}$



Fiber texture with $\langle 001 \rangle$ axis
parallel to the forging direction

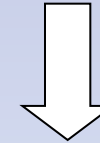


-Coercive and anisotropic powder
(patented process)

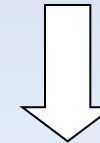
$BH_{max} = 24 \text{ MGOe}$ (191 kJ/m^3)

NdFeV

- $T_f = 980^\circ\text{C}$, Nd-excess=10% (fl<5%)
 $\dot{\varepsilon} = 125 \text{ s}^{-1}$



Fiber texture with $\langle 010 \rangle$ axis
parallel to the forging direction Y
+ 2 three-dimensional components



-Magnetic properties
still under optimisation